

Turbofan Noise Generation Volume 2: Computer Programs

by
C.S. Ventres
M.A. Theobald
W.D. Mark

(NASA-CR-167952) TURBOFAN NOISE GENERATION.
VOLUME 2: COMPUTER PROGRAMS Final Report
(Bolt, Beranek, and Newman, Inc.) 206 p
HC A10/EF A01 CSCL 20A 63/71 24800
N85-11791 Unclas



July 1982

Prepared Under Contract No. NAS3-2125

by
Bolt Beranek and Newman Inc.
Cambridge, Mass. 02138

for



National Aeronautics and
Space Administration
Lewis Research Center
Cleveland, Ohio 44135

Report No. 4770

TURBOFAN NOISE GENERATION:
VOLUME 2: COMPUTER PROGRAMS

C.S. Ventres
M.A. Theobald
W.D. Mark

April 1982

Prepared for:

National Aeronautics and Space Administration
Lewis Research Center
Cleveland, Ohio 44135

SUMMARY OF VOLUME 2

The computations for three different noise mechanisms - mean rotor wake, inlet turbulence, and rotor wake turbulence - described in Volume 1 of this report are coded as three separate computer program "packages." This arrangement was deemed reasonable because of differences in the required input data (e.g., rotor vs stator geometries), because of interest in the role of each separate noise mechanism, and for economy of execution during parametric studies. The computer codes are described by means of block diagrams, tables of data and variables, and example program executions. Reference to Volume 1 will be made via equation or figure number. FORTRAN listings of the programs appear in the appendix to Volume 2.

PRECEDING PAGE BLANK NOT FILMED

TABLE OF CONTENTS

	page
SUMMARY OF VOLUME 2	iii
LIST OF FIGURES	v
LIST OF TABLES	vi
CHAPTER 1: MEAN ROTOR WAKE PROGRAM	1
CHAPTER 2: TURBULENCE PROGRAMS	2
2.1 Inlet Turbulence Program	2
2.2 Rotor Wake Turbulence Program	3
CHAPTER 3: EXECUTION PARAMETERS AND PROGRAM LIMITA- TIONS	4
APPENDIX: PROGRAM LISTINGS	A-1

LIST OF FIGURES

	page
Figure 1. Block Diagram of Mean Rotor Wake Program	2
2. Block Diagram of Inlet Turbulence Program; Part A: Data Storage	10
3. Block Diagram of Inlet Turbulence Program; Part B: Noise Calculation	11
4. Block Diagram of Rotor Wake Turbulence Program; Part A: Data Storage	12
5. Block Diagram of Rotor Wake Turbulence Program; Part B: Noise Calculation	13
6. Schematic View of a Rotor Blade TE and Stator Vane LE Looking Down the Turbofan X Axis, in Stator-Fixed Coordinates	14
7. Schematic View of a Rotor Blade TE and Stator Vane LE Looking Perpendicular to the Rotor Axis	15
8. Typical Wake Profile	16
9. Schematic Diagram of the Stator Vane Mean Chord at the Instant When the Wake Centerline Intersects the Leading Edge	17

LIST OF TABLES

	page
Table 1. Input/Output Data for the Mean Rotor Wake Program	19
2. Important Internal Program Variables Mean Rotor Wake Program	22
3. Utility Subroutines	24
4. Sample Execution of the Mean Rotor Wake Program	30
5. Input/Output Data for the Inlet Turbulence Programs	48
6. Important Internal Variables for the Inlet Turbulence Program	51
7. Sample Execution of the Inlet Turbulence Data Storage Routine	52
8. Sample Execution of the Inlet Turbulence Noise Calculation	55
9. Input/Output Data for the Rotor Wake Turbulence Program	65
10. Important Internal Program Variables for the Rotor Wake Turbulence Program	68
11. Sample Execution of the Rotor Wake Turbulence Data Storage Routine	69
12. Sample Execution of the Rotor Wake Turbulence Noise Calculation	73

CHAPTER 1

MEAN ROTOR WAKE PROGRAM

The computer program described in Fig. 1* computes the sound power of each propagating mode for the first three harmonics of the blade passage frequency. The data required to run the program and the program results are described in Table 1.* Important FORTRAN variables used in the program are given in Table 2. Function subroutines utilized in the program are described in Table 3.

The terminal output from a sample execution of the Mean Rotor Wake Program is shown in Table 4 for the rotor/stator data provided by NASA Lewis. The mean flow velocity entering the stator is specified from measured data. The pressure amplitude and sound power of each mode for each harmonic number of the blade passage frequency are listed. Note that for a propagating mode (m,n) at harmonic s , another mode $(-m,n)$ of equal amplitude propagates with frequency $-s$. Thus the total sound power for the mode shape $(|m|, n)$ at frequency $|s| \times$ (blade passage frequency) is the sum of the two components.

*Note: Because of the number and complexity of the figures and tables, they have been collected at the end of each section of this volume. The 9 text figures and 12 tables appear before the appendix.

CHAPTER 2

TURBULENCE PROGRAMS

The calculations for two types of turbulence noise are considerably more time-consuming than for the tones of the mean-wake interaction because 1) all modes that are not cut off by the duct may be excited, i.e., there is no selection rule, as is the case for the mean-wake interaction, and 2) the noise is broadband rather than tonal, requiring the sound power at many frequencies to be calculated. For these reasons, the turbulence programs are each broken into two subsections. The method used is, first, to calculate and store, for a given number of blade radii, the pressure distributions across the rotor blades or stator vanes at a small number of frequencies over the range of interest. The power spectral density is essentially a spatial integral containing the pressure distribution and acoustic mode shape as factors in the integrand. The pressure distributions are slowly varying functions of frequency and duct radius when compared with the acoustic mode shapes. Thus it is reasonable to interpolate the pressure distribution for a specific frequency and radius from a look-up table of stored pressure values. All other variables that change with radius (or frequency) are calculated explicitly for that given radius (frequency). In this manner, convergence of the radial integration is improved by using more integration steps than there are stored pressure values. The pressure distributions are stored in binary form in a disc file for later use so that, for example, turbulence parameter values may be varied without recomputing the pressures.

2.1 Inlet Turbulence Program

The pressure distributions across the rotor blades are computed and stored as described in Fig. 2. The sound power calculation is diagrammed in Fig. 3. Input and output data for the programs are listed in Table 5. Additional program variables of possible interest to the user are given in Table 6.

Output from sample executions of the two program sections is shown in Tables 7 and 8. The input data relating to rotor geometry and performance are first entered as listed in Table 7. The pressure distributions are computed (as evidenced by the error code returned from LEQTIC; see Table 3), and the data are stored on a disc. The power spectral density for all propagating modes at a frequency of 15 times shaft rate (blade passage frequency in this 15-blade fan) is then computed, and the results are given in Table 8.

2.2 Rotor Wake Turbulence Program

The two-stage method of calculation described above is repeated for the Rotor Wake Turbulence problem. The calculation of pressure distributions across the stator vanes proceeds as shown in Fig. 4. The sound power calculation is explained in Fig. 5. Input and output data for the programs are listed in Table 9. Additional program variables are given in Table 10.

The output from sample program executions is shown in Tables 11 and 12. The mean flow into the stator may be specified as for the Mean Wake case. (Note that the print-out shown in Table 12 has been stripped of all messages other than the power spectral density per mode to minimize the amount of paper delivered for high frequencies (many modes). The standard program version would contain diagnostic messages, cut-off ratios, etc., as for Table 8.

CHAPTER 3

EXECUTION PARAMETERS AND PROGRAM LIMITATIONS

A. General Remarks

1. Specifying blade or vane geometries: Geometrical data are stored in matrix VGEOM. The number of radial positions at which data may be specified (NDAT) is presently limited to 10 by DIMENSION statements. This limitation may be lifted by increasing the size of VGEOM *in all main and subprograms*. The geometrical data are specified by proceeding radially *from hub to tip*, and *must include these two end points*. These data are linearly interpolated for integration stations between the data points.

2. Specifying mean flow distributions: Variable IVOR is a switch controlling whether a free vortex distribution (IVOR=0) or input data (IVOR=1) are used in stator calculations. Input data are stored in matrix VELOCV. The number of radial positions at which data are specified (NVELO) is presently limited to 10. This limitation may be lifted by increasing the size of VELOCV *in all main and subprograms*. The velocity data are specified by proceeding radially *from hub to tip* and *must include these two endpoints*. These data are also linearly interpolated for intermediate points in the radial integration.

3. Specifying Bessel function accuracies: The absolute accuracies for all Bessel function calculations (EB) and root convergence (EC) have been left as input parameters. Values of 0.001 and 0.0001, respectively, have been sufficient for these calculations.

4. Specifying the number of chordwise integration points: The number of chordwise integration points (NCHORD) is an input variable. DIMENSION statements currently limit the value of NCHORD to 20 in all programs. A value of 8 has yielded sufficient accuracy in the cases checked to date. Execution time increases radically for increases in NCHORD, so its value should be minimized. For cases where the acoustic wavelength is considerably less than the blade or stator chord, it may be necessary to increase NCHORD beyond 8. If NCHORD must be increased beyond 20, the following array sizes must be inspected and/or increased: CASCET, PHASE, DELTAP, F, A, WA, and B.

5. Specifying the number of radial integration points: The number of radial integration points (NRAD in Mean Wake, or NRADNU in the turbulence programs) is an input variable. The value must be large enough to achieve convergence of the result, yet small enough to minimize program execution time. A value of 7 has yielded adequate accuracy (± 1 dB) for the acoustic power levels in cases checked to date. The value of 20 must not be exceeded without inspecting and/or increasing the sizes of arrays PSISTO, BJ, RR, RRNU, and CASCET.

B. Turbulence Programs

1. Specifying the number of radial positions for pressure calculations: Both turbulence programs compute and store pressure distributions at a number (NRAD) of radial positions. Acoustic calculations are later performed by using NRADNU ($>NRAD$) integration points. This arrangement minimizes the execution time needed for pressure calculations while maintaining good accuracy in the radial integral. NRAD values of 5 have been used for the test cases cited here. NRAD may not be increased beyond 20 without violating DIMENSION statements, as discussed in Sec. A.5.

2. Range of Mode Number m : The turbulence programs that compute power spectral densities contain a summation of autocorrelation functions that vary with mode number m . If the annular duct/turbofan arrangement were to allow propagation of modes with mode number $|m|$ greater than 49 at a given frequency, then program execution would be terminated with an error message. This range may be increased by increasing the size of arrays ISUMTO and SUMTOT and by changing the decision value in the associated IF statement.

3. Selection of frequency values for data storage: The turbulence programs compute and store pressure distributions for a range of frequencies for later interpolation. The most useful frequencies to calculate in the subject spectrum of, for example, from 1 to 3 times the blade passage frequency (BPF), are probably the first, second, and third harmonics of BPF. This range is straightforwardly specified for the wake turbulence program. An important qualification to this procedure must be invoked for inflow turbulence, as explained below.

ORIGINAL PAGE 13
OF POOR QUALITY

The sound power calculations for the inflow turbulence routine require pressure distribution data for frequencies up to an equivalent frequency

$$(\omega^*/\Omega) = (\omega/\Omega)_{\max} + |m_{\max}| + m_{\text{sum}},$$

where $(\omega/\Omega)_{\max}$ is the highest frequency of interest, m_{\max} is the largest value of m which can propagate at frequency (ω/Ω) , and $m_{\text{sum}} = -|m_{\max}| + (\ell B)$ for some integer ℓ such that $0 \leq m_{\text{sum}} \leq B-1$, for B =number of rotor blades. Thus, before computing the pressure distribution, the user must know what modes can propagate for the turbofan under discussion. The utility program MAPIN/MAPPER (see appendix) will yield the propagating modes for a given geometry, frequency, and turbofan speed. As an example, suppose that the turbulence noise spectrum between BPF and 3BPF is desired for NASA Rotor 55 with the operating conditions: Number of blades = 15, $M_t = 0.508$, $M = 0.323$, and $\sigma_r = 0.484$. Pressure data will be needed from the lowest frequency of interest ($\omega/\Omega = \text{BPF} = 15$) to the highest equivalent frequency (ω^*/Ω). Program MAPIN/MAPPER reveals that $|m_{\max}| = 21$ for $(\omega/\Omega) = 3\text{BPF} = 45$. Thus,

$$(\omega^*/\Omega) = (\omega/\Omega)_{\max} + |m_{\max}| + m_{\text{sum}}$$

$$(\omega^*/\Omega) = 45 + 21 + 9 = 75,$$

$$\text{where } m_{\text{sum}} = -21 + (2 \cdot 15) = 9.$$

In the example, (ω^*/Ω) conveniently falls at the fifth multiple of blade passage frequency (5BPF) or $\omega/\Omega = 75$. The frequency range for pressure distribution calculations is then from $(\omega/\Omega) = 15$ to $(\omega/\Omega) = 75$ in steps of $(\omega/\Omega) = 15$. The results of calculations for that case are shown in Table 7. If programs INSRCH/INTURB were to be executed without pressure data of sufficiently high equivalent frequency, the program execution would be terminated with an error message.

4. DIMENSION of storage matrix CASCET: Pressure distributions are stored on the disc in matrix CASCET. It is desirable to keep this matrix as small as possible to minimize core and disc file requirement.. The DIMENSION of CASCET should therefore be adjusted as follows to suit the data: DIMENSION CASCET (NCHORD, NRAD, NBLADE, PRANGE), where NCHORD = number of chordwise integration points, NRAD = number of radial positions for pressure calculations, NBLADE = number of rotor blades, or, for the Rotor Wake Turbulence Program, use NVANE = number of stator vanes. PRANGE = number of frequencies for pressure calculations.

FIGURES

Calculate the sound power of each propagating mode for the first 3 harmonics of the blade passage frequency.

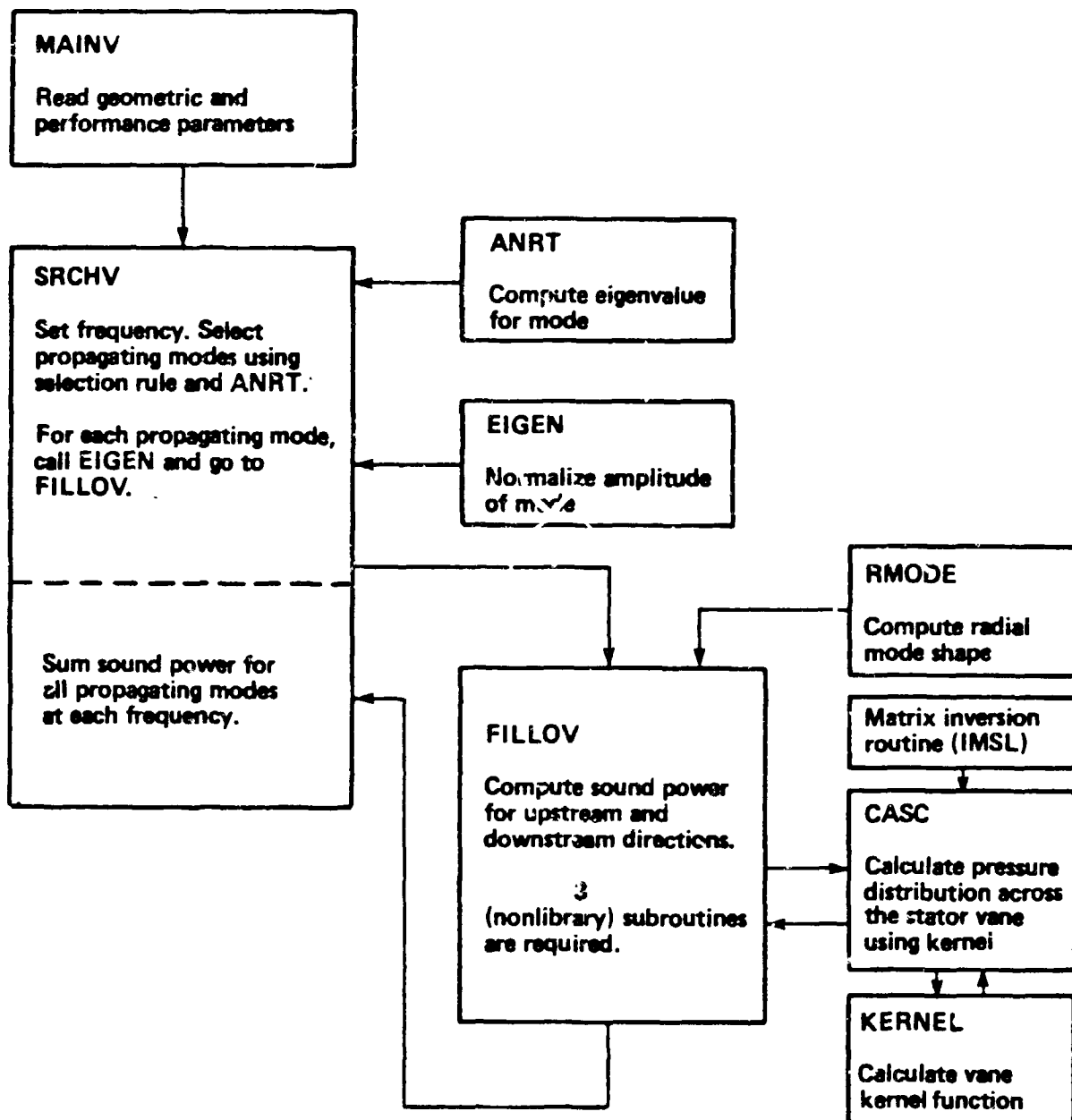


Figure 1. Block Diagram of Mean Rotor Wake Program

A. Calculate pressure distributions across the rotor blades and store data on the disk.

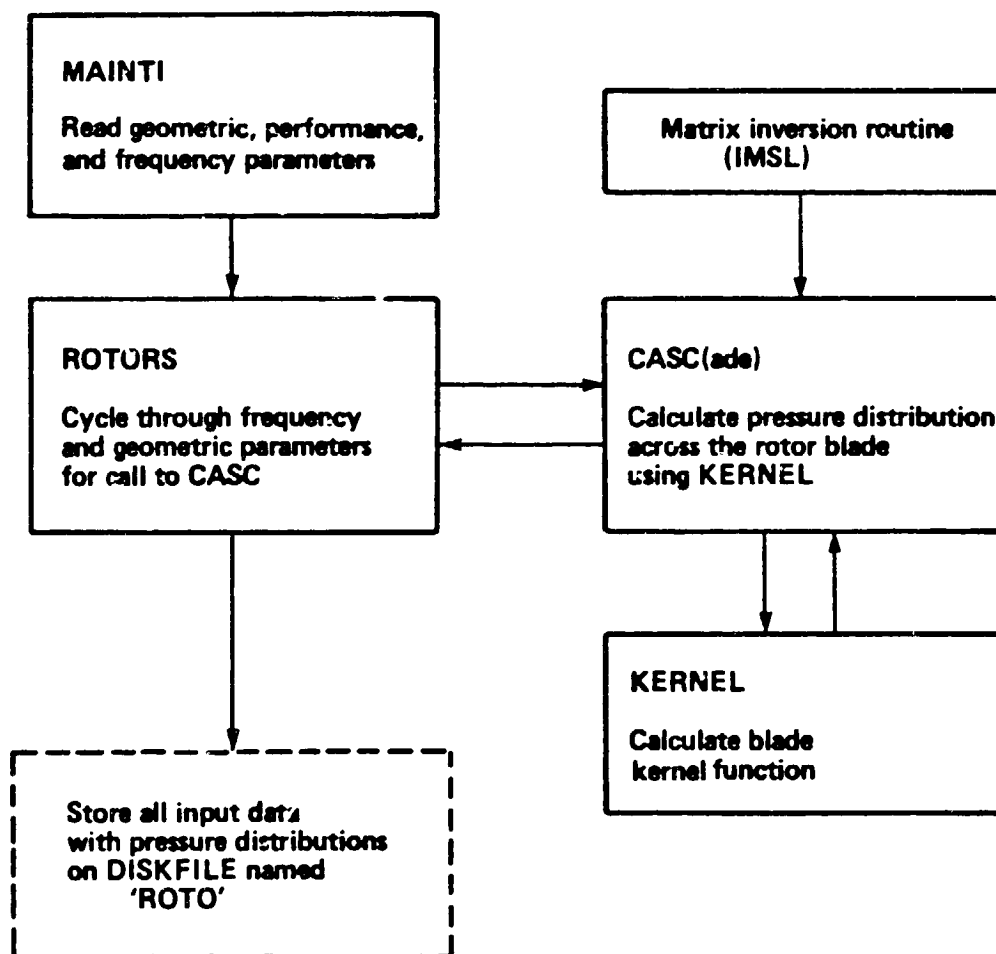


Figure 2. Block Diagram of Inlet Turbulence Program;
Part A: Data Storage

B. Calculate the power spectral density of each propagating mode at a given frequency and the total PSD for all modes.

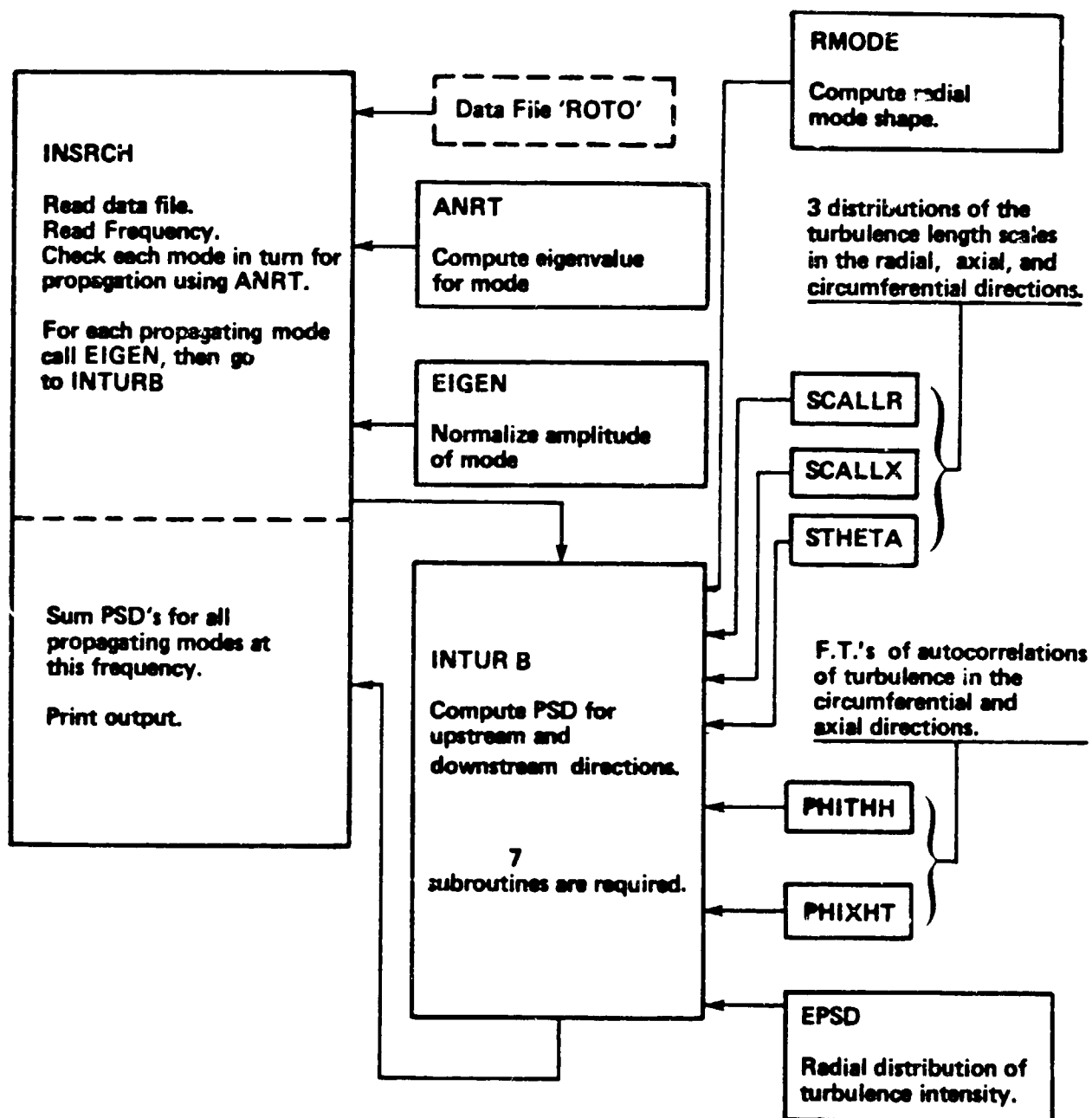


Figure 3. Block Diagram of Inlet Turbulence Program;
Part B: Noise Calculation

A. Calculate pressure distributions across the stator vanes and store data on the disk.

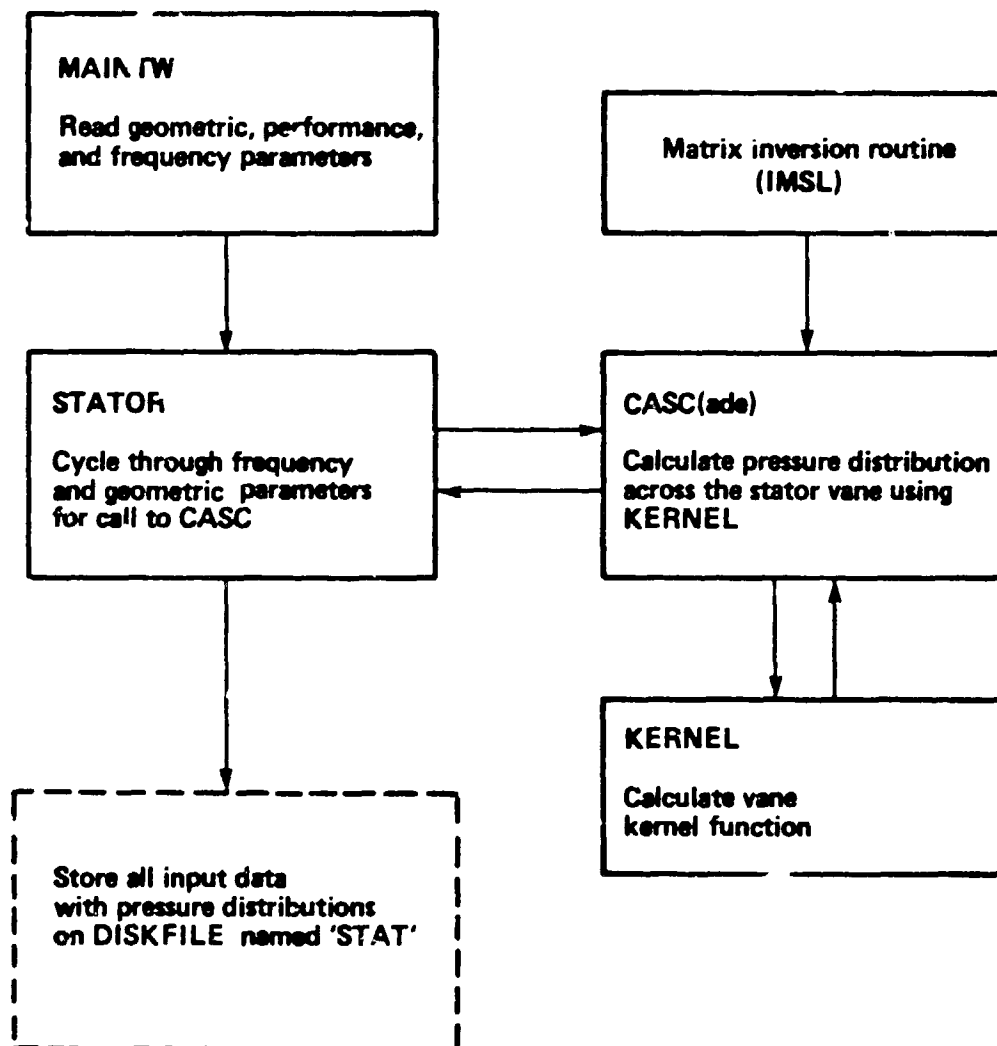


Figure 4. Block Diagram of Rotor Wake Turbulence Program;
Part A: Data Storage

B. Calculate the power spectral density of each propagating mode at a given frequency and the total PSD for all modes.

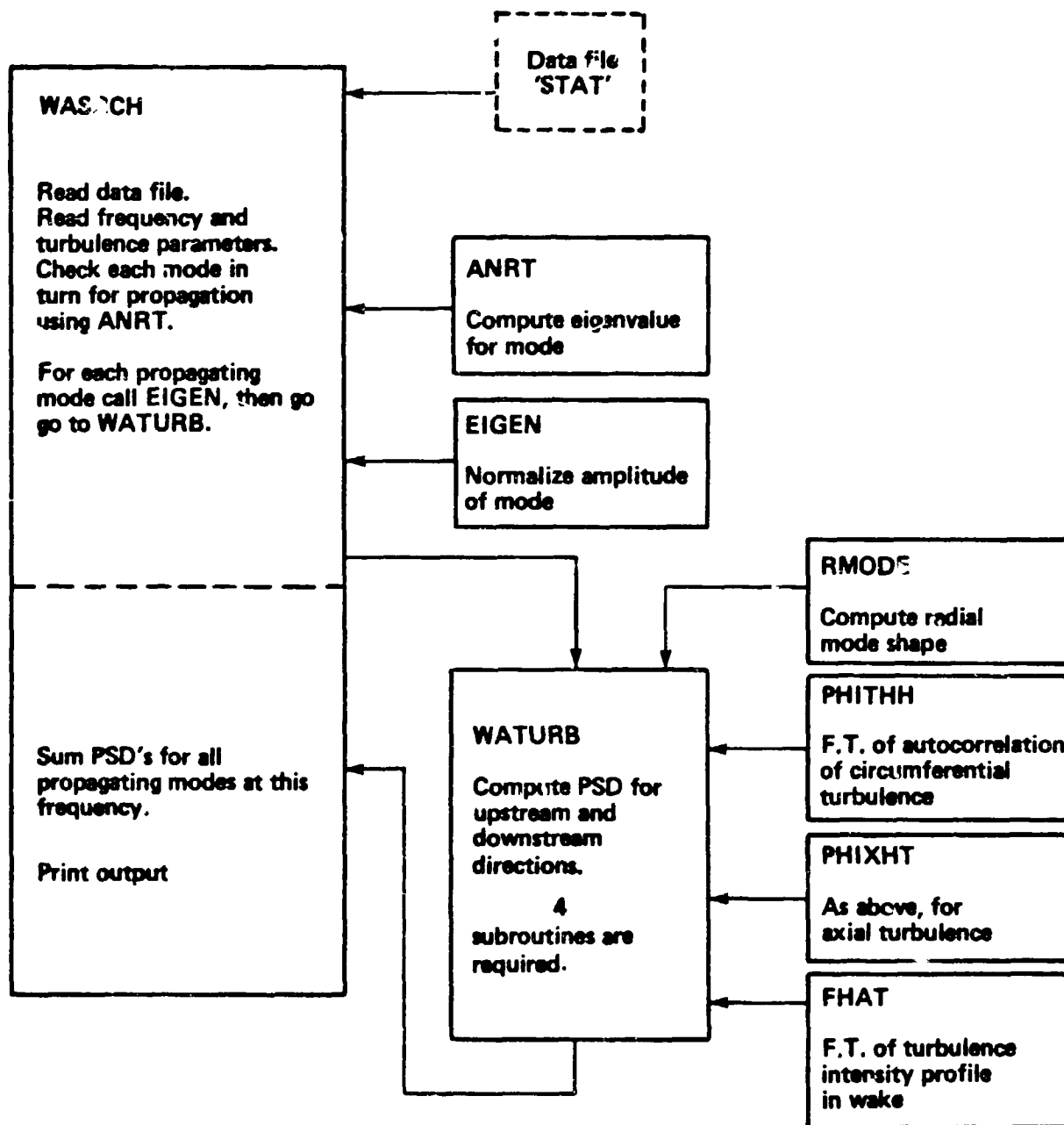


Figure 5. Block Diagram of Rotor Wake Turbulence Program;
Part B: Noise Calculation

ORIGINAL PAGE IS
OF POOR QUALITY

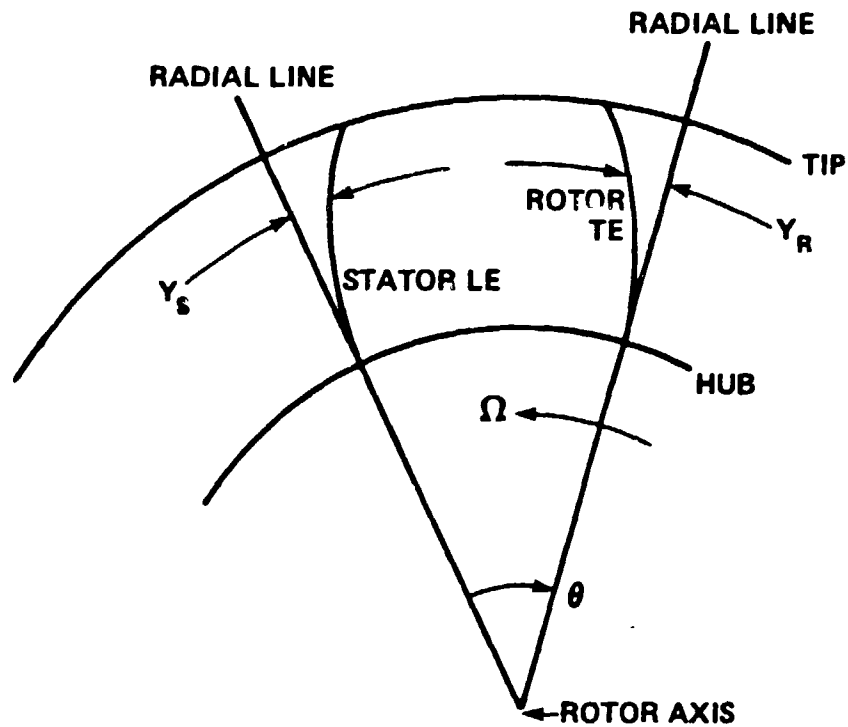


Figure 6. Schematic View of a Rotor Blade TE and Stator Vane LE Looking Down the Turbopan X Axis, in Stator-Fixed Coordinates

ORIGINAL PAGE IS
OF POOR QUALITY

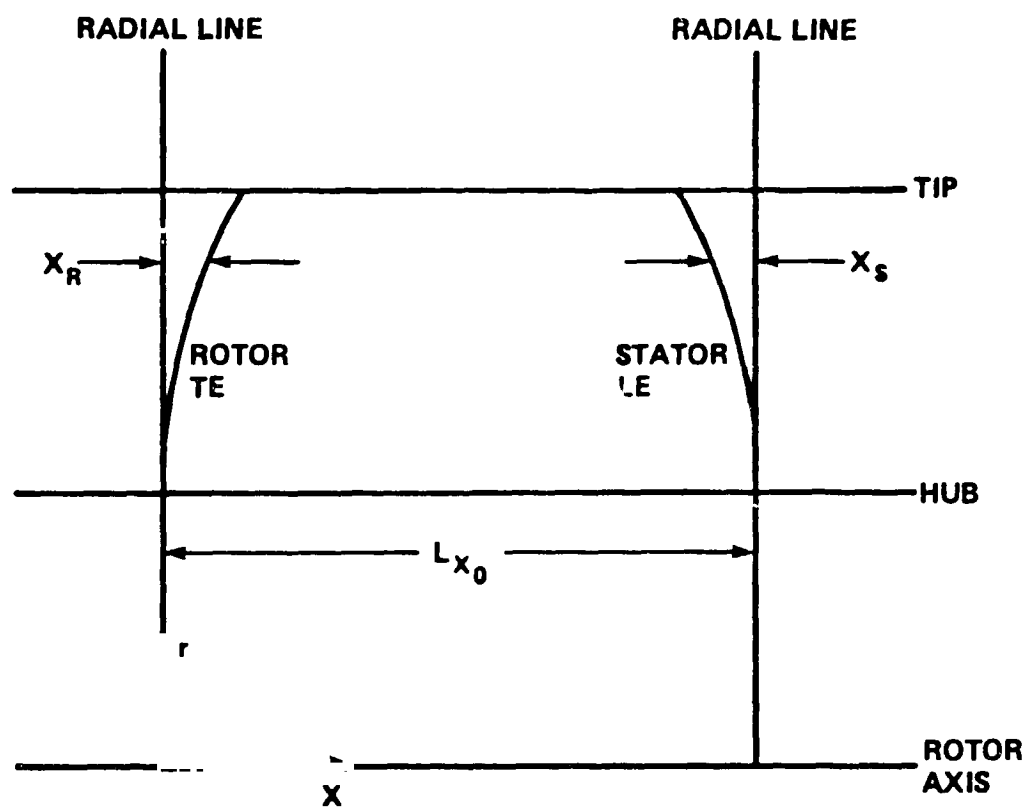


Figure 7. Schematic View of a Rotor Blade TE and Stator Vane LE Looking Perpendicular to the Rotor Axis

ORIGINAL PAGE IS
OF POOR QUALITY

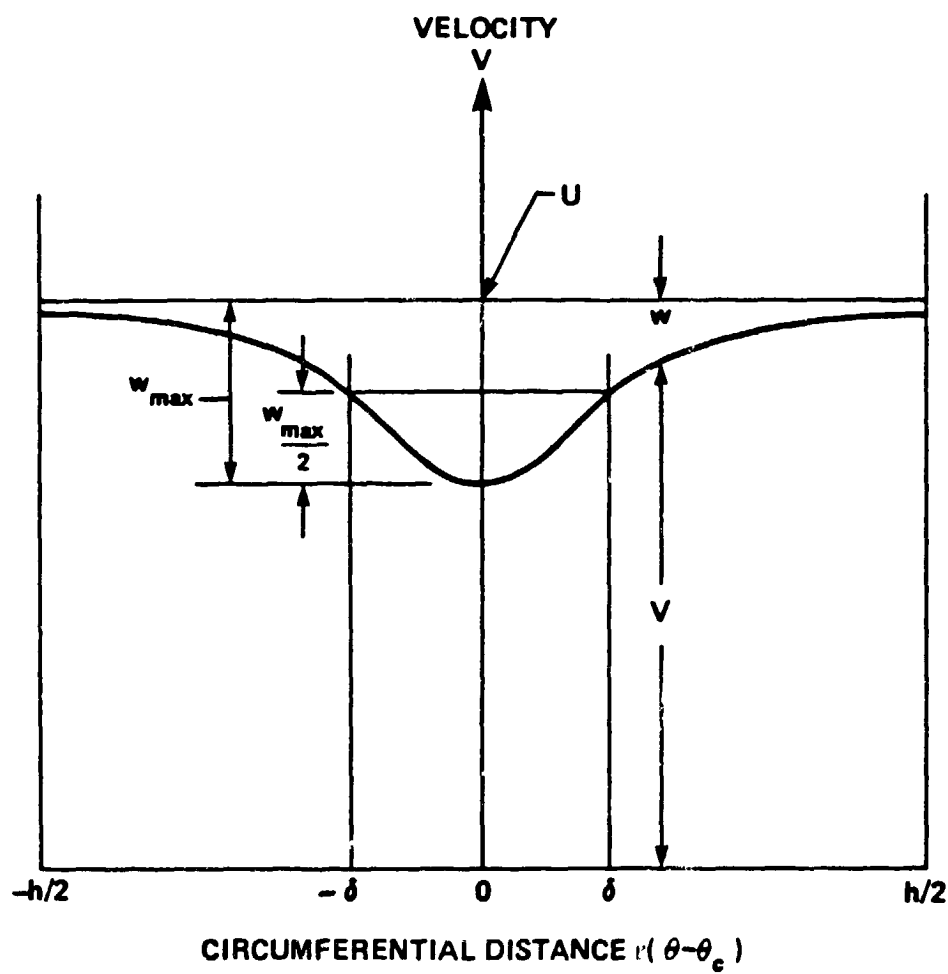


Figure 8. Typical Wake Profile

ORIGINAL PAGE IS
OF POOR QUALITY

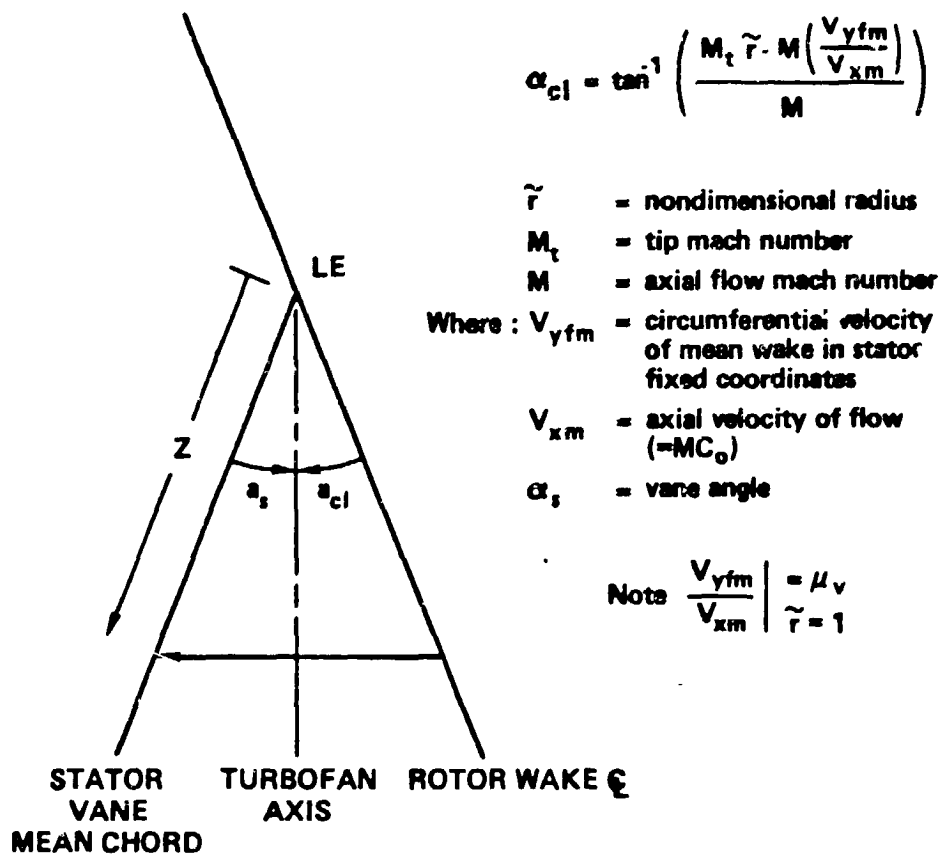


Figure 9. Schematic Diagram of the Stator Vane Mean Chord at the Instant When the Wake Centerline Intersects the Leading Edge

TABLES

TABLE 1. INPUT/OUTPUT DATA FOR THE MEAN ROTOR WAKE PROGRAM

This program calculates the complex modal amplitude and the modal sound power generated by the interaction of the mean rotor wakes with the stator vanes. All input and output data are nondimensional. The input data consist of geometric, performance, and computational parameters.

A. Geometric Data

	FORTTRAN NAME	SYMBOL	VARIABLE	FORTTRAN VARIABLE TYPE
1.	NBLADE	B	No. of rotor blades	Integer
2.	NVANE	V	No. of stator vanes	Integer
3.	SIGMAR	σ_r	Ratio of hub radius to duct radius	Floating Point
4.	SIGMAC	σ_c	Ratio of tip chord of stator vane to duct radius	Floating Point
5.	LXO	d/r_{duct}	Ratio of rotor-stator spacing to duct radius	Floating Point
6.			Vector of data for a number, NDAT (an integer variable) of stator vane radii	
a.	R	\tilde{r}	Nondimensional radius = r/r_{duct}	Floating Point
b.	C	\tilde{c}	Nondimensional vane chord = c/c_{tip}	Floating Point
c.	ALPHAS	α_s	Vane angle (degrees)	Floating Point
d.	YS*	\tilde{Y}_S	Nonradial variation of stator leading edge = Y_S/c_{tip}	Floating Point
e.	YR*	\tilde{Y}_R	Nonradial variation of rotor trailing edge = Y_R/c_{tip}	Floating Point
f.	XS**	\tilde{X}_S	Axial variation of stator leading edge = X_S/c_{tip}	Floating Point
g.	XR**	\tilde{X}_R	Axial variation of rotor trailing edge = X_R/c_{tip}	Floating Point

*See Figure 6

**See Figure 7

ORIGINAL PAGE IS
OF POOR QUALITY

TABLE 1. (Cont.)

Performance Data

FORTRAN NAME		SYMBOL	DESCRIPTION	FORTTRAN VARIABLE TYPE
1.	MT	M_t	Tip Mach number	Floating Point
2.	MA	M	Axial flow Mach number	Floating Point
3.	IVOR	-	Switch for rotor wake specification = 0 for free vortex distribution = 1 for specified input velocity distribution	Integer
4.			(for IVOR = 1) Vector of data for a number, NVELO, (an integer variable) of vane radii	
	R	\bar{r}	a. Nondimensional radius	Floating Point
	XVEL	$\frac{V_{yfm}}{V_{xm}}$	b. Ratio of circumferential velocity to axial flow velocity of the mean wake (See Fig. 9)	Floating Point
5.	MUV	μ_v	(for IVOR = 0) Ratio of circumfer- ential velocity at the duct radius to the axial flow velocity	Floating Point
6.	WWIDTH	δ/h	Ratio of wake half-width to wake spacing (See Fig. 8)	Floating Point
7.	VELDEF	W_{max}/U	Ratio of maximum wake velocity deficit to the streamwise flow velocity (assumed constant with radius). (See Fig. 8)	Floating Point

ORIGINAL PAGE IS
OF POOR QUALITY

TABLE 1. (Cont.)

C. Computational Data

These data set the number of integration stations in the chordwise and spanwise directions (and, indirectly, the accuracy of the results). The required accuracy for the Bessel functions used in the mode shape and eigenvalue routines are also specified.

	FORTTRAN NAME	VARIABLE	FORTTRAN VARIABLE TYPE
1.	NRAD	No. of integration stations in the radial direction (odd number)	Integer
2.	NCHORD	No. of integration stations in the chordwise direction (even number)	Integer
3.	EB	Absolute accuracy of all Bessel function calculations	Floating Point
4.	EC	Absolute accuracy of convergence to root of eigenvalue equation	Floating Point

Program Output

The output lists the complex nondimensional pressure amplitude for each propagating mode. The amplitude is nondimensionalized by the dynamic pressure of the mean axial flow $\rho_0 U^2/2$. Also given is the *relative* modal sound power level. To recover the conventional sound power level (dB re 10^{-12} watt) add

$$10 \log_{10} \left[\frac{\rho_0 c_0^3 M^4 r_{\text{duct}}^2}{8 \cdot 10^{-12}} \right]$$

to the computed relative power. This step is required because all computations performed in the program are nondimensional with absolute values of ρ_0 , c_0 , and r_{duct} unknown.

TABLE 2. IMPORTANT INTERNAL PROGRAM VARIABLES
MEAN ROTOR WAKE PROGRAM

(Used in addition to the INPUT/OUTPUT variables.)

FORTRAN NAME	SYMBOL	VARIABLE
AMN*	$A_{m,n}$	Weighting factors of mode shape $\psi = A_{m,n} J_m + B_{m,n} Y_m$
BMN*	$B_{m,n}$	
ARG*	$X_{m,n}$	Argument of the mode shape function ψ ($=\kappa_{m,n} r$)
B*	b	Nondimensional vane semi-chord $= c/2c_{tip}$
BETASQ*	β^2	$1-M^2$, where M is the axial flow Mach no.
DELTAP	$\Delta \bar{p}$	Nondimensional complex pressure along vane chord
DELTAR*	$\Delta \bar{r}$	Discrete radial interval for integration
GAMMA	Γ	Nondimensional wave number of the convected gust
GMNS*	$\tilde{\gamma}_{m,n,s}$	Nondimensional acoustic wavenumber for moving medium (See Eq. 87 of Vol. 1)
H1	h_1	Nondimensional stator vane spacing in direction parallel to vane (See Fig. B-1 of Vol. 1)
H2	h_2	Nondimensional stator vane spacing in direction perpendicular to vane (See Fig. B-1 of Vol. 1)
IER*, IERPS1	-	Error codes from Bessel function subroutines
IR*	-	Counter for integration stations in radial direction
IZ*	-	Counter for integration stations in chordwise direction
KMNS*	$K_{m,n,s}$	Nondimensional acoustic wavenumber $= r_{duct} \cdot K_{m,n,s}$ (See Eq. 88 of Vol. 1)

TABLE 2. (Cont.)

ORIGINAL PAGE IS
OF POOR QUALITY

KX	k_x	Nondimensional gust wavenumber in the axial direction
MM*	m	Circumferential mode number
MR	M_r	Relative Mach number of mean wake (vector sum of rotational and axial components)
MYM	-	Relative circumferential Mach no. of mean wake at \bar{r} .
NN*	n	Radial mode number
PMNS	-	Sum of terms comprising the radial integral
PSI*, OR PSISTO*	ψ	Nondimensional radial mode shape as a function of radius
QMNS	-	Sum of terms comprising the chordwise integral
R*	\bar{r}	Nondimensional radius = r/r_{duct}
RELPRL	-	Relative modal sound power level at harmonic s
REPLWR, SPWR	-	Relative modal sound power at harmonic s
SB	sB	Product of harmonic number and no. of blades
SS	s	Harmonic number (=1,2,3) multiple of the rotor blade passage frequency
WH	\hat{w}	Complex nondimensional amplitude of gust velocity impinging on stator vane
WHTC	-	Weighting factor for Simpson Integration method used in chordwise integral
XMN*	$\kappa_{m,n} r_{\text{duct}}$	Nondimensional root of duct eigenvalue equation (See Eq. 6 of Vol. 1)

*These variables are also used in the inlet and wake turbulence programs, but are listed here only.

TABLE 3. UTILITY SUBROUTINES

ORIGINAL PAGE IS
OF POOR QUALITY

A. Subroutines common to the Mean Wake, Inlet, and Wake Turbulence programs.

1. ANRT (ANnular RoOT), ANFU (ANnular FUnction), ISIGN
Programs find the roots $\kappa_{m,n}$ of the boundary value equation for the annular duct:
$$J'_m(\kappa_{m,n} r_{duct}) Y'_m(\kappa_{m,n} r_{hub}) - J'_m(\kappa_{m,n} r_{hub}) Y'_m(\kappa_{m,n} r_{duct}) = 0$$
2. FLSJ, BESJ (BESsel functions of the first [J] and the second [i] kind)
BESJ computes the mth order Bessel function of the first kind, $J_m(x)$.
BESY computes the mth order Bessel function of the second kind, $Y_m(x)$.
An error code is returned along with each answer. The error code is:
 - ERR = 0 No error (answer is correct to given accuracy)
 - = 1 m was negative (must be ≥ 0)
 - = 2 Argument was negative (must be ≥ 0)
 - = 3 Required accuracy not obtained
 - = 4 Range of n compared to the argument was not correct (see program listing).
3. EIGEN

The program normalizes the weighting factors $A_{m,n}$ and $B_{m,n}$ used in the mode function.

$$\psi = A_{m,n} J_m + B_{m,n} Y_m.$$

The orthogonality condition is

$$\int_A \psi_{1,j} \psi_{m,n}^* dA = \begin{cases} \Gamma_{m,n} & \text{if } i = m \text{ and } j = n \\ 0 & \text{otherwise} \end{cases}$$

The normalizing condition used is that

$$\tilde{\Gamma}_{m,n} \equiv \frac{\Gamma_{m,n}}{\pi(r_{duct}^2 - r_{hub}^2)} = 1 \text{ (non-dimensional).}$$

TABLE 3. (Cont.)

4. RMODE

Program computes the radial mode shape ψ for the m, nth mode of the annular duct. (See Eq. 4 of Vol. 1)

5. KERNEL

Program computes the kernel for the Green's function formulation of the cascade routine. (See Eqs. B-25 and B-26 of Vol. 1)
Used in conjunction with PRES or CASC.

B. Subroutine used specifically for the Mean Wake Routine

1. PRES (PRESSure distribution)

The program specifies the complex pressure distribution across the stator vane chord as produced by a velocity gust. The input parameters include the gust wavenumber, the wake velocity, and the stator vane spacings.

C. Subroutines used specifically for the Inlet Turbulence Routine

1. SCALLX (SCALE Length, X direction)

Program yields the turbulence length scale in the axial direction as a function of radial position. The routine is actually a program input whereby a particular turbulence distribution is loaded.

2. SCALLR (SCALE Length, Radial direction)

Program yields the turbulence length scale in the radial direction as a function of radial position. The routine is an input parameter.

3. STHETA (Scale length, THETA direction)

Program yields the turbulence length scale in the circumferential direction as a function of radial position. The routine is an input parameter.

4. EPSD (ϵ_D)

Program yields the inlet RMS turbulence intensity as a function of radial position. The routine is an input parameter.

5. PHITHH ($\hat{\phi}_\theta$)

The program computes the Fourier transform of the correlation function in the circumferential direction. This transform is usually a fairly simple analytic function such as an exponential.

TABLE 3. (Cont.)

ORIGINAL PAGE IS
OF POOR QUALITY

6. PHIXHT ($\hat{\phi}_x$)

The program computes the Fourier transform of the correlation function in the axial direction.

D. Subroutines used for the Inlet and Wake Turbulence Routines

1. CASC (CASCade function.)

The program calculates the complex pressure distribution across a blade chord as produced by a velocity gust. The input parameters include the gust wavenumber, the wake velocity, and the blade spacings. This program is a version of PRES (listed above) specialized for use with the extended range of arguments in the turbulence routines.

E. Subroutine used specifically for the Wake Turbulence Routine

1. FHAT (\hat{f})

The program computes the Fourier transform of the modulating function for the turbulent wake. The transform is usually a simple analytic function depending on the turbulence model in use.

F. IMSL Library Subroutine called by Subroutine KERNEL

IMSL Library routine LEQTIC is called by KERNEL to solve a set of simultaneous equations. The documentation provided by IMSL follows on the next three pages.

ORIGINAL PAGE IS
OF POOR QUALITY

TABLE 3. (Cont.) DESCRIPTION OF IMSL LIBRARY ROUTINE LEQ1IC.

IMSL ROUTINE NAME	- LEQ1IC																		
PURPOSE	- LINEAR EQUATION SOLUTION - COMPLEX MATRIX - SPACE ECONOMIZER SOLUTION																		
USAGE	- CALL LEQ1IC (A,N,IA,B,M,IB,IJOB,WA,IER)																		
ARGUMENTS	<table border="0"> <tr> <td>A</td> <td>- INPUT COMPLEX N BY N MATRIX CONTAINING THE COMPLEX COEFFICIENTS OF THE EQUATION $AX = B$. ON OUTPUT, A CONTAINS THE L-U DECOMPOSITION OF A ROWWISE PERMUTATION OF THE INPUT MATRIX A.</td> </tr> <tr> <td>N</td> <td>- ORDER OF MATRIX A. (INPUT)</td> </tr> <tr> <td>IA</td> <td>- ROW DIMENSION OF MATRIX A EXACTLY AS SPECIFIED IN THE DIMENSION STATEMENT IN THE CALLING PROGRAM. (INPUT)</td> </tr> <tr> <td>B</td> <td>- INPUT COMPLEX N BY M MATRIX CONTAINING THE COMPLEX VALUED RIGHT HAND SIDES OF THE EQUATION $AX = B$. ON OUTPUT, THE SOLUTION MATRIX X REPLACES B. IF IJOB=1, B IS NOT USED.</td> </tr> <tr> <td>M</td> <td>- NUMBER OF RIGHT HAND SIDES (COLUMNS IN B). (INPUT)</td> </tr> <tr> <td>IB</td> <td>- ROW DIMENSION OF MATRIX B EXACTLY AS SPECIFIED IN THE DIMENSION STATEMENT IN THE CALLING PROGRAM. (INPUT)</td> </tr> <tr> <td>IJOB</td> <td>- INPUT OPTION PARAMETER. IJOB=1 IMPLIES WHEN I=0, FACTOR THE MATRIX AND SOLVE THE EQUATION $AX=B$. I=1, FACTOR THE MATRIX A. I=2, SOLVE THE EQUATION $AX=B$. THIS OPTION IMPLIES THAT LEQ1IC HAS ALREADY BEEN CALLED USING IJOB=0 OR 1 SO THAT THE MATRIX HAS ALREADY BEEN FACTORED. IN THIS CASE OUTPUT MATRIX A MUST HAVE BEEN SAVED FOR REUSE IN THE CALL TO LEQ1IC.</td> </tr> <tr> <td>WA</td> <td>- WORK AREA OF LENGTH N CONTAINING THE PIVOT INDICES.</td> </tr> <tr> <td>IER</td> <td>- ERROR PARAMETER. (OUTPUT) TERMINAL ERROR IER=129 INDICATES THAT MATRIX A IS ALGORITHMICALLY SINGULAR. (SEE THE CHAPTER L PRELUDE.)</td> </tr> </table>	A	- INPUT COMPLEX N BY N MATRIX CONTAINING THE COMPLEX COEFFICIENTS OF THE EQUATION $AX = B$. ON OUTPUT, A CONTAINS THE L-U DECOMPOSITION OF A ROWWISE PERMUTATION OF THE INPUT MATRIX A.	N	- ORDER OF MATRIX A. (INPUT)	IA	- ROW DIMENSION OF MATRIX A EXACTLY AS SPECIFIED IN THE DIMENSION STATEMENT IN THE CALLING PROGRAM. (INPUT)	B	- INPUT COMPLEX N BY M MATRIX CONTAINING THE COMPLEX VALUED RIGHT HAND SIDES OF THE EQUATION $AX = B$. ON OUTPUT, THE SOLUTION MATRIX X REPLACES B. IF IJOB=1, B IS NOT USED.	M	- NUMBER OF RIGHT HAND SIDES (COLUMNS IN B). (INPUT)	IB	- ROW DIMENSION OF MATRIX B EXACTLY AS SPECIFIED IN THE DIMENSION STATEMENT IN THE CALLING PROGRAM. (INPUT)	IJOB	- INPUT OPTION PARAMETER. IJOB=1 IMPLIES WHEN I=0, FACTOR THE MATRIX AND SOLVE THE EQUATION $AX=B$. I=1, FACTOR THE MATRIX A. I=2, SOLVE THE EQUATION $AX=B$. THIS OPTION IMPLIES THAT LEQ1IC HAS ALREADY BEEN CALLED USING IJOB=0 OR 1 SO THAT THE MATRIX HAS ALREADY BEEN FACTORED. IN THIS CASE OUTPUT MATRIX A MUST HAVE BEEN SAVED FOR REUSE IN THE CALL TO LEQ1IC.	WA	- WORK AREA OF LENGTH N CONTAINING THE PIVOT INDICES.	IER	- ERROR PARAMETER. (OUTPUT) TERMINAL ERROR IER=129 INDICATES THAT MATRIX A IS ALGORITHMICALLY SINGULAR. (SEE THE CHAPTER L PRELUDE.)
A	- INPUT COMPLEX N BY N MATRIX CONTAINING THE COMPLEX COEFFICIENTS OF THE EQUATION $AX = B$. ON OUTPUT, A CONTAINS THE L-U DECOMPOSITION OF A ROWWISE PERMUTATION OF THE INPUT MATRIX A.																		
N	- ORDER OF MATRIX A. (INPUT)																		
IA	- ROW DIMENSION OF MATRIX A EXACTLY AS SPECIFIED IN THE DIMENSION STATEMENT IN THE CALLING PROGRAM. (INPUT)																		
B	- INPUT COMPLEX N BY M MATRIX CONTAINING THE COMPLEX VALUED RIGHT HAND SIDES OF THE EQUATION $AX = B$. ON OUTPUT, THE SOLUTION MATRIX X REPLACES B. IF IJOB=1, B IS NOT USED.																		
M	- NUMBER OF RIGHT HAND SIDES (COLUMNS IN B). (INPUT)																		
IB	- ROW DIMENSION OF MATRIX B EXACTLY AS SPECIFIED IN THE DIMENSION STATEMENT IN THE CALLING PROGRAM. (INPUT)																		
IJOB	- INPUT OPTION PARAMETER. IJOB=1 IMPLIES WHEN I=0, FACTOR THE MATRIX AND SOLVE THE EQUATION $AX=B$. I=1, FACTOR THE MATRIX A. I=2, SOLVE THE EQUATION $AX=B$. THIS OPTION IMPLIES THAT LEQ1IC HAS ALREADY BEEN CALLED USING IJOB=0 OR 1 SO THAT THE MATRIX HAS ALREADY BEEN FACTORED. IN THIS CASE OUTPUT MATRIX A MUST HAVE BEEN SAVED FOR REUSE IN THE CALL TO LEQ1IC.																		
WA	- WORK AREA OF LENGTH N CONTAINING THE PIVOT INDICES.																		
IER	- ERROR PARAMETER. (OUTPUT) TERMINAL ERROR IER=129 INDICATES THAT MATRIX A IS ALGORITHMICALLY SINGULAR. (SEE THE CHAPTER L PRELUDE.)																		
PRECISION/HARDWARE	- SINGLE AND DOUBLE/H32 - SINGLE/H36,H48,H60																		
REQD. IMSL ROUTINES	- UERTST,UGETIO																		
NOTATION	- INFORMATION ON SPECIAL NOTATION AND CONVENTIONS IS AVAILABLE IN THE MANUAL INTRODUCTION OR THROUGH IMSL ROUTINE UHELP																		
REMARKS	<table border="0"> <tr> <td>1.</td> <td>WHEN IJOB=1, ARGUMENTS B, M AND IB ARE NOT USED BY LEQ1IC.</td> </tr> <tr> <td>2.</td> <td>INPUT MATRIX A IS DESTROYED WHEN IJOB=0 OR 1. WHEN IJOB=0 OR 2, B IS REPLACED WITH THE SOLUTION X.</td> </tr> </table>	1.	WHEN IJOB=1, ARGUMENTS B, M AND IB ARE NOT USED BY LEQ1IC.	2.	INPUT MATRIX A IS DESTROYED WHEN IJOB=0 OR 1. WHEN IJOB=0 OR 2, B IS REPLACED WITH THE SOLUTION X.														
1.	WHEN IJOB=1, ARGUMENTS B, M AND IB ARE NOT USED BY LEQ1IC.																		
2.	INPUT MATRIX A IS DESTROYED WHEN IJOB=0 OR 1. WHEN IJOB=0 OR 2, B IS REPLACED WITH THE SOLUTION X.																		

ORIGINAL PAGE IS
OF POOR QUALITY

TABLE 3. (Cont.) DESCRIPTION OF IMSL LIBRARY ROUTINE LEQTLIC.

3. LEQTLIC CAN BE USED TO COMPUTE THE INVERSE OF A COMPLEX MATRIX. THIS IS DONE BY CALLING LEQTLIC WITH M=N, B=THE N BY N IDENTITY MATRIX AND IJOB=0. WHEN N IS LARGE, IT MAY BE MORE PRACTICAL TO COMPUTE THE INVERSE A COLUMN AT A TIME. TO DO THIS, FIRST CALL LEQTLIC WITH IJOB=1 TO FACTOR A. MAKE SUCCEEDING CALLS WITH M=1, B=A COLUMN OF THE IDENTITY MATRIX AND IJOB=2. B WILL BE REPLACED BY THE CORRESPONDING COLUMN OF A INVERSE.
4. THE DETERMINANT OF A CAN BE COMPUTED AFTER LEQTLIC HAS BEEN CALLED AS FOLLOWS

```

DET = (1.0,0.0)
DO 5 I = 1,N
  IPVT = WA(I)
  IF (IPVT .NE. I) DET = -DET
  DET = DET*A(I,I)
5 CONTINUE

```

Algorithm

For a given N by N complex matrix A and an N by M complex matrix B, LEQTLIC computes an LU decomposition of a rowwise permutation of A and solves the system of equations AX=B. Row equilibration and partial pivoting are used.

See reference:

Forsythe, George and Moler, Cleve B., Computer Solution of Linear Algebraic Systems, Prentice-Hall, Inc., Englewood Cliffs, New Jersey, 1967.

Example

This example shows how to solve a system of 3 equations in 3 unknowns using LEQTLIC.

The equations are

$$\begin{aligned}
 (1.+i3.)X(1) + (2.5-i3.5)X(2) + (1.+i)X(3) &= (1.-i2.) \\
 (6.+i2.)X(1) + (-4.+i3.)X(2) &= (3.-i4.) \\
 (5.-i) X(1) + (1.+i) X(2) + (3.+i3.)X(3) &= (5.-i6.)
 \end{aligned}$$

and the unknowns are X(1), X(2), and X(3).

In this case, N=3 (A is 3 by 3), and M=1. (B is 3 by 1, one right hand side).

Input:

```

INTEGER  N,IA,M,IB,IJOB,IER
COMPLEX  A(3,3),B(3)
REAL     WA(3)
IA = 3
IB = 3
N = 3

```

ORIGINAL PAGE 13
OF POOR QUALITY

TABLE 3. (Cont.) DESCRIPTION OF IMSL LIBRARY ROUTINE LEQ1C.

A = (1.,3.) (2.5,-3.5) (1.,1.)
 (6.,2.) (-4.,3.) (0.,0.)
 (5.,-1.) (1.,1.) (3.,3.)

M = 1

B = (1.,-2.)
 (3.,-4.)
 (5.,-6.)

IJOB=0

CALL LEQ1C (A,N,IA,B,M,IB,IJOB,WA,IER)

END

Output:

IER = 0

B = (-.32881, -.68795)
 (-.48127, -.55729)
 (.90092, -1.5177)

Hence the solution is

X(1) = -.32881 -i0.68795
X(2) = -.48127 -i0.55729
X(3) = .90092 -i1.5177

TABLE 4. SAMPLE EXECUTION OF THE MEAN ROTOR WAKE PROGRAM

ORIGINAL PAGE 13
OF POOR QUALITY

NVANE=
11
NVANE= 11
NBLADE=
15
NBLADE= 15
HUB RADIUS DIVIDED BY DUCT RADIUS =
.484
SIGMAR= 0.48400000E+00
VANE TIP CHORD DIVIDED BY DUCT RADIUS =
.408
SIGNAC= 0.40800000E+00
LX0 =
.6201
LX0= 0.62010000E+00
NDAT =
7
NDAT= 7
VANE GEOMETRY MATRIX INPUT
FEED MATRIX IN ONE ROW AT A TIME, FROM HUB TO TIP
ROW= 1 R/RDUCT =
.484
C/CTIP =
1.
ALPHAS (DEGREES)=
16.3
YS/CTIP =
0.
YR/CTIP =
0.
XS/CTIP =
0.
XR/CTIP =
0.
ROW= 2 R/RDUCT =
.56
C/CTIP =
1.
ALPHAS (DEGREES)=
15.67
YS/CTIP =
.027
YR/CTIP =
-.033
XS/CTIP =
-.001
XR/CTIP =
-.02

TABLE 4. (Cont.)

ORIGINAL PAGE IS
OF POOR QUALITY

ROW= 3 R/RDUCT =
 .739
 C/CTIP =
 1.
 ALPHAS (DEGREES)=
 14.07
 YS/CTIP =
 .093
 YR/CTIP =
 -.118
 XS/CTIP =
 -.005
 XR/CTIP =
 -.057
 ROW= 4 R/RDUCT =
 .92
 C/CTIP =
 1.
 ALPHAS (DEGREES)=
 12.57
 YS/CTIP =
 .158
 YR/CTIP =
 -.213
 XS/CTIP =
 -.008
 XR/CTIP =
 -.073
 ROW= 5 R/RDUCT =
 .946
 C/CTIP =
 1.
 ALPHAS (DEGREES)=
 12.36
 YS/CTIP =
 .163
 YR/CTIP =
 -.226
 XS/CTIP =
 -.008
 XR/CTIP =
 -.07
 ROW= 6 R/RDUCT =
 .973
 C/CTIP =
 1.

TABLE 4. (Cont.)

OPTIONAL PAGE 13
OF 2000

ALPHAS (DEGREES)=

12.15

YS/CTIP =

.177

YR/CTIP =

-.242

XS/CTIP =

-.009

XR/CTIP =

-.067

ROW= 7 R/RDUCT =

1.

C/CTIP =

1.

ALPHAS (DEGREES)=

11.92

YS/CTIP =

.187

YR/CTIP =

-.262

XS/CTIP =

-.009

XR/CTIP =

-.064

VANE GEOMETRY MATRIX IS

0.484E+00	0.100E+01	0.284E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
0.560E+00	0.100E+01	0.273E+00	0.270E-01	-0.330E-01	-0.100E-02	-0.200E-01
0.739E+00	0.100E+01	0.246E+00	0.930E-01	-0.118E+00	-0.500E-02	-0.570E-01
0.920E+00	0.100E+01	0.219E+00	0.158E+00	-0.213E+00	-0.800E-02	-0.730E-01
0.946E+00	0.100E+01	0.216E+00	0.163E+00	-0.226E+00	-0.800E-02	-0.700E-01
0.973E+00	0.100E+01	0.212E+00	0.177E+00	-0.242E+00	-0.900E-02	-0.670E-01
0.100E+01	0.100E+01	0.208E+00	0.187E+00	-0.262E+00	-0.900E-02	-0.640E-01

TYPE 1 TO INPUT ROTOR FLOW VELOCITY, 0 FOR FREE VORTEX

1

IVOR= 1

NUMBER OF RADII FOR SPECIFYING MEAN ROTOR FLOW=

8

NVELO= 8

INPUT MATRIX FOR MEAN ROTOR FLOW

FEED MATRIX IN ONE ROW AT A TIME, FROM HUB TO TIP

ROW= 1 R/RDUCT=

.484

MEAN CIRCUMFERENTIAL VELOCITY RATIO=

.808

ROW= 2 R/RDUCT=

.533

TABLE 4. (Cont.)

ORIGINAL PAGE IS
OF POOR QUALITY

MEAN CIRCUMFERENTIAL VELOCITY RATIO=
.700
ROW= 3 R/RDUCT=
.612
MEAN CIRCUMFERENTIAL VELOCITY RATIO=
.784
ROW= 4 R/RDUCT=
.834
MEAN CIRCUMFERENTIAL VELOCITY RATIO=
.712
ROW= 5 R/RDUCT=
.918
MEAN CIRCUMFERENTIAL VELOCITY RATIO=
.688
ROW= 6 R/RDUCT=
.946
MEAN CIRCUMFERENTIAL VELOCITY RATIO=
.686
ROW= 7 R/RDUCT=
.974
MEAN CIRCUMFERENTIAL VELOCITY RATIO=
.713
ROW= 8 R/RDUCT=
1.
MEAN CIRCUMFERENTIAL VELOCITY RATIO=
.713
MEAN ROTOR FLOW VELOCITY MATRIX IS
.4840E+00 .8080E+00
.5330E+00 .7880E+00
.6120E+00 .7840E+00
.8340E+00 .7120E+00
.9180E+00 .6880E+00
.9460E+00 .6860E+00
.9740E+00 .7130E+00
.1000E+01 .7130E+00
MT =
.508
MT= 0.50800000E+00
MA =
.323
MA = 0.32300000E+00
WAKE WIDTH =
.172
WWIDTH= 0.17200000E+00
MAX VEL DEFICIT DIVIDED BY UBAR
.27
VELDEF= 0.27000000E+00

TABLE 4. (Cont.)

ORIGINAL PAGE IS
OF POOR QUALITY

NUMBER OF RADIAL STATIONS =
7
NRAD= 7
NUMBER OF CHORDWISE STATIONS =
8
NCHORD= 8
ACCURACY OF BESSEL FN =
.001
EB= 0.10000000E-02
ACCURACY OF CONVERGENCE TO ROOT XMN =
.0001
EC= 0.10000000E-03

S = 3
XMN(MAX) FOR PROPAGATION = 0.24154718E+02
%FRSAPR Floating underflow PC= 6115

%FRSAPR Floating underflow PC= 6163

MODE DATA

S = 3 M = 1 N = 1 XMN = 0.13709056E+01
CUTOFF RATIO FOR MODE= .1762E+02
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.15152305E+01 BMN = -0.42119466E+00
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = 1 N = 1 S = 3
ERROR CODE FROM INVERSION ROUTINE= 0
ERROR CODE FROM INVERSION ROUTINE= 0
ERROR CODE FROM INVERSION ROUTINE= 0
ERROR CODE FROM INVERSION ROUTINE= 0
ERROR CODE FROM INVERSION ROUTINE= 0
ERROR CODE FROM INVERSION ROUTINE= 0
ERROR CODE FROM INVERSION ROUTINE= 0

UPSTREAM

GAMMA M,N,SB = 0.33725477E+02
MODE AMPLITUDE = 0.13613387E-03 0.33358998E-04
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
RELATIVE SOUND POWER LEVEL FOR MODE(0B)= -0.7364E+02

DOWNSTREAM

GAMMA M,N,SB = -0.17237771E+02
MODE AMPLITUDE = -0.47378941E-04 -0.72085580E-05
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
RELATIVE SOUND POWER LEVEL FOR MODE(0B)= -0.7715E+02

TABLE 4. (Cont.)

M = -1 N = 1 S = -3

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7364E+02

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7715E+02

MODE DATA

S = 3 M = 1 N = 2 XMN = 0.63900327E+01

CUTOFF RATIO FOR MODE= .3780E+01

SUM OF BESSEL FUNCTION ERROR CODES = 0

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0

AMN = 0.19356938E+01 BMN = 0.32269858E+01

ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = 1 N = 2 S = 3

UPSTREAM

GAMMA M,N,SB = 0.32857319E+02

MODE AMPLITUDE = -0.11049067E-03 -0.91503578E-04

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7351E+02

DOWNSTREAM

GAMMA M,N,SB = -0.16369614E+02

MODE AMPLITUDE = 0.56242548E-04 0.26364856E-04

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7519E+02

M = -1 N = 2 S = -3

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7351E+02

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7519E+02

MODE DATA

S = 3 M = 1 N = 3 XMN = 0.12724612E+02

CUTOFF RATIO FOR MODE= .1960E+01

SUM OF BESSEL FUNCTION ERROR CODES = 0

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0

AMN = 0.43514410E+01 BMN = 0.30726765E+01

ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

TABLE 4. (Cont.)

ORIGINAL PAGE 13
OF POOR QUALITY

M = 1 N = 3 S = 3

UPSTREAM

GAMMA M,N,SB = 0.30194305E+02

MODE AMPLITUDE = -0.67274867E-04 -0.89817303E-06

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.8036E+02

DOWNSTREAM

GAMMA M,N,SB = -0.13706599E+02

MODE AMPLITUDE = 0.39056430E-04 0.46102940E-04

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7634E+02

M= -1 N= 3 S= -3

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.8036E+02

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7634E+02

MODE DATA

S = 3 M = 1 N = 4 XMN = 0.18362274E+02

CUTOFF RATIO FOR MODE= .1315E+01

SUM OF BESSEL FUNCTION ERROR CODES = 0

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0

AMN = 0.61381751E+01 BMN = 0.22116971E+01

ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = 1 N = 4 S = 3

UPSTREAM

GAMMA M,N,SB = 0.24825892E+02

MODE AMPLITUDE = 0.88119635E-06 0.55164443E-06

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.1173E+03

DOWNSTREAM

GAMMA M,N,SB = -0.83381859E+01

MODE AMPLITUDE = 0.10458061E-04 0.45172844E-04

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.8064E+02

TABLE 4. (Cont.)

M= -1 N= 4 S= -3

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.1173E+03

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.8064E+02

LARGEST PROPAGATING N FOR THIS M = 4

MODE DATA

S = 3 M = -10 N = 1 XMN = 0.11769701E+02
CUTOFF RATIO FOR MODE= .2052E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.54757755E+01 BMN = -0.30348594E-02
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = -10 N = 1 S = 3

UPSTREAM

GAMMA M,N,SB = 0.30531741E+02
MODE AMPLITUDE = -0.90896823E-04 0.41207877E-04
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7690E+02

DOWNSTREAM

GAMMA M,N,SB = -0.14044035E+02
MODE AMPLITUDE = -0.64741460E-03 -0.25779423E-03
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5498E+02

M= 10 N= 1 S= -3

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7690E+02

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5498E+02

MODE DATA

S = 3 M = -10 N = 2 XMN = 0.16348282E+02
CUTOFF RATIO FOR MODE= .1478E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.48044727E+01 BMN = -0.37694076E+00
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

TABLE 4. (Cont.)

ORIGINAL PAGE 13
OF POOR QUALITY

M = -10 N = 2 S = 3

UPSTREAM

GAMMA M,N,SB = 0.27032509E+02

MODE AMPLITUDE = 0.36213808E-04 0.13253067E-04

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.8559E+02

DOWNSTREAM

GAMMA M,N,SB = -0.10544803E+02

MODE AMPLITUDE = 0.54190425E-03 0.25744146E-03

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5754E+02

M = 10 N = 2 S = -3

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.8559E+02

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5754E+02

MODE DATA

S = 3 M = -10 N = 3 XMN = 0.19710760E+02

CUTOFF RATIO FOR MODE= .1225E+01

SUM OF BESSEL FUNCTION ERROR CODES = 0

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0

AMN = 0.45357506E+01 BMN = -0.21469782E+01

ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = -10 N = 3 S = 3

UPSTREAM

GAMMA M,N,SB = 0.22996575E+02

MODE AMPLITUDE = 0.50912282E-05 0.44796741E-04

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.8472E+02

DOWNSTREAM

GAMMA M,N,SB = -0.65088688E+01

MODE AMPLITUDE = -0.32015018E-03 -0.56725690E-03

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5844E+02

TABLE 4. (Cont.)

ORIGINAL PAGE IS
OF POOR QUALITY

M= 10 N= 3 S= -3

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.8492E+02

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5844E+02

MODE DATA

S = 3 M = -10 N = 4 XMN = 0.23588640E+02

CUTOFF RATIO FOR MODE= .1024E+01

SUM OF BESSEL FUNCTION ERROR CODES = 0

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0

AMN = 0.62652037E+01 BMN = -0.98372497E+00

ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0

M = -10 N = 4 S = 3

UPSTREAM

GAMMA M,N,SB = 0.13736991E+02

MODE AMPLITUDE = -0.50110748E-03 -0.29130448E-03

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.6613E+02

DOWNSTREAM

GAMMA M,N,SB = 0.27507146E+01

MODE AMPLITUDE = -0.34158767E-03 0.85520260E-03

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.6090E+02

M= 10 N= 4 S= -3

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.6613E+02

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.6090E+02

LARGEST PROPAGATING N FOR THIS M = 4

MODE DATA

S = 3 M = 12 N = 1 XMN = 0.13878611E+02

CUTOFF RATIO FOR MODE= .1740E+01

SUM OF BESSEL FUNCTION ERROR CODES = 0

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0

AMN = 0.60892918E+01 BMN = -0.63711792E-03

ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0

TABLE 4. (Cont.)

ORIGINAL PAGE 12
OF POOR QUALITY

M = 12 N = 1 S = 3

UPSTREAM

GAMMA M,N,SB = 0.25133072E+02

MODE AMPLITUDE = 0.88696711E-04 0.15987079E-05

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7808E+02

DOWNSTREAM

GAMMA M,N,SB = -0.12645367E+07

MODE AMPLITUDE = 0.95047415E-04 0.45870526E-03

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5892E+02

M= -12 N= 1 S= -3

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7808E+02

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5892E+02

MODE DATA

S = 3 M = 12 N = 2 XMN = 0.18713666E+02

CUTOFF RATIO FOR MODE= .1291E+01

SUM OF BESSEL FUNCTION ERROR CODES = 0

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0

AMN = 0.53619937E+01 BMN = -0.12842323E+00

ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0

M = 12 N = 2 S = 3

UPSTREAM

GAMMA M,N,SB = 0.24381333E+02

MODE AMPLITUDE = 0.31973551E-03 -0.67991251E-04

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.6745E+02

DOWNSTREAM

GAMMA M,N,SB = -0.78936267E+01

MODE AMPLITUDE = 0.14232207E-03 -0.40642054E-03

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.6146E+02

TABLE 4. (Cont.)

ORIGINAL PAGE IS
OF POOR QUALITY

M= -12 N= 2 S= -3

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.6745E+02

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.6146E+02

MODE DATA

S = 3 M = 12 N = 3 XMN = 0.22297030E+02

CUTOFF RATIO FOR MODE= .1083E+01

SUM OF BESSEL FUNCTION ERROR CODES = 0

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0

AMN = 0.50662141E+01 BMN = -0.14574338E+01

ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = 12 N = 3 S = 3

UPSTREAM

GAMMA M,N,SB = 0.18059368E+02

MODE AMPLITUDE = -0.38293325E-03 -0.15805489E-03

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.6696E+02

DOWNSTREAM

GAMMA M,N,SB = -0.15716621E+01

MODE AMPLITUDE = -0.11038813E-02 0.41711175E-03

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5569E+02

M= -12 N= 3 S= -3

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.6696E+02

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5569E+02

LARGEST PROPAGATING N FOR THIS M = 3

MODE DATA

S = 3 M = -21 N = 1 XMN = 0.23254819E+02

CUTOFF RATIO FOR MODE= .1039E+01

SUM OF BESSEL FUNCTION ERROR CODES = 0

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0

AMN = 0.85042393E+01 BMN = -0.38116337E-05

ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

TABLE 4. (Cont.)

M = -21 N = 1 S = 3

UPSTREAM

GAMMA M,N,SB = 0.15145542E+02
MODE AMPLITUDE = 0.63165623E-03 -0.10433352E-02
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5882E+02

DOWNSTREAM

GAMMA M,N,SB = 0.13421642E+01
MODE AMPLITUDE = -0.18827030E-02 0.30355092E-02
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.4796E+02

M= 21 N= 1 S= -3

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5882E+02

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.4796E+02

LARGEST PROPAGATING N FOR THIS M = 1
NO MORE PROPAGATING MODES FOR THIS VALUE OF S

S = 2
XMN(MAX) FOR PROPAGATION = 0.16103146E+02

MODE DATA

S = 2 M = -3 N = 1 XMN = 0.39866274E+01
CUTOFF RATIO FOR MODE= .4039E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.26023450E+01 BMN = -0.32589376E+00
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = -3 N = 1 S = 2
ERROR CODE FROM INVERSION ROUTINE= 0
ERROR CODE FROM INVERSION ROUTINE= 0
ERROR CODE FROM INVERSION ROUTINE= 0
ERROR CODE FROM INVERSION ROUTINE= 0
ERROR CODE FROM INVERSION ROUTINE= 0
ERROR CODE FROM INVERSION ROUTINE= 0
ERROR CODE FROM INVERSION ROUTINE= 0

TABLE 4. (Cont.)

ORIGINAL PAGE IS
OF POOR QUALITY

UPSTREAM

GAMMA M,N,SB = 0.21981403E+02

MODE AMPLITUDE = 0.13526694E-03 -0.11438489E-03

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7167E+02

DOWNSTREAM

GAMMA M,N,SB = -0.10989599E+02

MODE AMPLITUDE = -0.12497451E-04 -0.25469007E-03

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.6288E+02

M= 3 N= 1 S= -2

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7167E+02

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.6288E+02

MODE DATA

S = 2 M = -3 N = 2 XMN = 0.77467003E+01

CUTOFF RATIO FOR MODE= .2079E+01

SUM OF BESSEL FUNCTION ERROR CODES = 0

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0

AMN = 0.35705322E+01 BMN = -0.89511162E+00

ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = -3 N = 2 S = 2

UPSTREAM

GAMMA M,N,SB = 0.20412827E+02

MODE AMPLITUDE = -0.62938154E-04 0.18019367E-03

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7126E+02

DOWNSTREAM

GAMMA M,N,SB = -0.94210234E+01

MODE AMPLITUDE = -0.56493354E-03 0.30607513E-03

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5566E+02

TABLE 4. (Cont.)

M= 3 N= 2 S= -2

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7126E+02

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5566E+02

MODE DATA

S = 2 M = -3 N = 3 XMN = 0.13008803E+02
CUTOFF RATIO FOR MODE= .1238E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = -0.18754296E+00 BMN = 0.53089865E+01
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = -3 N = 3 S = 2

UPSTREAM

GAMMA M,N,SB = 0.15524623E+02
MODE AMPLITUDE = -0.87384578E-05 -0.13593062E-03
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7526E+02

DOWNSTREAM

GAMMA M,N,SB = -0.45328195E+01
MODE AMPLITUDE = 0.50005592E-03 0.24067449E-03
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5971E+02

M= 3 N= 3 S= -2

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7526E+02

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5971E+02

LARGEST PROPAGATING N FOR THIS M = 3

MODE DATA

S = 2 M = 8 N = 1 XMN = 0.96413107E+01
CUTOFF RATIO FOR MODE= .1670E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.48101923E+01 BMN = -0.14625735E-01
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

TABLE 4. (Cont.)

ORIGINAL PAGE IS
OF POOR QUALITY

M = 8 N = 1 S = 2

UPSTREAM

GAMMA M,N,SB = 0.19124322E+02

MODE AMPLITUDE = -0.15710355E-02 0.39986281E-02

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.4444E+02

DOWNSTREAM

GAMMA M,N,SB = -0.81325179E+01

MODE AMPLITUDE = 0.66897707E-03 -0.60581600E-04

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5598E+02

M = -8 N = 1 S = -2

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.4444E+02

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5598E+02

MODE DATA

S = 2 M = 8 N = 2 XMN = 0.13862791E+02

CUTOFF RATIO FOR MODE= .1162E+01

SUM OF BESSEL FUNCTION ERROR CODES = 0

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0

AMN = 0.41234860E+01 BMN = -0.85984376E+00

ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = 8 N = 2 S = 2

UPSTREAM

GAMMA M,N,SB = 0.14153511E+02

MODE AMPLITUDE = -0.50227789E-02 -0.46086625E-02

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.4172E+02

DOWNSTREAM

GAMMA M,N,SB = -0.31617076E+01

MODE AMPLITUDE = -0.18333959E-02 -0.37698765E-03

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5006E+02

TABLE 4. (Cont.)

ORIGINAL PAGE IS
OF POOR QUALITY

M= -8 N= 2 S= -2

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.4172E+02

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5006E+02

LARGEST PROPAGATING N FOR THIS M = 2

MODE DATA

S = 2 M = -14 N = 1 XMN = 0.15975402E+02

CUTOFF RATIO FOR MODE= .1008E+01

SUM OF BESSEL FUNCTION ERROR CODES = 0

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0

AMN = 0.66675895E+01 BMN = -0.10554324E-03

ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = -14 N = 1 S = 2

UPSTREAM

GAMMA M,N,SB = 0.76348570E+01

MODE AMPLITUDE = -0.15299872E-01 0.33717128E-01

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.3212E+02

DOWNSTREAM

GAMMA M,N,SB = 0.33569469E+01

MODE AMPLITUDE = 0.13580878E-01 0.28533771E-01

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.3279E+02

M= 14 N= 1 S= -2

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.3212E+02

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.3279E+02

LARGEST PROPAGATING N FOR THIS M = 1

NO MORE PROPAGATING MODES FOR THIS VALUE OF S

S = 1

XMN(MAX) FOR PROPAGATION = 0.80515728E+01

TABLE 4. (Cont.)

ORIGINAL PAGE 13
OF POOR QUALITY

MODE DATA

S = 1 M = 4 N = 1 XMN = 0.51995376E+01
 CUTOFF RATIO FOR MODE = .1549E+01
 SUM OF BESSEL FUNCTION ERROR CODES = 0
 ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
 AMN = 0.31336383E+01 BMN = -0.20930871E+00
 ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = 4 N = 1 S = 1
 ERROR CODE FROM INVERSION ROUTINE = 0
 ERROR CODE FROM INVERSION ROUTINE = 0
 ERROR CODE FROM INVERSION ROUTINE = 0
 ERROR CODE FROM INVERSION ROUTINE = 0
 ERROR CODE FROM INVERSION ROUTINE = 0
 ERROR CODE FROM INVERSION ROUTINE = 0
 ERROR CODE FROM INVERSION ROUTINE = 0

UPSTREAM
 GAMMA M,N,SB = 0.92437007E+01
 MODE AMPLITUDE = -0.16022921E-01 -0.12244703E-01
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
 RELATIVE SOUND POWER LEVEL FOR MODE(DB) = -0.3113E+02

DOWNSTREAM
 GAMMA M,N,SB = -0.37477989E+01
 MODE AMPLITUDE = -0.10714520E-02 0.23857642E-02
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
 RELATIVE SOUND POWER LEVEL FOR MODE(DB) = -0.4450E+02

M = -4 N = 1 S = -1

UPSTREAM
 RELATIVE SOUND POWER LEVEL FOR MODE(DB) = -0.3113E+02

DOWNSTREAM
 RELATIVE SOUND POWER LEVEL FOR MODE(DB) = -0.4450E+02

LARGEST PROPAGATING N FOR THIS M = 1
 NO MORE PROPAGATING MODES FOR THIS VALUE OF S
 PROBLEM COMPLETED

RELATIVE POWER LEVEL UPSTREAM S = 1	-0.2812E+02
RELATIVE POWER LEVEL UPSTREAM S = 2	-0.2843E+02
RELATIVE POWER LEVEL UPSTREAM S = 3	-0.5381E+02
RELATIVE POWER LEVEL DOWNSTREAM S = 1	-0.4149E+02
RELATIVE POWER LEVEL DOWNSTREAM S = 2	-0.2964E+02
RELATIVE POWER LEVEL DOWNSTREAM S = 3	-0.4253E+02

STOP

END OF EXECUTION
 CPU TIME: 4:39.68 ELAPSED TIME: 20:51.21
 EXIT.

TABLE 5. INPUT/OUTPUT DATA FOR THE INLET TURBULENCE PROGRAMS

This program calculates the modal power spectral density for noise generated by a turbofan rotor subjected to inlet turbulence. All input and output data are nondimensional. The input variables are defined in order to parallel as closely as possible the variables used in the Mean Wake Program. The input data consist of geometric, performance, turbulence, and computational parameters.

A. Geometric Data

	FORTRAN NAME	SYMBOL	VARIABLE	FORTRAN VARIABLE TYPE
1.	NBLADE	B	No. of rotor blades	Integer
2.	SIGMAR	σ_r	Ratio of hub radius to duct radius	Floating Point
3.	SIGMAC	σ_c	Ratio of tip chord of rotor blade to duct radius	Floating Point
4.			Vector of data for a number, NDAT (an integer variable) of rotor blade radii	
a.	R	\bar{r}	Nondimensional radius = r/r_{duct}	Floating Point
b.	C	\bar{c}	Nondimensional blade chord = c/c_{tip}	Floating Point
c.	CHI	X	Blade angle (degrees) [See Fig. 3 of Vol. 1]	Floating Point

B. Performance Data

	FORTRAN NAME	SYMBOL	VARIABLE	FORTRAN VARIABLE TYPE
1.	MT	M_t	Tip Mach number	Floating Point
2.	MA	M	Axial flow Mach number	Floating Point
3.			Frequency range data: Pressure distributions are calculated and stored for the range of frequencies from PSTART to PEND in steps of PSTEP. These data are interpolated for calculations at the frequency of interest OMEGA.	

TABLE 5. (Cont.)

ORIGINAL PAGE IS
OF POOR QUALITY

	FORTRAN NAME	SYMBOL	VARIABLE	FORTRAN VARIABLE TYPE
a.	PSTART	-	First frequency for pressure calculation. Must be an integer multiple of shaft frequency. (Usually = NBLADE)	Integer
b.	PEND	-	Final frequency for pressure calculation. See text for description of value required.	Integer
c.	PSTEP	-	Frequency step size in pressure calculation. (Usually = NBLADE)	Integer
d.	OMEGA	ω/Ω	Noise frequency of interest (nondimensionalized on the rotor shaft frequency)	Floating Point

C. Turbulence Data

The inlet turbulence data are loaded into separate function subroutines. This arrangement allows rather complicated radial distributions of turbulence to be modeled.

	FORTRAN FUNCTION NAME	SYMBOL	VARIABLE
1.	SCALLX	$\tilde{L}_x(\tilde{r})$	Axial turbulence length scale (nondimensionalized on the duct radius) as a function of nondimensionalized radius.*
2.	SCALLR	$\tilde{L}_r(\tilde{r})$	Radial turbulence length scale (nondimensionalized on the duct radius) as a function of nondimensionalized radius.
3.	STHETA	$\tilde{L}_\theta(\tilde{r})$	Circumferential turbulence length scale (nondimensionalized on the duct radius) as a function of nondimensionalized radius.*
4.	EPSD	$\epsilon_D(\tilde{r})$	RMS turbulence velocity (nondimensionalized on the mean axial velocity) as a function of nondimensionalized radius. (See Eq. 94 of Vol. 1)

*See page 48 of Vol. 1.

TABLE 5. (Cont.)

ORIGINAL PAGE IS
OF POOR QUALITY

D. Computational Data

These data set the number of integration stations in the chordwise and spanwise directions (and, indirectly, the accuracy of the results). The required accuracy for the Bessel functions used in the mode shape and eigenvalue routines are also specified.

	FORTRAN NAME	VARIABLE	FORTRAN VARIABLE TYPE
1.	NRAD	No. of radial stations at which pressure distributions are calculated (odd number)	Integer
2.	NRADNU	No. of integration stations in the chordwise direction (odd number)	Integer
3.	NCHORD	No. of integration stations in the chordwise direction (even number)	Integer
4.	EB	Absolute accuracy of all Bessel function calculations	Floating Point
5.	EC	Absolute accuracy of convergence to annular root for boundary value problem	Floating Point

Program Output

The output consists of the *relative* power spectral density for each propagating mode and for the sum of all propagating modes at the frequency of interest. The output is given in terms of the nondimensional quantity

$$10 \log_{10} \left[\frac{S_{mn}}{\rho_0 c_0^2 r_{\text{duct}}^3} \right]$$

where S_{mn} is the spectral density (watt/Hz), ρ_0 is the ambient air density, c_0 is the small-signal speed of sound and r_{duct} is the (dimensional) duct radius. To recover the conventional spectral density (dB re 10^{-12} watt/Hz) one must add

$$10 \log_{10} \left[\frac{\rho_0 c_0^2 r_{\text{duct}}^3}{10^{-12} \text{ watt}} \right]$$

to the output of the program. This step is required because all computations performed in the program are nondimensional with absolute values of ρ_0 , c_0 , and r_{duct} unknown.

TABLE 6. IMPORTANT INTERNAL VARIABLES FOR THE INLET TURBULENCE PROGRAM

(Used in addition to INPUT/OUTPUT Variables)

FORTTRAN NAME	SYMBOL	VARIABLE
BJ(N) ⁺	$J_N(X)$	Nth order Bessel function of the first kind
CASCET ⁺	$\Delta\bar{p}$	Stored values of the chordwise pressure distribution
H ⁺	-	Vector length of blade spacing between corresponding points on any two neighboring blades (See Fig. B.1)
KB ⁺	-	Nondimensional gust wave number $[=M_t b \sigma_c (\frac{\omega}{\Omega} - m)/M_r]$
LR ⁺	$\tilde{L}_r(\bar{r})$	Ratio of radial turbulence length scale to duct radius
LTHETA	$\tilde{L}_\theta(\bar{r})$	Ratio of circumferential turbulence length scale to duct radius
LX ⁺	$\tilde{L}_x(\bar{r})$	Ratio of axial turbulence length scale to duct radius
OMEGA ⁺	ω/Ω	Ratio of noise frequency to rotor shaft frequency
OMEGBC ⁺	-	Nondimensional acoustic wavenumber for reduced frequency $[=M_t \sigma_c b (\frac{\omega}{\Omega} - m)]$
PHIARG ⁺	-	Argument of $\hat{\phi}_x$ (Argument)
PMNS	-	Sum of terms comprising the radial integral
QMNS	-	Sum of terms comprising the chordwise integral
RELPR ⁺	-	Relative modal power spectral density level at a given frequency
RELPR ⁺ or SPWR ⁺	-	Relative modal power spectral density at given frequency
RRRS ⁺	R_s	Weighting factor for Bessel-type integration in chordwise direction
SIGMA ⁺	σ	Interblade phase angle (See page 52 of Vol. 1)
THEARG ⁺	-	Argument of $\hat{\phi}_\theta$ (Argument)
WHT ⁺	-	Weighting factor for Simpson integration in radial direction

*These variables are also used in the wake turbulence routine, but are listed here only.

TABLE 7. SAMPLE EXECUTION OF THE INLET TURBULENCE DATA
STORAGE ROUTINE

@ROTORS
 NBLADE=
 15
 NBLADE= 15
 HUB RADIUS DIVIDED BY DUCT RADIUS =
 .46
 SIGNAR= 0.46000000E+00
 BLADE TIP CHORD DIVIDED BY DUCT RADIUS=
 .374
 SIGNAC= 0.37400000E+00
 NDAT =
 10
 NDAT= 10
 BLADE GEOMETRY MATRIX INPUT
 FEED MATRIX IN ONE ROW AT A TIME, FROM HUB TO TIP
 ROW= 1 R/RDUCT =
 .46
 C/CTIP =
 .628
 CHI (DEGREES)=
 5.61
 ROW= 2 R/RDUCT =
 .514
 C/CTIP =
 .662
 CHI (DEGREES)=
 9.73
 ROW= 3 R/RDUCT =
 .541
 C/CTIP =
 .68
 CHI (DEGREES)=
 11.74
 ROW= 4 R/RDUCT =
 .622
 C/CTIP =
 .735
 CHI (DEGREES)=
 17.48
 ROW= 5 R/RDUCT =
 .73
 C/CTIP =
 .811
 CHI (DEGREES)=
 24.22
 ROW= 6 R/RDUCT =
 .838

ORIGINAL PAGE
 OF POOR QUALITY

ORIGINAL PAGE IS
OF POOR QUALITY

TABLE 7. (Cont.)

C/CTIP =
.887
CHI (DEGREES)=
30.66
ROW= 7 R/RDUCT =
.919
C/CTIP =
.945
CHI (DEGREES)=
35.44
ROW= 8 R/RDUCT =
.946
C/CTIP =
.959
CHI (DEGREES)=
37.05
ROW= 9 R/RDUCT =
.973
C/CTIP =
.976
CHI (DEGREES)=
38.96
ROW= 10 R/RDUCT =
1.
C/CTIP =
1.
CHI (DEGREES)=
41.14

BLADE GEOMETRY MATRIX IS

0.460E+00	0.628E+00	0.979E-01
0.514E+00	0.662E+00	0.170E+00
0.541E+00	0.680E+00	0.205E+00
0.622E+00	0.735E+00	0.305E+00
0.730E+00	0.811E+00	0.423E+00
0.838E+00	0.887E+00	0.535E+00
0.919E+00	0.945E+00	0.619E+00
0.946E+00	0.959E+00	0.647E+00
0.973E+00	0.976E+00	0.680E+00
1.100E+01	0.100E+01	0.718E+00

MT =

.508

MT= 0.50800000E+00

MA =

.323

MA = 0.32300000E+00

NUMBER OF RADIAL STATIONS =

5

NRAD= 5

ORIGINAL PAGE IS
OF POOR QUALITY

TABLE 7. (Cont.)

NUMBER OF CHORDWISE STATIONS =
8
NCHORD= 8
START FREQUENCY(HARMONIC NO. OF SHAFT) =
15
PSTART= 15
END FREQUENCY(HARMONIC NO. OF SHAFT) =
75
P END= 75
FREQUENCY STEP SIZE (HARMONIC ORDERS) =
15
PSTEP= 15
ENTER TITLE FOR DATA FILE(MAX 72 CHARACTERS)
NASA ROTOR 55,NCHORD=8,NRAD=580Z DESIGN SPEED/9-25-9\980
ERROR CODE FROM INVERSION ROUTINE= 0

*(Note: Edited for brevity -- Error Code
repeated for 375 inversions.)*

ERROR CODE FROM INVERSION ROUTINE= 0
STOP

END OF EXECUTION
CPU TIME: 52:32.72 ELAPSED TIME: 1:32:28.46
EXIT.

TABLE 8. SAMPLE EXECUTION OF THE INLET TURBULENCE NOISE
CALCULATION

@INSRCH

USER-ASSIGNED TITLE OF DATA SET FROM FILE "ROTO" IS
NASA ROTOR 55, NCHORD=8, NRAD=580% DESIGN SPEED/9-25-80
NOISE FREQUENCY/SHAFT FREQUENCY=
15.

OMEGA= .1500E+02

NUMBER OF RADIAL POSITIONS FOR ACOUSTIC COMP.=

7

NRADNU= 7

ACCURACY OF BESSEL FNS=

.001

EB= .1000E-02

ACCURACY OF CONVERGENCE TO ROOT XMN=

.0001

EC= .1000E-03

XMN(MAX) FOR PROPAGATION = 0.80515728E+01

*WARNING: This sample is for
illustration purposes only.
The input data for this
execution did not correspond
with Table 7 above.*

MODE DATA

OMEGA= .1500E+02 M= 0 N= 1 XMN= .0000E+00

PLANE WAVE MODE: CUTOFF RATIO IS + INFINITE

SUM OF BESSEL FUNCTION ERROR CODES = 0

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0

AMN = 0.10000000E+01 BMN = 0.00000000E+00

ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= 0 N= 1 OMEGA= .1500E+02

UPSTREAM

GAMMA M,N,SB = 0.11255539E+02

REL. MODAL SOUND POWER SPECTRAL DENSITY=-.2031E-08

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

SUM OF ALL ERRORS IN RS CALCULATIONS= 0

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8692E+02

DOWNSTREAM

GAMMA M,N,SB = -0.57596368E+01

REL. MODAL SOUND POWER SPECTRAL DENSITY= .4316E-08

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

SUM OF ALL ERRORS IN RS CALCULATIONS= 0

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8365E+02

MODE DATA

OMEGA= .1500E+02 M= 0 N= 2 XMN= .5944E+01

CUTOFF RATIO FOR MODE= .1354E+01

SUM OF BESSEL FUNCTION ERROR CODES = 0

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0

AMN = -0.17828589E+01 BMN = 0.31951480E+01

ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

TABLE 8. (Cont.)

M= 0 N= 2 OMEGA= .1500E+02

UPSTREAM

GAMMA M,N,SB = 0.84861763E+01
REL. MODAL SOUND POWER SPECTRAL DENSITY=-.4482E-08
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
SUM OF ALL ERRORS IN RS CALCULATIONS= 0
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8349E+02

DOWNSTREAM

GAMMA M,N,SB = -0.29907743E+01
REL. MODAL SOUND POWER SPECTRAL DENSITY= .2133E-08
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
SUM OF ALL ERRORS IN RS CALCULATIONS= 0
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8671E+02

LARGEST PROPAGATING N FOR THIS M = 2

ZFRSAPR Floating underflow PC= 17366

ZFRSAPR Floating underflow PC= 17433

MODE DATA

OMEGA= .1500E+02 M= 1 N= 1 XMN= .1396E+01
CUTOFF RATIO FOR MODE= .5769E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.15347161E+01 BMN = -0.40872429E+00
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= 1 N= 1 OMEGA= .1500E+02

UPSTREAM

GAMMA M,N,SB = 0.11126733E+02
REL. MODAL SOUND POWER SPECTRAL DENSITY=-.2481E-07
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
SUM OF ALL ERRORS IN RS CALCULATIONS= 0
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.7458E+02

DOWNSTREAM

GAMMA M,N,SB = -0.56308314E+01
REL. MODAL SOUND POWER SPECTRAL DENSITY= .6363E-07
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
SUM OF ALL ERRORS IN RS CALCULATIONS= 0
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.7196E+02

TABLE 8. (Cont.)

ORIGINAL PAGE IS
OF POOR QUALITY

M= -1 N= 1 OMEGA= .1500E+02

M= -1 N= 1 OMEGA= .1500E+02

UPSTREAM

GAMMA M,N,SB = 0.11126733E+02

REL. MODAL SOUND POWER SPECTRAL DENSITY=-.1139E-09

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

SUM OF ALL ERRORS IN RS CALCULATIONS= 0

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9943E+02

DOWNSTREAM

GAMMA M,N,SB = -0.56308314E+01

REL. MODAL SOUND POWER SPECTRAL DENSITY= .2030E-09

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

SUM OF ALL ERRORS IN RS CALCULATIONS= 0

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9492E+02

MODE DATA

OMEGA= .1500E+02 M= 1 N= 2 XMN= .6150E+01

CUTOFF RATIO FOR MODE= .1309E+01

SUM OF BESSEL FUNCTION ERROR CODES = 0

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0

AMN = 0.25524893E+01 BMN = 0.26060464E+01

ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= 1 N= 2 OMEGA= .1500E+02

UPSTREAM

GAMMA M,N,SB = 0.82391651E+01

REL. MODAL SOUND POWER SPECTRAL DENSITY=-.5133E-07

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

SUM OF ALL ERRORS IN RS CALCULATIONS= 0

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.7290E+02

DOWNSTREAM

GAMMA M,N,SB = -0.27432631E+01

REL. MODAL SOUND POWER SPECTRAL DENSITY= .3747E-07

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

SUM OF ALL ERRORS IN RS CALCULATIONS= 0

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.7426E+02

M= -1 N= 2 OMEGA= .1500E+02

M= -1 N= 2 OMEGA= .1500E+02

TABLE 8. (Cont.)

ORIGINAL PAGE 13
OF POOR QUALITY

UPSTREAM

GAMMA M,N,SB = 0.82391651E+01
REL. MODAL SOUND POWER SPECTRAL DENSITY=-.3109E-09
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
SUM OF ALL ERRORS IN RS CALCULATIONS= 0
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9507E+02

DOWNSTREAM

GAMMA M,N,SB = -0.27432631E+01
REL. MODAL SOUND POWER SPECTRAL DENSITY= .4165E-10
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
SUM OF ALL ERRORS IN RS CALCULATIONS= 0
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1038E+03

LARGEST PROPAGATING N FOR THIS M = 2

MODE DATA

OMEGA= .1500E+02 M= 2 N= 1 XMN= .2748E+01
CUTOFF RATIO FOR MODE= .2930E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.21049825E+01 BMN = -0.38973734E+00
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= 2 N= 1 OMEGA= .1500E+02

UPSTREAM

GAMMA M,N,SB = 0.10714435E+02
REL. MODAL SOUND POWER SPECTRAL DENSITY=-.2065E-06
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
SUM OF ALL ERRORS IN RS CALCULATIONS= 0
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.66E5E+02

DOWNSTREAM

GAMMA M,N,SB = -0.52489328E+01
REL. MODAL SOUND POWER SPECTRAL DENSITY= .7372E-06
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
SUM OF ALL ERRORS IN RS CALCULATIONS= 0
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.6132E+02

M= -2 N= 1 OMEGA= .1500E+02

M= -2 N= 1 OMEGA= .1500E+02

TABLE 8. (Cont.)

ORIGINAL PAGE IS
OF POOR QUALITY

UPSTREAM

GAMMA M,N,SB = 0.10744835E+02
 REL. MODAL SOUND POWER SPECTRAL DENSITY=-.7070E-11
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1115E+03

DOWNSTREAM

GAMMA M,N,SB = -0.52489328E+01
 REL. MODAL SOUND POWER SPECTRAL DENSITY= .6529E-11
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1119E+03

MODE DATA

OMEGA= .1500E+02 M= 2 N= 2 XMN= .6738E+01
 CUTOFF RATIO FOR MODE= .1195E+01
 SUM OF BESSEL FUNCTION ERROR CODES = 0
 ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
 AMN = 0.36099485E+01 BMN = 0.11001426E+01
 ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= 2 N= 2 OMEGA= .1500E+02

UPSTREAM

GAMMA M,N,SB = 0.74045386E+01
 REL. MODAL SOUND POWER SPECTRAL DENSITY=-.1927E-06
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.6715E+02

DOWNSTREAM

GAMMA M,N,SB = -0.19086367E+01
 REL. MODAL SOUND POWER SPECTRAL DENSITY= .3230E-06
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.6491E+02

M= -2 N= 2 OMEGA= .1500E+02

M= -2 N= 2 OMEGA= .1500E+02

UPSTREAM

GAMMA M,N,SB = 0.74045386E+01
 REL. MODAL SOUND POWER SPECTRAL DENSITY=-.2280E-10
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1064E+03

DOWNSTREAM

GAMMA M,N,SB = -0.19086367E+01
 REL. MODAL SOUND POWER SPECTRAL DENSITY= .2400E-12
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1262E+03

LARGEST PROPAGATING N FOR THIS M = 2

TABLE 8. (Cont.)

ORIGINAL PAGE IS
OF POOR QUALITY

MODE DATA

OMEGA= .1500E+02 M= 3 N= 1 XMN= .4027E+01
 CUTOFF RATIO FOR MODE= .2000E+01
 SUM OF BESSEL FUNCTION ERROR CODES = 0
 ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
 AMN = 0.26815693E+01 BMN = -0.27568805E+00
 ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= 3 N= 1 OMEGA= .1500E+02

UPSTREAM

GAMMA M,N,SB = 0.10115297E+02
 REL. MODAL SOUND POWER SPECTRAL DENSITY= -.8401E-06
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)= -.6076E+02

DOWNSTREAM

GAMMA M,N,SB = -0.46193948E+01
 REL. MODAL SOUND POWER SPECTRAL DENSITY= .7621E-05
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)= -5118E+02

M= -3 N= 1 OMEGA= .1500E+02

M= -3 N= 1 OMEGA= .1500E+02

UPSTREAM

GAMMA M,N,SB = 0.10115297E+02
 REL. MODAL SOUND POWER SPECTRAL DENSITY= -.5393E-12
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)= -.1227E+03

DOWNSTREAM

GAMMA M,N,SB = -0.46193948E+01
 REL. MODAL SOUND POWER SPECTRAL DENSITY= .6330E-13
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)= -.1320E+03

MODE DATA

OMEGA= .1500E+02 M= 3 N= 2 XMN= .7642E+01
 CUTOFF RATIO FOR MODE= .1054E+01
 SUM OF BESSEL FUNCTION ERROR CODES = 0
 ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
 AMN = 0.33544744E+01 BMN = -0.11908489E+01
 ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

TABLE 8. (Cont.)

ORIGINAL PAGE IS
OF POOR QUALITY

M= 3 N= 2 OMEGA= .1500E+02

UPSTREAM

GAMMA M,N,SB = 0.54275270E+01

REL. MODAL SOUND POWER SPECTRAL DENSITY=-.2364E-06

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

SUM OF ALL ERRORS IN RS CALCULATIONS= 0

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.6626E+02

DOWNSTREAM

GAMMA M,N,SB = 0.68375036E-01

REL. MODAL SOUND POWER SPECTRAL DENSITY= .1706E-05

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

SUM OF ALL ERRORS IN RS CALCULATIONS= 0

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.5768E+02

M= -3 N= 2 OMEGA= .1500E+02

M= -3 N= 2 OMEGA= .1500E+02

UPSTREAM

GAMMA M,N,SB = 0.54275270E+01

REL. MODAL SOUND POWER SPECTRAL DENSITY=-.2331E-11

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

SUM OF ALL ERRORS IN RS CALCULATIONS= 0

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1163E+03

DOWNSTREAM

GAMMA M,N,SB = 0.68375036E-01

REL. MODAL SOUND POWER SPECTRAL DENSITY= .9788E-12

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

SUM OF ALL ERRORS IN RS CALCULATIONS= 0

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1201E+03

LARGEST PROPAGATING N FOR THIS M = 2

MODE DATA

OMEGA= .1500E+02 M= 4 N= 1 XMN= .5230E+01

CUTOFF RATIO FOR MODE= .1539E+01

SUM OF BESSEL FUNCTION ERROR CODES = 0

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0

AMN = 0.32237284E+01 BNN = -0.16030403E+00

ERROR CODE FOR BESSEL FNS IN AMN AND BNN CALC = 0 0 0 0 0 0 0 0

M= 4 N= 1 OMEGA= .1500E+02

TABLE 8. (Cont.)

ORIGINAL PAGE 13
OF POOR QUALITY

UPSTREAM

GAMMA M,N,SB = 0.92161443E+01
 REL. MODAL SOUND POWER SPECTRAL DENSITY = -.2038E-05
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
 SUM OF ALL ERRORS IN RS CALCULATIONS = 0
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB) = -.5691E+02

DOWNSTREAM

GAMMA M,N,SB = -0.37202422E+01
 REL. MODAL SOUND POWER SPECTRAL DENSITY = .6538E-04
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
 SUM OF ALL ERRORS IN RS CALCULATIONS = 0
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB) = -.4185E+02

M = -4 N = 1 OMEGA = .1500E+02

M = -4 N = 1 OMEGA = .1500E+02

UPSTREAM

GAMMA M,N,SB = 0.92161443E+01
 REL. MODAL SOUND POWER SPECTRAL DENSITY = -.5114E-13
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
 SUM OF ALL ERRORS IN RS CALCULATIONS = 0
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB) = -.1329E+03

DOWNSTREAM

GAMMA M,N,SB = -0.37202422E+01
 REL. MODAL SOUND POWER SPECTRAL DENSITY = .3263E-14
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
 SUM OF ALL ERRORS IN RS CALCULATIONS = 0
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB) = -.1449E+03

LARGEST PROPAGATING N FOR THIS M = 1

MODE DATA

OMEGA = .1500E+02 M = 5 N = 1 XMN = .6376E+01
 CUTOFF RATIO FOR MODE = .1263E+01
 SUM OF BESSEL FUNCTION ERROR CODES = 0
 ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
 AMN = 0.37079083E+01 BMN = -0.81471940E-01
 ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = 5 N = 1 OMEGA = .1500E+02

UPSTREAM

GAMMA M,N,SB = 0.79436739E+01
 REL. MODAL SOUND POWER SPECTRAL DENSITY = -.1669E-05
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
 SUM OF ALL ERRORS IN RS CALCULATIONS = 0
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB) = -.5778E+02

TABLE 8. (Cont.)

ORIGINAL PAGE IS
OF POOR QUALITY

DOWNSTREAM

GAMMA M,N,SB = -0.24477719E+01
 REL. MODAL SOUND POWER SPECTRAL DENSITY= .4521E-03
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.3345E+02

M= -5 N= 1 OMEGA= .1500E+02

M= -5 N= 1 OMEGA= .1500E+02

UPSTREAM

GAMMA M,N,SB = 0.79436739E+01
 REL. MODAL SOUND POWER SPECTRAL DENSITY=-.4608E-14
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1434E+03

DOWNSTREAM

GAMMA M,N,SB = -0.24477719E+01
 REL. MODAL SOUND POWER SPECTRAL DENSITY= .1763E-14
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1475E+03

LARGEST PROPAGATING N FOR THIS M = 1

MODE DATA

OMEGA= .1500E+02 M= 6 N= 1 XMN= .7484E+01
 CUTOFF RATIO FOR MODE= .1076E+01
 SUM OF BESSEL FUNCTION ERROR CODES = 0
 ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
 AMN = 0.41370714E+01 BMN = -0.38730478E-01
 ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= 6 N= 1 OMEGA= .1500E+02

UPSTREAM

GAMMA M,N,SB = 0.58865744E+01
 REL. MODAL SOUND POWER SPECTRAL DENSITY=-.4244E-04
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.4372E+02

DOWNSTREAM

GAMMA M,N,SB = -0.39067242E+00
 REL. MODAL SOUND POWER SPECTRAL DENSITY= .2657E-02
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.2576E+02

TABLE 8. (Cont.)

ORIGINAL PAGE 13
OF POOR QUALITY

M= -6 N= 1 OMEGA= .1500E+02

M= -6 N= 1 OMEGA= .1500E+02

UPSTREAM

GAMMA M,N,SB = 0.58865744E+01

REL. MODAL SOUND POWER SPECTRAL DENSITY= -.3327E-15

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

SUM OF ALL ERRORS IN RS CALCULATIONS= 0

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)= -.1548E+03

DOWNSTREAM

GAMMA M,N,SB = -0.39067242E+00

REL. MODAL SOUND POWER SPECTRAL DENSITY= .2438E-15

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

SUM OF ALL ERRORS IN RS CALCULATIONS= 0

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)= -.1561E+03

LARGEST PROPAGATING N FOR THIS M = 1

NO MORE PROPAGATING MODES FOR THIS OMEGA

PROBLEM COMPLETED

RELATIVE POWER SPECTRAL DENSITY LEVEL UPSTREAM= -.4321E+02

REL. POWER SPECTRAL DENSITY LEVEL DOWNSTREAM= -.2497E+02

STOP

END OF EXECUTION

CPU TIME: 3:0.55

ELAPSED TIME: 11:11.94

EXIT.

TABLE 9. INPUT/OUTPUT DATA FOR THE ROTOR WAKE TURBULENCE PROGRAM

This program calculates the modal power spectral density for noise generated by the interaction of rotor wake turbulence with the stator vanes. All input and output data are nondimensional. The input variables are defined in order to parallel as closely as possible the variables used in the Mean Wake and Inlet Turbulence programs. The input data consist of geometric, performance, turbulence, and computational parameters.

A. Geometric Data

FORTRAN NAME	SYMBOL	VARIABLE	FORTRAN VARIABLE TYPE
1. NVANE	V	No. of stator vanes	Integer
2. NBLADE	B	No. of rotor blades	Integer
3. SIGMAR	σ_r	Ratio of hub radius to duct radius	Floating Point
4. SIGMAC	σ_c	Ratio of tip chord of stator vane to duct radius	Floating Point
5.		Vector of data for a number, NDAT (an integer variable) of stator vane radii	
a. R	\bar{r}	Nondimensional radius = r/r_{duct}	Floating Point
b. C	\bar{c}	Nondimensional vane chord = c/c_{tip}	Floating Point
c. THETA	θ	Vane angle (degrees)	Floating Point

B. Performance Data

FORTRAN NAME	SYMBOL	VARIABLE	FORTRAN VARIABLE TYPE
1. MT	M_t	Tip Mach number	Floating Point
2. MA	M	Axial flow Mach number	Floating Point
3.		Frequency range data: Pressure distributions are calculated and stored for the range of frequencies from PSTART to PEND in steps of PSTEP. These data are interpolated for calculations at the frequency of interest OMEGA. See text.	

TABLE 9. (Cont.)

ORIGINAL PRO-
OF POOR QUALITY

FORTRAN NAME		SYMBOL	VARIABLE	FORTTRAN VARIABLE TYPE
a.	PSTART	-	First frequency for pressure calculation. Must be an integer multiple of shaft frequency. (Usually = NBLADE)	Integer
b.	PEND	-	Final frequency for pressure calculation. (Usually = 3x NBLADE)	Integer
c.	PSTEP	-	Frequency step size in pressure calculations. (Usually = NBLADE)	Integer
d.	OMEGA	ω/Ω	Noise frequency of interest (non-dimensionalized on the rotor shaft frequency)	Floating Point
4.	IVOR	-	Switch for rotor wake specification = 0 for free vortex distribution = 1 for specified input velocity distribution	Integer
5.		(for IVOR = 1)	Vector of data for a number, NVELO (an integer variable) of vane radii	
	R	\bar{r}	a. Nondimensional radius	Floating Point
	XVEL	$\frac{V_{yfm}}{V_{xm}}$	b. Ratio of circumferential velocity of mean wake to axial flow velocity (See Fig. 9)	Floating Point
6.	MUV	μ_v	(for IVOR = 0) Ratio of circumferential velocity at the duct radius to the axial flow velocity	Floating Point

C. Turbulence Data

The wake turbulence data are assumed to be constant across the duct.

FORTRAN NAME		SYMBOL	VARIABLE	FORTTRAN VARIABLE TYPE
1.	LX	\bar{L}_x	Axial turbulence length scale (nondimensionalized on the duct radius)	Floating Point

TABLE 9. (Cont.)

ORIGINAL PAGE IS
OF POOR QUALITY

FORTTRAN NAME	SYMBOL	VARIABLE	FORTTRAN VARIABLE TYPE
2. LR	\bar{L}_r	Radial turbulence length scale (nondimensionalized on the duct radius)	Floating Point
3. LTHETA	\bar{L}_θ	Circumferential turbulence length scale (nondimensionalized on the duct radius)	Floating Point
4. EPSW	ϵ_w	RMS turbulence velocity at wake centerline (nondimensionalized on the mean axial velocity), [see Eq. 138 of Vol. 1]	Floating Point
5. WWIDTH	δ	Ratio of turbulent wake width to duct radius (See Eq. 140 of Vol. 1)	Floating Point

D. Computational Data

The computational input data are identical to those used for the inlet turbulence routine.

Program Output

The output consists of the *relative* power spectral density for all propagating modes at the frequency of interest. The nondimensionalization used here is identical to that used for the inlet turbulence routine.

TABLE 10. IMPORTANT INTERNAL PROGRAM VARIABLES FOR THE ROTOR
WAKE TURBULENCE PROGRAM

(Used in addition to INPUT/OUTPUT variables)

FORTRAN NAME	SYMBOL	VARIABLE
OMEGA	ω/Ω	Ratio of noise frequency to rotor shaft frequency
FARG		Argument of \hat{f} (argument)
-THETA		Stator vane angle (radius)
QSUM	-	Sum of correlation function contributions multiplying pressure distribution. Value must exceed QTESTR (input variable) before pressure distribution is actually calculated.
MTHETA	-	Circumferential wake Mach number at a given radius
MYM	-	Relative circumferential wake Mach number at a given radius

TABLE 11. SAMPLE EXECUTION OF THE ROTOR WAKE TURBULENCE
DATA STORAGE ROUTINE

ORIGINAL PAGE IS
OF POOR QUALITY

QSTATOR
NVANE=
11
NVANE= 11
NBLADE=
15
NBLADE= 15
HUB RADIUS DIVIDED BY DUCT RADIUS =
.484
SIGMAR= 0.48400000E+00
VANE TIP CHORD DIVIDED BY DUCT RADIUS=
.408
SIGNAC= 0.40800000E+00
NDAT =
7
NDAT= 7
VANE GEOMETRY MATRIX INPUT
FEED MATRIX IN ONE ROW AT A TIME, FROM HUB TO TIP
ROW= 1 R/RDUCT =
.484
C/CTIP =
1.
THETA (DEGREES)=
16.3
ROW= 2 R/RDUCT =
.56
C/CTIP =
1.
THETA (DEGREES)=
15.67
ROW= 3 R/RDUCT =
.739
C/CTIP =
1.
THETA (DEGREES)=
14.07
ROW= 4 R/RDUCT =
.92
C/CTIP =
1.
THETA (DEGREES)=
12.57
ROW= 5 R/RDUCT =
.946
C/CTIP =
1.

TABLE 11. (Cont.)

ORIGINAL PAGE IS
OF POOR QUALITY

THETA (DEGREES)=

12.36

ROW= 6 R/RDUCT =

.973

C/CTIP =

1.

THETA (DEGREES)=

12.15

ROW= 7 R/RDUCT =

1.

C/CTIP =

1.

THETA (DEGREES)=

11.92

VANE GEOMETRY MATRIX IS

0.484E+00 0.100E+01 0.284E+00

0.560E+00 0.100E+01 0.273E+00

0.739E+00 0.100E+01 0.246E+00

0.920E+00 0.100E+01 0.219E+00

0.946E+00 0.100E+01 0.216E+00

0.973E+00 0.100E+01 0.212E+00

0.100E+01 0.100E+01 0.208E+00

TYPE 1 TO INPUT ROTOR WAKE VELOCITY; 0 FOR FREE VORTEX

1

IVOR= 1

NUMBER OF RADII FOR SPECIFYING MEAN ROTOR FLOW=

8

NVELO= 8

INPUT MATRIX FOR MEAN ROTOR FLOW

FEED MATRIX IN ONE ROW AT A TIME, FROM HUB TO TIP

ROW= 1 R/RDUCT=

.484

MEAN CIRCUMFERENTIAL VELOCITY RATIO(U CIRCUM/U AXIAL)=

.808

ROW= 2 R/RDUCT=

.533

MEAN CIRCUMFERENTIAL VELOCITY RATIO(U CIRCUM/U AXIAL)=

.788

ROW= 3 R/RDUCT=

.612

MEAN CIRCUMFERENTIAL VELOCITY RATIO(U CIRCUM/U AXIAL)=

.784

ROW= 4 R/RDUCT=

.834

MEAN CIRCUMFERENTIAL VELOCITY RATIO(U CIRCUM/U AXIAL)=

.712

TABLE 11. (Cont.)

ORIGINAL PAGE IS
OF POOR QUALITY

ROW= 5 R/RDUCT=
 .918
 MEAN CIRCUMFERENTIAL VELOCITY RATIO(U CIRCUM/U AXIAL)=
 .688
 ROW= 6 R/RDUCT=
 .946
 MEAN CIRCUMFERENTIAL VELOCITY RATIO(U CIRCUM/U AXIAL)=
 .686
 ROW= 7 R/RDUCT=
 .974
 MEAN CIRCUMFERENTIAL VELOCITY RATIO(U CIRCUM/U AXIAL)=
 .713
 ROW= 8 R/RDUCT=
 1.
 MEAN CIRCUMFERENTIAL VELOCITY RATIO(U CIRCUM/U AXIAL)=
 .713
 MEAN ROTOR FLOW VELOCITY MATRIX IS
 .4840E+00 .8080E+00
 .5330E+00 .7880E+00
 .6120E+00 .7840E+00
 .8340E+00 .7120E+00
 .9180E+00 .6880E+00
 .9460E+00 .6860E+00
 .9740E+00 .7130E+00
 .1000E+01 .7130E+00
 MT =
 .508
 MT= 0.50800000E+00
 MA =
 .323
 MA = 0.32300000E+00
 NUMBER OF RADIAL STATIONS =
 5
 NRAD= 5
 NUMBER OF CHORDWISE STATIONS (.LE.20) =
 8
 NCHORD= 8
 START FREQUENCY(HARMONIC NO. OF SHAFT)=
 15
 PSTART= 15
 END FREQUENCY(HARMONIC NO. OF SHAFT)=
 45
 P END= 45
 FREQUENCY STEP SIZE (HARMONIC ORDERS)=
 15
 PSTEP= 15

TABLE 11. (Cont.)

ENTER TITLE FOR DATA FILE (MAX 72 CHARACTERS)
NASA ROTOR/STATOR 55/15 BLADES, 11 VANES/WAKE TURBULENCE STORAGE
ERROR CODE FROM INVERSION ROUTINE= 0
ERROR CODE FROM INVERSION ROUTINE= 0
ERROR CODE FROM INVERSION ROUTINE= 0
ERROR CODE FROM INVERSION ROUTINE= 0
ERROR CODE FROM INVERSION ROUTINE= 0
ERROR CODE FROM INVERSION ROUTINE= 0
ERROR CODE FROM INVERSION ROUTINE= 0

(Note: Edited for brevity -- Error Code
repeated 165 times.)

ERROR CODE FROM INVERSION ROUTINE= 0
STOP

END OF EXECUTION
CPU TIME: 21:28.07 ELAPSED TIME: 1:16:29.97
EXIT.
^C

TABLE 12. SAMPLE EXECUTION OF THE ROTOR WAKE TURBULENCE
NOISE CALCULATION

ORIGINAL PAGE 13
OF POOR QUALITY

WASRCH
USER-ASSIGNED TITLE OF DATA SET FROM FILE "STAT" IS
NASA ROTOR/STATOR 55/15 BLADES, 11 VANES/WAKE TURBULENCE STORAGE
NOISE FREQUENCY/SHAFT FREQUENCY=
15.

OMEGA= .1500E+02
NUMBER OF RADIAL POSITIONS FOR ACOUSTIC COMP.=
7

NRADNU= 7
ACCURACY OF BESSEL FNS=
.001

EB= .1000E-02
ACCURACY OF CONVERGENCE TO ROOT XMN=
.0001

EC= .1000E-03
WAKE WIDTH=
.072

WWIDTH= .7200E-01
TURBULENCE INTENSITY(RMS FLUCTUATING U/U BAR)=
.01

EPSU= .1000E-01
TURBULENCE LENGTH SCALE IN AXIAL DIRECTION=
.5

LX= .5000E+00
TURBULENCE LENGTH SCALE IN RADIAL DIRECTION=
.5

LR= .5000E+00
TURBULENCE LENGTH SCALE IN CIRCUMFERENTIAL DIRECTION=
.5
LTHETA= .5000E+00

M= 0 N= 1 OMEGA= .1500E+02
XFRSAPR Floating underflow PC= 17374

XFRSAPR Floating underflow PC= 17374

UPSTREAM
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9627E+02

DOWNSTREAM
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9577E+02

M= 0 N= 2 OMEGA= .1500E+02

UPSTREAM
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9546E+02

DOWNSTREAM
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1009E+03

TABLE 12. (Cont.)

M= 1 N= 1 OMEGA= .1500E+02

UPSTREAM
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8998E+02

DOWNSTREAM
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1116E+03

M= -1 N= 1 OMEGA= .1500E+02

UPSTREAM
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1050E+03

DOWNSTREAM
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9336E+02

M= 1 N= 2 OMEGA= .1500E+02

UPSTREAM
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8850E+02

DOWNSTREAM
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9785E+02

M= -1 N= 2 OMEGA= .1500E+02

UPSTREAM
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1071E+03

DOWNSTREAM
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9508E+02

M= 2 N= 1 OMEGA= .1500E+02

UPSTREAM
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8758E+02

DOWNSTREAM
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9249E+02

M= -2 N= 1 OMEGA= .1500E+02

UPSTREAM
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1222E+03

DOWNSTREAM
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9020E+02

TABLE 12. (Cont.)

M= 2 N= 2 OMEGA= .1500E+02

UPSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8410E+02

DOWNSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8596E+02

M= -2 N= 2 OMEGA= .1500E+02

UPSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1090E+03

DOWNSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9225E+02

M= 3 N= 1 OMEGA= .1500E+02

UPSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8632E+02

DOWNSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8503E+02

M= -3 N= 1 OMEGA= .1500E+02

UPSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1081E+03

DOWNSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8705E+02

M= 3 N= 2 OMEGA= .1500E+02

UPSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.7849E+02

DOWNSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.7829E+02

M= -3 N= 2 OMEGA= .1500E+02

UPSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9483E+02

DOWNSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9060E+02

TABLE 12. (Cont.)

ORIGINAL PAGE IS
OF POOR QUALITY

M= 4 N= 1 OMEGA= .1500E+02

UPSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8833E+02

DOWNSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8132E+02

M= -4 N= 1 OMEGA= .1500E+02

UPSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1006E+03

DOWNSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8528E+02

M= 5 N= 1 OMEGA= .1500E+02

UPSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8864E+02

DOWNSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8005E+02

M= -5 N= 1 OMEGA= .1500E+02

UPSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9498E+02

DOWNSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8460E+02

M= 6 N= 1 OMEGA= .1500E+02

UPSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8764E+02

DOWNSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8147E+02

M= -6 N= 1 OMEGA= .1500E+02

UPSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8544E+02

DOWNSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8534E+02

PROBLEM COMPLETED

RELATIVE POWER SPECTRAL DENSITY LEVEL UPSTREAM=-.7473E+02

REL. POWER SPECTRAL DENSITY LEVEL DOWNSTREAM=-.7218E+02

STOP

END OF EXECUTION

CPU TIME: 1:59.28

ELAPSED TIME: 4:6.50

EXIT.

APPENDIX

FORTRAN CODE LISTINGS

TABLE OF CONTENTS

	page
I. MAIN PROGRAMS	
A. Mean Wake/Stator Interaction	
MAINV	1
SRCHV	6
FILLOV	11
B. Inlet Turbulence/Rotor Interaction	
1. Calculation and storage of pressure distributions	
MAINTI	18
ROTORS	22
2. Calculation of power spectral density	
INSRCH	27
INTURB	33
C. Wake Turbulence/Stator Interaction	
1. Calculation and storage of pressure distributions	
MAINTW	45
STATOR	50
2. Calculation of power spectral density	
WASRCH	55
WATURB	62
II. Function Subroutines	
ANRT (Contains ANRT, ANFU, BESJ, BESY, ISIG) ...	74
CASC	84
EIGEN	86
EPSD	88
FHAT	90
KERNEL	92
PHITHH	94
PHIXHT	96
PRES	98
RMODE	100

PRECEDING PAGE BLANK NOT FILMED

TABLE OF CONTENTS (Cont.)

	page
II.	
SCALLR	102
SCALLX	104
STHETA	106
III. Utility Programs	
MAPIN/MAPPER	108
Sample Execution of MAPIN/MAPPER	113

PROGRAM MAINV

This is the calling program
controlling the computation of
mean wake/stator interaction
noise.

PROGRAM MAINV
 DIMENSION IDATA(10),FDATA(20),VGROW(10,7),VELOCV(10,2)
 REAL VT,VA,MUV,LX?

C
 C

2001 WRITE(5,2001)
 FORMAT(' NVANE=')
 READ(5,1001) NVANE
 1001 FORMAT(20.0)
 WRITE(5,2101) NVANE
 2101 FORMAT(' NVANE=',I3)
 WRITE(5,2002)
 2002 FORMAT(' VELADE=')
 READ(5,1001) VELADE
 WRITE(5,2102) VELADE
 2102 FORMAT(' VELADE=',I3)
 WRITE(5,2003)
 2003 FORMAT(' HUB RADIUS DIVIDED BY DUCT RADIUS =')
 READ(5,1001) SIGMAR
 WRITE(5,2103) SIGMAR
 2103 FORMAT(' SIGMAR=',E16.8)
 WRITE(5,2004)
 2004 FORMAT(' VANE TIP CHORD DIVIDED BY DUCT RADIUS =')
 READ(5,1001) SIGMAC
 WRITE(5,2104) SIGMAC
 2104 FORMAT(' SIGMAC=',E16.8)
 WRITE(5,2005)
 2005 FORMAT(' LX? =')
 READ(5,1001) LX?
 WRITE(5,2105) LX?
 2105 FORMAT(' LX?=',E16.8)

C
 C

WRITE(5,2006)
 2006 FORMAT(' NDAT =')
 READ(5,1001) NDAT
 WRITE(5,2106) NDAT
 2106 FORMAT(' NDAT=',I3)
 WRITE(5,2007)
 2007 FORMAT(' VANE GEOMETRY MATRIX INPUT')
 WRITE(5,2008)
 2008 FORMAT(' FEED MATRIX IN ONE ROW AT A TIME, FROM HUB TO TIP')

C
 C

DO 10 IPOM=1,NDAT
 WRITE(5,2009) IPOM
 2009 FORMAT(' POM=',I3,' R/RODUCT =')
 READ(5,1001) VGROW(IPOM,1)
 WRITE(5,2010)
 2010 FORMAT(' C/CTIP =')
 READ(5,1001) VGROW(IPOM,2)
 WRITE(5,2011)

ORIGINAL PAGE IS
OF POOR QUALITY

```

2011      FORMAT(' ALPHAS (DEGREES)=')
        READ(5,1001) VGEOM(IPOW,3)
        VGEOM(IPOW,3)=VGEOM(IPOW,3)*.21*.533
        WRITE(5,2012)
2012      FORMAT(' VS/CTIP =')
        READ(5,1001) VGEOM(IPOW,4)
        WRITE(5,2013)
2013      FORMAT(' VF/CTIP =')
        READ(5,1001) VGEOM(IPOW,5)
        WRITE(5,2014)
2014      FORMAT(' YS/CTIP =')
        READ(5,1001) VGEOM(IPOW,6)
        WRITE(5,2015)
2015      FORMAT(' XS/CTIP =')
        READ(5,1001) VGEOM(IPOW,7)
10      CONTINUE
C
C
        WRITE(5,2020)
2020      FORMAT(' VANE GEOMETRY MATRIX IS')
        DO 11 IPOW=1,NDAT
        WRITE(5,2120) (VGEOM(IROW,ICOLN),ICOLN=1,7)
2120      FORMAT(' ',7E13.3)
11      CONTINUE
        WRITE(5,5000)
5000      FORMAT(' TYPE 1 TO INPUT ROTOR FLOW VELOCITY,2 FOR FREE VORTEX')
        READ(5,1001) IVOR
        WRITE(5,5010) IVOR
5010      FORMAT(' IVOR=',I3)
        IF (IVOR.EQ.0) NVELO=C
        IF (IVOR.EQ.1) GO TO 4005
C
C
        WRITE(5,3000)
3000      FORMAT(' NUMBER OF RADII FOR SPECIFYING MEAN ROTOR FLOW=')
        READ(5,1001) NVELO
        WRITE(5,3010) NVELO
3010      FORMAT(' NVELO=',I3)
        WRITE(5,3014)
3014      FORMAT(' INPUT MATRIX FOR MEAN ROTOR FLOW')
        WRITE(5,3016)
3016      FORMAT(' FEED MATRIX IN ONE ROW AT A TIME, FROM HUB TO TIP')
        DO 4012 IROW=1,NVELO
        WRITE(5,3003) IROW
3003      FORMAT(' ROW=',I3,' R/RDUCT=')
        READ(5,1001) VELOCV(IROW,1)
        WRITE(5,3012)
3012      FORMAT(' MEAN CIRCUMFERENCEAL VELOCITY RATIO=')
        READ(5,1001) VELOCV(IROW,2)
4012      CONTINUE
C

```



```

C
3014 WRITE(5,2014)
      FORMAT(' MEAN ROTOR FLOW VELOCITY MATRIX IS ')
      DO 4022 IROW=1,NVFLC
3016 WRITE(5,2016) (VLLDCV(IROW,ICOLMN),ICOLMN=1,2)
4022 CONTINUE

```

```

C
C
4025 CONTINUE

```

ORIGINAL PAGE 17
OF POOR QUALITY

```

      WRITE(5,2030)
2030 FORMAT(' MT = ')
      READ(5,1071) MT
      WRITE(5,2137) MT
2137 FORMAT(' MT= ',E16.8)
      WRITE(5,2031)
2031 FORMAT(' MA = ')
      READ(5,1071) MA
      WRITE(5,2131) MA
2131 FORMAT(' MA = ',E16.8)
      IF(IWOR.EQ.1) GO TO 6022
      WRITE(5,2032)
2032 FORMAT(' VVFA/VVFA 2 PRODUCT = ')
      READ(5,1071) VVFA
      WRITE(5,2132) VVFA
2132 FORMAT(' VVFA= ',E16.8)
6022 CONTINUE

```

```

      IF(IWOR.EQ.1) VVFA=2.
      WRITE(5,2033)
2033 FORMAT(' WAKE WIDTH = ')
      READ(5,1071) WWIDTH
      WRITE(5,2133) WWIDTH
2133 FORMAT(' WWIDTH= ',E16.8)
      WRITE(5,2034)
2034 FORMAT(' MAY VEL DEFICIT DIVIDED BY UBAF ')
      READ(5,1071) VELDEF
      WRITE(5,2134) VELDEF
2134 FORMAT(' WELDEF= ',E16.8)

```

```

C
C
2035 WRITE(5,2135)
      FORMAT(' NUMBER OF RADIAL STATIONS = ')
      READ(5,1071) NRAD
      WRITE(5,2135) NRAD
2135 FORMAT(' NRAD= ',I4)
      WRITE(5,2036)
2036 FORMAT(' NUMBER OF CHORDWISE STATIONS = ')
      READ(5,1071) NCHORD
      WRITE(5,2136) NCHORD

```

ORIGINAL PAGE IS
OF POOR QUALITY

```
2136  FORMAT(' NCHORD=',I4)
      WRITE(5,2037)
2037  FORMAT(' ACCURACY OF BESSEL FN =')
      READ(5,1001) EB
      WRITE(5,2137) EB
2137  FORMAT(' EB=',E16.8)
      WRITE(5,2038)
2038  FORMAT(' ACCURACY OF CONVERGENCE TO ROOT XMN =')
      READ(5,1001) EC
      WRITE(5,2138) EC
2138  FORMAT(' EC=',E16.8)
```

C
C

```
IDATA(1)=NVANE
IDATA(2)=NBLADE
IDATA(3)=NRAD
IDATA(4)=NCHORD
IDATA(5)=NDAT
IDATA(9)=IVOR
IDATA(10)=NVELO
```

C
C

```
RDATA(1)=MT
RDATA(2)=MA
RDATA(3)=LX0
RDATA(4)=SIGMAC
RDATA(5)=SIGMAR
RDATA(6)=MUV
RDATA(7)=WWIDTH
RDATA(8)=VELDEF
RDATA(9)=EB
RDATA(10)=EC
```

C
C

```
CALL SRCHV(IDATA,RDATA,VGEOM,VELOCV)
STOP
END
```

PROGRAM SRCHV

Program determines which modes
propagate for the mean wake/
stator interaction and enables
the noise calculation.

```

      SUBROUTINE SPCHV(IDATA,ADATA,VGEOM,VELOCV)
      INTEGER S,P1
      DIMENSION IER(9),IDATA(12),M(122)
      DIMENSION RDATA(27),VGEOM(17,7),POWER(3,2),SPWR(2),RELER(3,2)
      DIMENSION VELOCV(15,2)
      REAL VT,VA

```

```

      DATA((POWER(I,J),I=1,3),J=1,2)/6*E.2/

```

```

      S=4

```

```

      S=S-1

```

```

      IF(S.LE.2) GO TO 9830

```

```

      WRITE(5,2007) S
      FORMAT('2S =',I2)

```

ORIGINAL PAGE IS
OF POOR QUALITY

```

      NVANE=IDATA(1)
      NBLADE=IDATA(2)
      VT=ADATA(1)
      VA=ADATA(2)
      SIGMA=ADATA(5)
      EP=ADATA(9)
      EC=ADATA(10)

```

```

      XVAX=S*NBLADE*VT/(1.-VA**2)**.5

```

```

      WRITE(5,2001) XVAX
      FORMAT('XVAX(XV) FOR PROPAGATION =',E16.8)

```

```

      P1=(S*NBLADE)/NVANE
      MTEST=2*S*NBLADE-(2*P1+1)*NVANE
      IF(MTEST.GT.0) P1=P1+1

```

```

      J=1
      M(1)=S*NBLADE-P1*NVANE

```

```

      N=1
      N=N+1

```

```

      MABS=M(J)
      IF(M(J).LT.0) MABS=-MABS

```

C

CALL ANPT (MABS,N,SIGMAP,BB,EC,XMN,IEB,IEC)

C

C

IF(XMN.GE.XMAX) GO TO 6003

C

C

ORIGINAL PAGE IS
OF POOR QUALITY

WRITE(5,3000)

3000

FORMAT('2MODE DATA')

WRITE(5,3001) S,'(J)',N,XMN

3001

FORMAT('S =',I3,' N =',I3,' MN =',I3,' XMN =',E16.8)

IF(XMN.EQ.0.) GO TO 1000

COEFF=XMAX/XMN

WRITE(5,4000) COEFF

4000

FORMAT(' CUTOFF RATIO FOR MODE=',E12.4)

GO TO 1005

1005

CONTINUE

WRITE(5,4005)

4005

FORMAT(' PLANE WAVE MODE: CUTOFF RATIO IS + INFINITE')

1005

CONTINUE

WRITE(5,3002) IEB

3002

FORMAT(' SUM OF BESSEL FUNCTION ERROR CODES =',I3)

WRITE(5,3003) IEC

3003

FORMAT(' ERROR CODE FOR CONVERGENCE TO ROOT XMN =',I3)

C

C

CALL FICEN (MABS,SIGMAR,XMN,AMN,BMN,BB,IER)

C

C

WRITE(5,3004) AMN,BMN

3004

FORMAT(' AMN =',E16.8,' BMN =',E16.8)

WRITE(5,3005) IER

3005

FORMAT(' ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC =',I3)

C

C

RDATA(11)=XMN

RDATA(12)=AMN

RDATA(13)=BMN

IDATA(6)=N(J)

IDATA(7)=N

IDATA(8)=S

C

C

CALL FIELLO(IDATA,RDATA,V3EOM,VELOCV,SPWR)

II=IABS(IDATA(8))

POWER(II,1)=POWER(II,1)+SPWR(1)

POWER(II,2)=POWER(II,2)+SPWR(2)

C

C

IDATA(6)=-IDATA(6)

IDATA(8)=-IDATA(8)

C
C

```

8300 WRITE(5,8300) IDATA(6),IDATA(7),IDATA(8)
      FORMAT('X=',I5,' N=',I5,' S=',I5)
      RELUP=12.*ALOG10(SPWR(1))
      WRITE(5,8400)
8400 FORMAT('UPSTREAM ')
      WRITE(5,8600) RELUP
8600 FORMAT(' RELATIVE SOUND POWER LEVEL FOR MODE(02)=' ,F16.4)
      RELDN=12.*ALOG10(SPWR(2))
      WRITE(5,8200)
8200 FORMAT('DOWNSTREAM ')
      WRITE(5,8600) RELDN
      II=IABS(IDATA(8))
      POWER(II,1)=POWER(II,1)+SPWR(1)
      POWER(II,2)=POWER(II,2)+SPWR(2)

```

C
C

```

      IDATA(6)=-IDATA(6)
      IDATA(8)=-IDATA(8)

```

C
C

```

      GO TO 2'

```

C
CC
CC
CC
CC
CC
CC
CC
CC
CC
CC
CC
CC
CC
CC
CC
CC
CC
C

ORIGINAL PAGE IS
OF POOR QUALITY

```

6100 IF(N.EQ.1) GO TO 7000

```

```

      NMAX=N-1

```

```

      WRITE(5,6000) NMAX

```

6000

```

      FORMAT('LARGEST PROPAGATING N FOR THIS M =' ,I3)

```

```

      IF(J.EQ.1) GO TO 6100

```

```

      IF(V(1).EQ.0) GO TO 6200

```

```

      IF(V(J-1).LT.0) W(J+1)=V(J-1)-NVAVE

```

```

      IF(V(J-1).GT.0) W(J+1)=V(J-1)+NVAVE

```

```

      J=J+1

```

```

      GO TO 1'

```

```
6100  CONTINUE
      IF(M(1).LT.2) M(2)=M(1)+NVAVE
      IF(M(1).GT.2) M(2)=M(1)-NVAVE
C
C
      J=2
      GO TO 15
C
C
6200  V(J+1)=M(J)+NVAVE
      J=J+1
      GO TO 15
C
C
7000  IF(J.EQ.1) GO TO 3000
C
C
      WRITE(5,7001)
7001  FORMAT(' NO MORE PROPAGATING MODES FOR THIS VALUE OF S')
      GO TO 15
8000  CONTINUE
      WRITE(5,8001)
8001  FORMAT(' NO PROPAGATING MODES FOR THIS VALUE OF S')
      GO TO 15
C
C
9000  CONTINUE
      WRITE(5,9001)
9001  FORMAT(' PROBLEM COMPLETED')
      DO 550 II=1,3
      DO 550 JJ=1,2
      IF(POWER(II,JJ).EQ.2.) GO TO 5215
      RELPR(II,JJ)=17.*ALOG10(POWER(II,JJ))
      GO TO 550
5215  RELPR(II,JJ)=1.7+35
550  CONTINUE
      DO 600 II=1,3
      IF(RELPR(II,1).EQ.1.5+35) GO TO 5315
      WRITE(5,610) II,RELPR(II,1)
      GO TO 600
5315  WRITE(5,5610) II
5610  FORMAT(' S=',I2,' HARMONIC IS UNEXCITED')
600  CONTINUE
610  FORMAT(' RELATIVE POWER LEVEL UPSTREAM S=',I2,5X,E16.4)
      DO 620 II=1,3
      IF(RELPR(II,2).EQ.1.5+35) GO TO 5415
      WRITE(5,630) II,RELPR(II,2)
      GO TO 620
5415  WRITE(5,5610) II
620  CONTINUE
630  FORMAT(' RELATIVE POWER LEVEL DOWNSTREAM S=',I2,5X,E16.4)
      STOP
      END
```

ORIGINAL PAGE IS
OF POOR QUALITY

ORIGINAL PAGE IS
OF POOR QUALITY

PROGRAM FILLOV

Program computes the noise
generated by the mean wake/
stator interaction in a sub-
sonic turbofan.


```

SUBROUTINE FILLUV(IDATA,RDATA,VGEOM,VELOCV,SPWR)
DIMENSION VGEOM(14,7),RDATA(27),IDATA(12),XX(6),IERPSI(2),SPWR(2)
DIMENSION PHASE(40),VELOCV(14,2)
DIMENSION PSISTD(2)
INTEGER SS,SS
REAL KX,K,KVNS,IR,IT,IA,MUV,NYA,LYZ
REAL MTHETA,MTHRUB
COMPLEX L,AF,DELTA(140),FMS,FVNS,FANS,AMNS
COMPLEX FAN(40)
COMPLEX QNSTA(50,50)
COMPLEX CASCET(20,30)
DATA ISS/3/
I=(0.,1.)
PI=3.1415926

```

ORIGINAL PAGE IS
OF POOR QUALITY

```

NNAME=IDATA(1)
NPLAGE=IDATA(2)
NPAO=IDATA(3)
NCHORD=IDATA(4)
ADAT=IDATA(5)
MV=IDATA(6)
AN=IDATA(7)
SS=IDATA(8)
IVDP=IDATA(9)
AVELO=IDATA(10)

```

```

WRITE(5,8306) MV,AN,SS
8306 FORMAT('MV=',I5,' AN=',I5,' S=',I5)
7204 FORMAT(' NPAO=',I3,' NCHORD=',I3)

```

```

MT=PDAT(1)
N2=PDAT(2)
LYE=PDAT(3)
SIGMAC=PDAT(4)
SIGMAR=PDAT(5)
MUV=PDAT(6)
NWIDTH=PDAT(7)
VELLOC=PDAT(8)
ER=PDAT(9)
EC=PDAT(10)
XUN=PDAT(11)
AMN=PDAT(12)
BMN=PDAT(13)

```

SP=SS*VELLOC

C
BETASQ=1.-V1**2
KANS=((((SP**NT)**2-LEFTASQ**X**2)**.5)*ABS(1.*SS))/(1.*SS)
7016 FORMAT(' KANS=',F10.4)

C
C
WDATA=EVF(14.038879*WIDTH**2)
SUM=2.
ERROR=.1E-5
INDEX=0
100 INDEX=INDEX+1
DSUM=1./((VST**2**((INDEX**2)))
SUM=SUM+DSUM
IF(DSUM.LT.ERROR) GO TO 110
GO TO 100

ORIGINAL PAGE IS
OF POOR QUALITY

C
C
110 XSIGN=1.
111 GVNS=(SP**NA*NT+XSIGN**X**S)/BETASQ
PVNS=(2.,E.)
DELTA=(1.-SIGNAR)/(N*AD-1)
IF=0
IDAT=0
IDOT=2

C
C
SWTP=-1.
DO 200 IF=1, N*AD

C
C
R=SIGNAR+(IF-1.)*(1.-SIGNAR)/(N*AD-1.)
IF(P.LE.VGEOM(IDAT,1)) GO TO 221
IDAT=IDAT+1
IF(IDAT.GT.NDAT) IDAT=NDAT
201 DELTA=(P-VGEOM(IDAT,1))/(VGEOM(IDAT,1)-VGEOM(IDAT-1,1))
DO 210 IX=2,7
210 AX(IX-1)=VGEOM(IDAT,IX)+DELTA*(VGEOM(IDAT,IX)-VGEOM(IDAT-1,IX))

C
C
P=XV(1)/2.
ALPHAS=XX(2)
YS=YX(3)
YR=YX(4)
XS=YX(5)
XP=YX(6)
7011 FORMAT(' B,ALPHAS,YS,YR,YS,XP OF R IS')
7012 FORMAT(6F10.4)

C
C
IF(IVOR.EQ.7) GO TO 4127

ORIGINAL PAGE IS
OF POOR QUALITY

$$K=SP*VT*B*SIGMAC/(1.-VR**2)$$

$$GAMMA=(2.*SP*PI/NUAN**2)*(1.+VT*VR*K*SINAS/(1.-VR**2))$$

$$H1=-2.*PI*K*SINAS/(NUAN**2*SIGMAC)$$

$$H2=2.*PI*B*COBAS/(NUAN**2*SIGMAC)$$

SKIP CALL AND STOP OF PRES FOR DOWNSTREAM
IF(YSTGV.FD.-1.) GO TO 328

SKIP PRES CALL AFTER NAD CALLS FOR THIS VALUE OF S(=SS)
IF(SS.EQ.ISS) GO TO 302

307 FORMAT('INPUT TO SUBROUTINE PRES')

307 FORMAT(' W4=',E16.4)

304 FORMAT(' WY=',E16.4,' W=',E16.4,' GAMMA=',E16.4)

WRITE(21,305) W4,H1,H2,NCHORD

306 FORMAT(' W2=',E16.4,' H1=',E16.4,' H2=',E16.4,' NCRD=',I3)

CALL PRES((1.,W.),WY,W,GAMMA,W2,H1,H2,NCHORD,DELTAP,IERP)

IF(YE.EQ.NAD) ISS=SS

DO 310 IC=1,NCHORD

CASCET(IC,IC)=DELTAP(IC)

CONTINUE

312 WRITE(5,7500) IERP

7500 FORMAT(' ERROR CODE FROM INVERSION ROUTINE=',I3)

7025 FORMAT(' OUTPUT FROM PRES:(DELTAP(I2),I2=1,NCHORD)
(DELTAP(I4),I2=1,NCHORD)

308 CONTINUE
Z'UD=SIGMAC*B*(GAMMA*COBAS-WY*SINAS/P)

Q'AS=CASCET(IP,NCHORD)/2.

Q'NST'(IP,NCHORD)=Q'AS

S'IC=1.

```

C
  NFIN=NCHORD-1
  DO 227 IZ=1,NFIN
    WHIC=1.+SWTC/3.
    SWTC=-SWTC
    THETA=(IZ*PI)/NCHORD
    QVNSTV(IF,IZ)=CISCT(IN,IZ)*CEXP(I*ZMOL*(1.+COS(THETA)))
220  QVNS=QVNSTV+WHIC*CACTT(IF,IZ)*CEXP(I*ZMOL*(1.+COS(THETA)))
    QVNS=QVNS*(1.+(IX/5)**2)*PI/NCHORD

7022  FOR AT(' IF=',IZ,' QVNS(P)=' ,2E12.4,' WH(R)=' ,2E12.4)
    QVNS=QVNSTV

C
C
C  SKIP BRIDGE CALL AND STORE FOR DOWNSTREAM
    IF(XSIGN.DQ.-1.) GO TO 7021

C
C  APP=XAN*W

C
C  CALL BRIDGE (M,ARG,MW,PM,PSI,FB,IEAPSI)
    PSISTO(IZ)=PSI
7020  FORMAT(' PSI(2)=' ,F16.5)

C
C  IEA=IEA+IEAPSI(1)+IEAPSI(2)

C
C  7021  CONTINUE
    CA=QVNS*SIGNIS+44*COBAS/P
    CB=(MW*YB/R-QVNS*XS)*SIGNAC
    PHLS=(QVNS*PSISTO(IZ)/QVNS)*CA
    PHN(IZ)=PHN
    PHASE(IZ)=CB-PHASE1-PHASE2

200  CONTINUE
    DO 2004 J=1,NFAT
2001  FORMAT(I4,3F14.5)
2004  CONTINUE
    PHC=?.
    DO 272 N=1,NRAD-1
      GP=.5*(PHASE(N)+PHASE(N+1))
      X=.5*(PHASE(N+1)-PHASE(N))
      IF(ABS(X).LT.F.001) GO TO 268
      W=.5*(X)/(2.*X)
      W1=(SIN(X)/Y-COS(X))/(4.*X)
      GO TO 269
268  W=.5*(1.-X**2/6.)
      W1=X*(1.-X**2/12.)/6.
269  CON 100
      PHNS=PHNS+DELTAIR*CEXP(I*G2)*((W2-I*W1)*PHN(N)+(W2+I*W1)*PHN(N+1)
      **)
```

ORIGINAL PAGE IS
OF POOR QUALITY

```

276      CONTINUE
      AMPS=-PMNS*WAVE*SIGMAC/(PI*(1.-SIGMA**2))
C
      POWNUM=2.*AMNS*SE*MT*(CABS(PMNS)*FETASJ*WAVE*SIGMAC)**2
      POWDEN=PI*(1.-SIGMA**2)*((SE*MT)+XSIGV*WAVE*PMNS)**2
      RELPMR=POWNUM/POWDEN
      RELPEL=12.*ALOG10(RELPMR)
C
CC
C
      IF(XSIGV.LT.0.) GO TO 9221
C
C
      WRITE(5,3201)
      FORMAT('UPSTREAM ')
      WRITE(5,8101) GUNS
      8101   FORMAT(' GAMMA M,N,SE =',E16.8)
      WRITE(5,5122) AMNS
      8102   FORMAT(' MODE AMPLITUDE =',2E16.8)
      WRITE(5,8522) IER
      8500   FORMAT(' SUM OF ALL ERRORS IN PSI CALCULATIONS =',I5)
      WRITE(5,8622) RELPEL
      8600   FORMAT(' RELATIVE SOUND POWER LEVEL FOR MODE(0)=',E16.4)
      DO 7006 IF=1,NRAD
      P=SIGMAR+(IF-1.)*(1.-SIGMAR)/(NRAD-1.)
      7002   FORMAT(5X,E12.4)
      7006   CONTINUE
      7202   FORMAT(' END OF UPSTREAM INTEGRATION')
      YSIGV=-1.
      SPVP(1)=RELPMR
      GO TO 111
      9080   WRITE(5,8200)
      8200   FORMAT('DOWNSTREAM')
      WRITE(5,8201) GUNS
      8201   FORMAT(' GAMMA M,N,SE =',E16.8)
      WRITE(5,8202) AMNS
      8202   FORMAT(' MODE AMPLITUDE =',2E16.8)
      WRITE(5,8422) IER
      8400   FORMAT(' SUM OF ALL ERRORS IN PSI CALCULATIONS =',I5)
      WRITE(5,8622) RELPEL
      SPVP(2)=RELPMR
      7202   FORMAT(' END OF DOWNSTREAM INTEGRATION')
      RETURN
      END

```

ORIGINAL PAGE IS
OF POOR QUALITY

PROGRAM MAINTI

This is a calling program to control the computation of pressure data for the inlet turbulence case.

```

      PROGRAM MAINTI
      DIMENSION IDATA(10),RDATA(20),VGEOM(10,7)
      REAL MT,MA
      INTEGER PSTART,PEND,P,PRANGE,PSTEP
      DATA (IDATA(J),J=1,10)/10*0/
      DATA (RDATA(J),J=1,20)/20*0.0/

```

ROTOR INFLOW TURBULENCE -- MATRIX STORAGE PROGRAM

THIS PROGRAM GROUP CALCULATES AND STORES VECTORS OF
THE COMPLEX PRESSURE DISTRIBUTION ACROSS THE ROTOR BLADE.

DATA REQUIRED TO EXECUTE THIS ROUTINE INCLUDE:

1. BLADE GEOMETRY
2. ROTOR OPERATING SPEEDS
3. NUMBER OF RADIAL AND CHORDWISE POSITIONS AT WHICH THE
PRESSURES ARE CALCULATED
4. FREQUENCY RANGE OF INTEREST (EXPRESSED IN TERMS
OF HARMONIC ORDER OF SHAFT ROTATION).

THE RANGE OF CIRCUMFERENTIAL MODE NUMBER M IS 0 TO NBLADE-1.

NCHORD MUST BE NO GREATER THAN 20.

```

1001  FORMAT(G20.8)
      WRITE(5,2002)
2002  FORMAT(' NBLADE=')
      READ(5,1001) NBLADE
      WRITE(5,2102) NBLADE
2102  FORMAT(' NBLADE=',I3)
      WRITE(5,2003)
2003  FORMAT(' HUB RADIUS DIVIDED BY DUCT RADIUS =')
      READ(5,1001) SIGMAR
      WRITE(5,2103) SIGMAR
2103  FORMAT(' SIGMAR=',E16.8)
      WRITE(5,2004)
2004  FORMAT(' BLADE TIP CHORD DIVIDED BY DUCT RADIUS=')
      READ(5,1001) SIGMAC
      WRITE(5,2104) SIGMAC
2104  FORMAT(' SIGMAC=',E16.8)
      C
      C
      WRITE(5,2006)
2006  FORMAT(' NDAT =')
      READ(5,1001) NDAT
      WRITE(5,2106) NDAT
2106  FORMAT(' NDAT=',I3)
      WRITE(5,2007)

```

ORIGINAL PAGE IS
OF POOR QUALITY


```

2007  FORMAT(' BLADE GEOMETRY MATRIX INPUT')
      WRITE(5,2008)
2008  FORMAT(' FEED MATRIX IN ONE ROW AT A TIME, FROM HUB TO TIP')
C
C
      DO 10 IROW=1,NDAT
      WRITE(5,2009) IROW
2009  FORMAT(' ROW=',I3,' R/RDUCT =')
      READ(5,1001) VGEOM(IROW,1)
      WRITE(5,2010)
2010  FORMAT(' C/CTIP =')
      READ(5,1001) VGEOM(IROW,2)
      WRITE(5,2011)
2011  FORMAT(' CHI (DEGREES)=')
      READ(5,1001) VGEOM(IROW,3)
      VGEOM(IROW,3)=VGEOM(IROW,3)*.0174533
10    CONTINUE
C
C
      WRITE(5,2020)
2020  FORMAT(' BLADE GEOMETRY MATRIX IS')
      DO 11 IROW=1,NDAT
      WRITE(5,2120) (VGEOM(IROW,ICOLMN),ICOLMN=1,3)
2120  FORMAT(' ',7E10.3)
11    CONTINUE
C
C
      WRITE(5,2030)
2030  FORMAT(' MT =')
      READ(5,1001) MT
      WRITE(5,2130) MT
2130  FORMAT(' MT=',E16.8)
      WRITE(5,2031)
2031  FORMAT(' MA =')
      READ(5,1001) MA
      WRITE(5,2131) MA
2131  FORMAT(' MA=',E16.8)
C
C
      WRITE(5,2035)
2035  FORMAT(' NUMBER OF RADIAL STATIONS =')
      READ(5,1001) NRAD
      WRITE(5,2135) NRAD
2135  FORMAT(' NRAD=',I4)
      WRITE(5,2036)
2036  FORMAT(' NUMBER OF CHORDWISE STATIONS =')
      READ(5,1001) NCHORD
      WRITE(5,2136) NCHORD
2136  FORMAT(' NCHORD=',I4)
C

```

ORIGINAL PAGE IS
OF POOR QUALITY

C
C
100 WRITE(5,100)
FORMAT(' START FREQUENCY(HARMONIC NO. OF SHAFT)=')
READ(5,1001) PSTART
WRITE(5,110) PSTART
110 FORMAT(' PSTART=',I4)
WRITE(5,120)
120 FORMAT(' END FREQUENCY(HARMONIC NO. OF SHAFT)=')
READ(5,1001) PEND
WRITE(5,130) PEND
130 FORMAT(' P END=',I4)

C
C
140 WRITE(5,140)
FORMAT(' FREQUENCY STEP SIZE (HARMONIC ORDERS)=')
READ(5,1001) PSTEP
WRITE(5,150) PSTEP
150 FORMAT(' PSTEP=',I4)
PRANGE=(PEND-PSTART)/PSTEP+1
IDATA(2)=NBLADE
IDATA(3)=NRAD
IDATA(4)=NCHORD
IDATA(5)=NDAT
IDATA(6)=PSTART
IDATA(7)=PEND
IDATA(8)=PSTEP

ORIGINAL PAGE IS
OF POOR QUALITY

C
C
RDATA(1)=MT
RDATA(2)=MA
KDATA(4)=SIGMAC
RDATA(5)=SIGNAR

C
C
CALL ROTORS(IDATA,RDATA,VGEOM)
STOP
END

ORIGINAL PAGE IS
OF POOR QUALITY

PROGRAM ROTORS

Program calculates and stores
the pressures generated on a
turbofan rotor by inlet tur-
bulence.

SUBROUTINE ROTORS(IUATA,RDATA,VGEOM)

ADJUSTABLE DIMENSION STATEMENTS USED TO MINIMIZE STORAGE
REQUIREMENTS OF MATRIX CASCET

DIMENSION OF DELTAP=20
DIMENSION OF CASCET=(NCHORD,NRAD,NBLADE,PRANGE)

NOTE NCHORD MUST BE NO GREATER THAN 20
DIMENSION DELTAP(20)
DIMENSION VGEOM(10,7),RDATA(20),IUATA(10),AA(6)
DIMENSION CASCET(0,0,10,0)
DIMENSION A(72)
REAL KB,MP,MA,MT
COMPLEX L,DELTAP,CASCET
INTEGER PSTART,PEND,P,PRANGE,POLY
I=(0,1.)
PI=3.1415926

ORIGINAL PAGE IS
OF POOR QUALITY

NBLADE=IUATA(2)
NRAD=IUATA(3)
NCHORD=IUATA(4)
NDA1=IUATA(5)
PSTART=IUATA(6)
PEND=IUATA(7)
PSTEP=IUATA(8)

M1=RDATA(1)
MA=RDATA(2)
SIGNAC=RDATA(4)
SIGNAR=RDATA(5)

INITIALIZE IUAT FOR GEOMETRIC DATA

IUAT=2

WRITE(5,100)
100 FORMAT(' ENTER TITLE FOR DATA FILE(MAX 72 CHARACTERS)')
READ(5,100) A
1003 FORMAT(72A1)

START LOOPS TO CALL CASC-DECOM WITH LOOP ON RADIAL
POSITION TO MINIMIZE INTERPOLATION.

DO 330 IK=1,NRAD

C
 R=SIGMAR*(IR-1.)*(1.-SIGMAR)/(NRAD-1.) ORIGINAL PAGE IS
 IF(R.LE.VGEUM(IDAT,1)) GO TO 201 OF POOR QUALITY
 IDAT=IDAT+1
 IF(IDAT.GT.NDAT) IDAT=NDAT
 201 DELTA=(R-VGEUM(IDAT,1))/(VGEUM(IDAT,1)-VGEUM(IDAT-1,1))
 DO 210 IA=2,3
 210 XX(IA-1)=VGEUM(IDAT,IX)+DELTA*(VGEUM(IDAT,IX)-VGEUM(IDAT-1,IX))

C
 C
 D=XX(1)/2.
 CNI=XX(2)
 WRITE(21,7010) D,CNI,R
 7010 FORMAT(' D=',E10.4,' CNI=',E10.4,' R=',E10.4)

C
 C
 C
 C
 COSCNI=COS(CNI)
 SINCNI=SIN(CNI)

C
 C
 C
 BEGIN LOOPS ON MODE NUMBER M AND FREQUENCY COUNTER P

C
 DO 300 M=1,NBLAUE
 MM=M+COUNT-1

C
 C
 C
 IF IS STORAGE COUNTER FOR PARAMETER P IN MATRIX CASCET
 IP=?

C
 C
 C
 DO 310 P=PSTART,PEND,PSTEP
 IP=IP+1

C
 C
 C
 C
 C
 UNCOUC=M1*SIGMAC*D*(P-MM)

C
 C
 C
 C
 C
 MR=(MA**2+(MT+R)**2)**+.5

C
 C
 C
 C
 C
 AD=M1/MR*D*SINAC*(P-MM)
 SIGMA=-2.*PI*MM/NBLAUE

C
 C
 C
 C
 C
 B=2.*PI*R/NBLAUE/SINAC/D

```

C
C      WRITE(21,300)
300      FORMAT('INPUT TO SUBROUTINE CASC')
C      WRITE(21,302) OMEGBC
302      FORMAT(' OMEGBC=',E12.4)
C      WRITE(21,304) MR,KB,SIGMA
304      FORMAT(' MR=',E12.4,' KB=',E12.4,' SIGMA=',E12.4)
C      WRITE(21,306) n,CHI,NCHORD
306      FORMAT(' n=',E12.4,' CHI=',E12.4,' nchord=',I3)

C
C
C
C
C      CALL CASC(OMEGBC,MR,KB,SIGMA,H,CHI,NCHORD,DELTAP,IERP)

C
C      STORE RESULTS OF CASC IN STORAGE MATRIX FOR DISK FILE.
C      MATRIX POSITION DESCRIPTORS ARE (IN ORDER OF APPEARANCE):
C      1. CHORDWISE POSITION (TRAILING TO LEADING EDGES)
C      2. RADIAL POSITION (INNER RADIUS TO OUTER RADIUS)
C      3. CIRCUMFERENTIAL MODE NUMBER + 1 (M+1)
C      4. ORDER OF FREQUENCY COMPUTATIONS (FIRST TO LAST)
C      WITH: IP=1 FOR PSTART
C           IP=PRANGE FOR PEND
C
C      DO 310 ICA=1,NCHORD
C      CASCET(ICA,IR,NCOUNT,IP)=DELTAP(ICA)
310      CONTINUE
C      WRITE(5,7503) IERP
7503      FORMAT(' ERROR CODE FROM INVERSION ROUTINE=',I3)
C      WRITE(21,7025)
7025      FORMAT(' OUTPUT FROM CASC: (DELTAP(IQ), IQ=1,NCHORD)')
C      WRITE(21,7032) (DELTAP(IQ), IQ=1,NCHORD)
7032      FORMAT(5X,E12.4)

C
C
C
C
C      320      CONTINUE

C
C      STORE MATRIX OF PRESSURE VALUES ON THE DISK FOR LATER
C      PROCESSING BY OTHER PROGRAMS.

C      CALL OFILE(23,'ROTO')
C      WRITE (23) A
C      WRITE (23) IDATA
C      WRITE (23) RDATA
C      WRITE (23) VGEOM
C      WRITE (23) CASCET

```

ORIGINAL PAGE IS
OF POOR QUALITY

C <MTHEUBALD>ROTORS.FOR,14 wed 23-Sep, 01 9:31AM PAGE 1:3

C
C
C
ENDFILE 23

STOP
END

ORIGINAL PAGE IS
OF POOR QUALITY

PROGRAM INSRCH

Program determines which modes
propagate for the case of inlet
turbulence and controls the
noise computation.


```

PROGRAM INSRCH
  DIMENSION CASCET(8,5,15,5)
  DIMENSION IER(8),IDATA(10)
  DIMENSION RDATA(20),VGEOM(10,7),POWER(2),SPWR(2),RELPR(2)
  DIMENSION NPCJN(4)
  DIMENSION A(72)
  INTEGER PRANGE,PEND,PSTART,PSTEP
  COMPLEX CASCET
  REAL MT,MA

```

```

      DATA(POWER(J),J=1,2)/2*0.0/

```

```

      CALLING PROGRAM FOR INTUR3 TO SEARCH OUT AND CALCULATE
      ALL PROPAGATING MODES AT A GIVEN POSITIVE FREQUENCY.

```

```

      OPEN FILE "ROTO" AND READ INPUT ARRAYS
      INCLUDING MAIN STORAGE MATRIX "CASCET".

```

```

      *****NOTE THAT "ROTO" IS A SEQUENTIAL UNFORMATTED BINARY FILE--

```

```

      ORDER OF STORAGE=A,IDATA,RDATA,VGEOM,CASCET
      *****

```

```

      CALL IFILE(23,"ROTO")
      READ (23) A
      READ (23) IDATA
      READ (23) RDATA
      READ (23) VGEOM
      READ (23) CASCET
      ENDFILE 23

```

```

      WRITE(5,5)
      FORMAT(' USER-ASSIGNED TITLE OF DATA SET FROM FILE "ROTO" IS')
      WRITE(5,6) A
      FORMAT(' ',72A1)
      PSTART=IDATA(5)
      PEND=IDATA(7)
      PSTEP=IDATA(8)
      PRANGE=(PEND-PSTART)/PSTEP+1
      NPCON(1)=PSTART
      NPCON(2)=PEND
      NPCON(3)=PSTEP
      NPCON(4)=PRANGE

```

ORIGINAL PAGE IS
OF POOR QUALITY.

C ENTER NOISE FREQUENCY OF INTEREST(MUST BE POSITIVE FREQUENCY)

C
C SELECT NO. OF RADIAL POSITIONS TO INTERPOLATE PRESSURES
C (ASSUMED THAT NRADNU.GE.NRAD)

C*****

C
C
XMAX=OMEGA*4T/(1.-MA**2)**.5

START WITH PLANE WAVE MODE (0,1). COUNT UP IN N, THEN M UNTIL ALL POSSIBLE HIGHER MODES ARE CUT OFF.

J=1
N=0

ORIGINAL PAGE IS
OF POOR QUALITY

RESTART N COUNT HERE FOR NEW M

N=0

INCREMENT N

N=N+1

MABS=IABS(M)

CALL ANRT (MABS,N,SIGMAR,EB,EC,XMN,IEB,IEC)

IF MODE IS CUT OFF, GO TO 6000

IF(XMN.GE.XMAX) GO TO 6000

WRITE(5,3000)

3000 FORMAT('MODE DATA')

WRITE(5,3001) OMEGA,M,N,XMN

3001 FORMAT('OMEGA=',E10.4,' M=',I3,' N=',I3,' XMN=',E10.4)

IF(XMN.EQ.0.) GO TO 1000

COFFRA=XMAX/XMN

WRITE(5,4000) COFFRA

4000 FORMAT('CUTOFF RATIO FOR MODE=',E10.4)

GO TO 1005

1000 CONTINUE

WRITE(5,4005)

4005 FORMAT('PLANE WAVE MODE: CUTOFF RATIO IS + INFINITE')

1005 CONTINUE

WRITE(5,3002) IEB

3002 FORMAT('SUM OF BESSEL FUNCTION ERROR CODES =',I3)

WRITE(5,3003) IEC

3003 FORMAT('ERROR CODE FOR CONVERGENCE TO ROOT XMN =',I3)

NORMALIZE MODE AMPLITUDE

CALL EIGEN (MABS,SIGMAR,XMN,AMN,BMN,EB,IER)

WRITE(5,3004) AMN,BMN

3004 FORMAT(' AMN =',E16.8,' BMN =',E16.8)
 WRITE(5,3005) IER
 3005 FORMAT(' ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC =',I2)

RDATA(11)=XMN
 RDATA(12)=AMN
 RDATA(13)=BMN
 IDATA(6)=M
 IDATA(7)=N

ORIGINAL PAGE IS
 OF POOR QUALITY

CALL INTURB(IDATA,RDATA,VGEOM,SPWR,CASCET,NPCON)
 POWER(1)=POWER(1)+SPWR(1)
 POWER(2)=POWER(2)+SPWR(2)

DO NOT SWITCH SIGN ON M IF M=0

IF(M.EQ.0) GO TO 20

IDATA(6)=-IDATA(6)

WRITE(5,8300) IDATA(6),IDATA(7),RDATA(8)
 8300 FORMAT('OM=',I5,' N=',I5,' OMEGA=',E10.4)

SWITCH SIGN ON M AND RECALCULATE

CALL INTURB(IDATA,RDATA,VGEOM,SPWR,CASCET,NPCON)
 POWER(1)=POWER(1)+SPWR(1)
 POWER(2)=POWER(2)+SPWR(2)

IDATA(6)=-IDATA(6)

GO TO 20

IF MODE IS CUTOFF, DECIDE WHICH MODE TO TRY NEXT.

IF(N.EQ.1) GO TO 7000

NMAX=N-1
 WRITE(5,6001) NMAX

6001 FORMAT('0LARGEST PROPAGATING N FOR THIS M =',I3)

C
C

J=J+1

C
C
C

INCREMENT M

ORIGINAL PAGE IS
OF POOR QUALITY

M=M+1
GO TO 15

C
C
C

M=1 TO REACH THIS POINT

7000 CONTINUE

C
C

WRITE(5,7001)

7001 FORMAT(' NO MORE PROPAGATING MODES FOR THIS OMEGA')

10 CONTINUE

WRITE(5,9001)

9001 FORMAT(' PROBLEM COMPLETED')

DO 550 JJ=1,2

IF(POWER(JJ).EQ.0.) GO TO 5215

RELPR(JJ)=10.*ALOG10(ABS(POWER(JJ)))

GO TO 550

5215 RELPR(JJ)=1.E+35

550 CONTINUE

IF(RELPR(1).EQ.1.E+35) GO TO 5315

WRITE(5,610) RELPR(1)

GO TO 600

5315 WRITE(5,5610)

5610 FORMAT(' FREQUENCY IS CUT OFF')

600 CONTINUE

610 FORMAT(' RELATIVE POWER SPECTRAL DENSITY LEVEL UPSTREAM=',E10.4)

IF(RELPR(2).EQ.1.E+35) GO TO 5415

WRITE(5,630) RELPR(2)

GO TO 620

5415 WRITE(5,5610)

620 CONTINUE

630 FORMAT(' REL. POWER SPECTRAL DENSITY LEVEL DOWNSTREAM=',E10.4)

STOP

END

PROGRAM INTURB

Program computes the noise
generated by a turbofan rotor
subjected to inlet turbulence.

SUBROUTINE INTURB(IDATA,RDATA,VGEOM,SPWR,CASCET,NPCON)

PROGRAM COMPUTES THE SOUND POWER GENERATED BY A TURBOFAN
ROTOR SUBJECTED TO INLET TURBULENCE. THIS IS A SIMPLIFIED
VERSION SUITABLE FOR VERY SMALL TURBULENCE LENGTH SCALES
IN THE RADIAL DIRECTION

PROGRAM INTERPOLATES IN RADIAL POSITION AND FREQUENCY FROM A
STORED MATRIX OF PRESSURE DISTRIBUTIONS (NAME=CASCET)

DIMENSION VGEOM(10,7),RDATA(20),IDATA(10),XX(6),IERPSI(2),SPWR(2)
DIMENSION BJ(20)
DIMENSION CASCET(8,5,15,5)
DIMENSION PSISTO(30),NPCON(4),RR(30),RRNU(30)
INTEGER P,PSTEP,PRANGE,PSTART,PEND
REAL KMNS,MT,MA,LR,LTHETA,LX
COMPLEX I,DELTAP,QMNS,CASCET
COMPLEX Z,RRS,RRRS,QMNST
COMPLEX Y

C *****
C DIMENSION OF PSISTO AND RRNU MUST BE .GE. NRADNU
C DIMENSION OF RR MUST BE .GE. NRAD
C *****

I=(0.,1.)
PI=3.1415926

NRADNU=IDATA(1)
NBLADE=IDATA(2)
NRAD=IDATA(3)
NCHORD=IDATA(4)
NDAT=IDATA(5)
MM=IDATA(6)
NN=IDATA(7)
OMEGA=RDATA(8)
PRANGE=NPCON(4)
PSTART=NPCON(1)
PEND=NPCON(2)
PSTEP=NPCON(3)
SIGMAR=RDATA(5)

ORIGINAL PAGE IS
OF POOR QUALITY

0300 WRITE(5,8300) MM,NN,OMEGA
FORMAT('MM=',15,' N=',15,' OMEGA=',E10.4)
WRITE(21,8300) MM,NN,OMEGA
WRITE(21,700)

700 FORMAT(' INTURB EXECUTION')
 WRITE(21,7204) NRAD,NCHORD
 7204 FORMAT(' NRAD=',I3,' NCHORD=',I3)

LIST NONDIMENSIONAL RADIAL POSITIONS AVAILABLE IN STORED
 DATA (NEEDED FOR INTERPOLATION)

DO 5 IR=1,NRAD
 R=SIGMAR*(IR-1.)*(1.-SIGMAR)/(NRAD-1.)
 RR(IR)=R
 CONTINUE

ORIGINAL PAGE IS
 OF POOR QUALITY

WRITE(21,6)
 6 FORMAT(' R VALUES FROM STORAGE ARE')
 WRITE(21,8) RR
 8 FORMAT(7E10.4)

MT=RDATA(1)
 MA=RDATA(2)
 SIGMAC=RDATA(4)
 EB=RDATA(9)
 EC=RDATA(10)
 XMN=RDATA(11)
 AMN=RDATA(12)
 BMN=RDATA(13)

INITIALIZE ERROR ACCUMULATOR IN PSI CALCULATIONS
 IER=0

LIST NONDIMENSIONAL RADIAL POSITIONS TO BE USED IN INTERPOLATION

DO 7 IRNU=1,NRADNU
 R=SIGMAR*(IRNU-1.)*(1.-SIGMAR)/(NRADNU-1.)
 RRNU(IRNU)=R

COMPUTE AND STORE MODE SHAPE WEIGHTING AT EACH RADIUS

ARG=XMN*R
 CALL RMODE(MN,ARG,AMN,BMN,PSI,EB,IERPSI)
 PSISTO(IRNU)=PSI
 IER=IER+IERPSI(1)+IERPSI(2)

7 CONTINUE

(+)

C
C

9 WRITE(21,9)
FORMAT(' R VALUES FOR INTERPOLATION ARE')
WRITE(21,8) RRNU
WRITE(21,11)
11 FORMAT(' PSISTO VALUES ARE')
WRITE(21,3) PSISTO

C
C

BETASQ=1.-MA**2
KMNS=((OMEGA*MT)**2-BETASQ*XMN**2)**.5)*ABS(OMEGA)/OMEGA
WRITE(21,7C18) KMNS
7018 FORMAT(' KMNS=',310.4)

C
C
C
C

CHECK TO BE SURE MODE NUMBER M IS IN RANGE OF STORED DATA

IF(MM.LT.0) GO TO 300

C
C
C

FOR POSITIVE M, WANT 0.LE.M.LE.(NBLADE-1)

IF(0.LE.MM.AND.MM.LE.(NBLADE-1)) GO TO 310

C
C
C

IF M POSITIVE BUT OUT OF RANGE, SUBTRACT INTEGER*NBLADE

MTRIAL=MM
NTRIAL=0
320 CONTINUE
NTRIAL=NTRIAL+1
MSUM=MTRIAL-NTRIAL*NBLADE
IF(0.LE.MSUM.AND.MSUM.LE.(NBLADE-1)) GO TO 330
GO TO 320
330 MUSE=MSUM+1
GO TO 340

C
C
C

FOR NEGATIVE M, ADD INTEGER*NBLADE TO M

300 MTRIAL=MM
NTRIAL=0
350 CONTINUE
NTRIAL=NTRIAL+1
MSUM=MTRIAL+NTRIAL*NBLADE
IF(0.LE.MSUM.AND.MSUM.LE.(NBLADE-1)) GO TO 360
GO TO 350
360 MUSE=MSUM+1
GO TO 340

C
C

310 MUSE=MM+1
340 CONTINUE

ORIGINAL PAGE IS
OF POOR QUALITY

341 WRITE(21,341) MM,MUSE
FORMAT(' MM=',I5,' MUSE=',I5)

SEARCH HARMONIC ORDERS FOR FREQUENCY INTERPOLATION

WANT PMIN.LE.OMEGA.LE.PMAX

IF(MM.LT.0) GO TO 400
NUPMIN=PSTART

NUPMAX=PEND
DO 10 P=PSTART,PEND-PSTEP,PSTEP
IF (OMEGA.GE.(1.*P)) NUPMIN=P
CONTINUE
DO 20 P=PEND,PSTART,-PSTEP
IF (OMEGA.LT.(1.*P)) NUPMAX=P
CONTINUE
GO TO 490

ORIGINAL PAGE IS
OF POOR QUALITY

400 CONTINUE

FOR MODE NUMBER M.LT.0 MUST SHIFT FREQUENCY PARAMETER TO
RETRIEVE CASCET DATA.

EQUIV.(OMEGA)=OMEGA+ABS(MM)+MSUM

EQOMEG=OMEGA+ABS(MM)+MSUM
NUPMIN=PSTART
NUPMAX=PEND
DO 410 P=PSTART,PEND-PSTEP,PSTEP
IF(EQOMEG.GE.(1.*P)) NUPMIN=P
CONTINUE
DO 420 P=PEND,PSTART,-PSTEP
IF(EQOMEG.LT.(1.*P)) NUPMAX=P
CONTINUE

490 CONTINUE

CONVERT TO FIND IP PARAMETER OF DATA STORAGE IN CASCET

IP=0
DO 25 P=PSTART,PEND,PSTEP
IP=IP+1
IPP=P
IF (NUPMIN.2Q.IPP) IPMIN=IP
IF (NUPMAX.3Q.IPP) IPMAX=IP
CONTINUE

25

C

```

21      WRITE(21,21) NUPMIN,NUPMAX
      FORMAT(' NUPMIN=',I5,' NUPMAX=',I5)
22      WRITE(21,22) IPMIN,IPMAX
      FORMAT(' IPMIN=',I5,' IPMAX=',I5)

```

C

C

C

```

      KILL PROGRAM IF DESIRED FREQUENCY IS OUT OF RANGE OF DATA
      PSTARF=FLOAT(PSTART)
      PENDF=FLOAT(PEND)
      OMEGAT=OMEGA
      IF (MM.LT.0) OMEGAT=EQOMEG
      IF(PSTARF.LE.OMEGAT.AND.OMEGAT.LE.PENDF) GO TO 343
      WRITE(5,342)
342     FORMAT(' FREQUENCY OUT OF RANGE OF DATA FILE')
      STOP
343     CONTINUE

```

C

C

110

XSIGN=1.

C

C

C

C

111

OMNS=(MT*MA*OMEGA+XSIGN*KMNS)/BETASQ

C

C

C

C

C

C

```

      INITIALIZE VARIABLES
      ISUMR IS ERROR CODE ACCUMULATOR FOR BESSEL WEIGHTING FUNCTION
      PMNS IS RESULT OF DOUBLE INTEGRAL
      SWTR IS WEIGHTING SIGN FUNCTION FOR RADIAL INTEGRATION

```

```

      PMNS=0.
      DELTAR=(1.-SIGMAR)/(NRADN-1)
      ISUMR=0
      IDAT=2

```

C

C

SWTR=-1.

C

C

C

C

C

C

C

C

C

C

C

C

```

      RADIAL POSITION SEARCH FOR INTERPOLATION COORDINATES
      WANT RR(IRMIN).LE.RRNU(IRNU).LE.RR(IRMAX)
      ***NOTE: RR(1)=RRNU(1)
               RR(NRAD)=RRNU(NRADNU)

```

ORIGINAL PAGE IS
OF POOR QUALITY

ORIGINAL PAGE IS
OF POOR QUALITY

```

IF (IRNU.EQ.1) GO TO 50
IF (IRNU.EQ.NRADNU) GO TO 60
IRMIN=1
IRMAX=NRAD
DO 30 IR=1,NRAD-1,1
  IF (RRNU(IRNU).GE.RR(IR)) IRMIN=IR
30  CONTINUE
  DO 40 IR=NRAD,1,-1
    IF (RRNU(IRNU).LT.RR(IR)) IRMAX=IR
40  CONTINUE
GO TO 70
50  CONTINUE
  IRMIN=1
  IRMAX=2
GO TO 70
60  CONTINUE
  IRMIN=NRAD-1
  IRMAX=NRAD
GO TO 70
70  CONTINUE

```

```

WRITE(21,71) IRMIN,IRMAX
71  FORMAT(' IRMIN=',I5,' IRMAX=',I5)
  WRITE(21,72) RR(IRMIN),RRNU(IRNU),RR(IRMAX)
72  FORMAT(' RR(IRMIN=',E10.4,' RRNU(NU=',E10.4,' RR(IRMAX=',E10.4)

```

BLADE GEOMETRY AT RADIAL STATION OF INTEGRATION

```

R=RRNU(IRNU)
IF(R.LE.VGEOM(IDAT,1)) GO TO 201
IDAT=IDAT+1
IF(IDAT.GT.NDAT) IDAT=NDAT
201 DELTA=(R-VGEOM(IDAT,1))/(VGEOM(IDAT,1)-VGEOM(IDAT-1,1))
DO 210 IX=2,3
210 XX(IX-1)=VGEOM(IDAT,IX)+DELTA*(VGEOM(IDAT,IX)-VGEOM(IDAT-1,IX))

```

```

B=XX(1)/2.
CHI=XX(2)
WRITE(21,7010) B,CHI,R
7010 FORMAT(' B=',E10.4,' CHI=',E10.4,' R=',E10.4)

```

```

COSCHI=COS(CHI)
SINCHI=SIN(CHI)

```

```

ZMOD=SIGMAC*B*(GMNS*COSCHI+MM*SINCHI/R)

```

ORIGINAL PAGE IS
OF POOR QUALITY

CHORDWISE INTEGRATION USES BESSEL INTEGRATION METHOD

---CALCULATE BESSEL WEIGHTING FUNCTIONS
BESJ REQUIRES POSITIVE ARGUMENT

X=ABS(ZMOD)
CALL BESJ(X,0,BJ0,EB,IRROR1)
CALL BESJ(X,NCHORD,BJ(NCHORD),EB,IRROR2)
CALL BESJ(X,NCHORD-1,BJ(NCHORD-1),EB,IRROR3)
ISERR=IRROR1+IRROR2+IRROR3
WRITE(21,5400) ZMOD,ISERR
5400 FORMAT(' ZMOD=',E10.4,' ISERR=',I5)
IF(ZMOD.GT.0.) GO TO 5040

C BJ0 IS EVEN FUNCTION, ADJUST SIGN ON OTHERS
BJ(NCHORD)=BJ(NCHORD)*(-1.)**NCHORD

BJ(NCHORD-1)=BJ(NCHORD-1)*(-1.)**(NCHORD-1)

5040 CONTINUE

C USE RECURSION RELATION TO COMPUTE AND STORE BESSEL FUNCTIONS

DO 2080 N=NCHORD-1,2,-1
BJ(N-1)= -BJ(N+1)+2.*N*BJ(N)/ZMOD

2080 CONTINUE

INITIALIZE INTERPOLATION TO GET PRESSURE VALUE FOR THIS
FREQUENCY AND RADIAL POSITION FROM STORED DATA

USE 4 POINT BIVARIATE INTERPOLATION. SEE ABRAMOWITZ AND
STEGUN 25.2.65

NOTE QQ AND PP ARE LESS THAN 1

DETERMINE FRACTIONAL PARTS OF FREQ. AND RADIAL SPACING

PP=(RRNU(IRNU)-RR(IRMIN))/(RR(IRMAX)-RR(IRMIN))
QQ=(OMEGA-NUPMIN)/(NUPMAX-NUPMIN)
IF(MM.LT.0) QQ=(EQOMEG-NUPMIN)/(NUPMAX-NUPMIN)

WRITE(21,912) PP,QQ
912 FORMAT(' PP=',E10.4,' QQ=',E10.4)

QMNS=(0.,0.)

***** BEGIN CHORDWISE INTEGRATION LOOP HERE *****

DO 220 IZ=1,NCHORD

C COMPUTE R SUB S, THE WEIGHTING FUNCTION AT THE CHORDAL

C STATION

NOTE THAT Z=I*IKOUNT BELOW

ORIGINAL PAGE IS
OF POOR QUALITY

RRRS=(0.,0.)

Z=(1.,0.)

DO 5000 IKOUNT=0,NCHORD

BM=1.

IF(IKOUNT.EQ.0.OR.IKOUNT.EQ.NCHORD) BM=0.5

ARGU=IKOUNT*IZ*PI/NCHORD

IF(IKOUNT.GT.0) GO TO 5010

RRS=BM*Z*BJ0

GO TO 5020

5010 CONTINUE

RRS=BM*Z*BJ(IKOUNT)*COS(ARGU)

5020 CONTINUE

Z=Z*I

RRRS=RRRS+RRS

5000 CONTINUE

RRRS=RRRS*2.*PI/NCHORD

BN=1.

IF(IZ.EQ.NCHORD) BN=0.5

INTERPOLATE PRESSURE VALUES IN FREQUENCY AND RADIUS

MCOUNT=MUSE

Y=(1.-PP)*(1.-QQ)*CASCET(IZ,IRMIN,MCOUNT,IPMIN)

Y=Y+PP*(1.-QQ)*CASCET(IZ,IRMAX,MCOUNT,IPMIN)

Y=Y+QQ*(1.-PP)*CASCET(IZ,IRMIN,MCOUNT,IPMAX)

Y=Y+PP*QQ*CASCET(IZ,IRMAX,MCOUNT,IPMAX)

WRITE(21,2) CASCET(IZ,IRMIN,MCOUNT,IPMIN)

WRITE(21,2) CASCET(IZ,IRMAX,MCOUNT,IPMIN)

WRITE(21,2) CASCET(IZ,IRMIN,MCOUNT,IPMAX)

WRITE(21,2) CASCET(IZ,IRMAX,MCOUNT,IPMAX)

2 FORMAT(' CASCET=',2E10.4)

EVALUATE FINITE CHORDWISE SUM TO APPROX. INTEGRAL

QMNST=Y*RRRS*BN

QMNS=QMNS+Y*RRRS*BN

WRITE(21,5030) IZ,QMNST

5030 FORMAT(' IZ=',I5,' QMNST=',2E10.4)

220 CONTINUE

C *****END OF CHORDWISE INTEGRATION LOOP (220) *****

WRITE(21,7022) IRNU,QMNS

7022 FORMAT(' IRNU=',I3,' QMNS=',2E10.4)

8010 CONTINUE
GO TO 8013

8012 CONTINUE
SUMNU=0.

8013 CONTINUE

8015 WRITE(21,8015) SUMNU,P,TURM
FORMAT(' SUMNU=',E10.4,' P=',I5,' TURM=',E10.4)

ORIGINAL PAGE IS
OF POOR QUALITY

FMNS=CB*CC*CD*SUMNU/R

WHTR=1.+SWTR/3.

SWTR=-SWTR

IF(IR.EQ.1.OR.IR.EQ.NRAD) WHTR=WHTR/2.

PMNS=PMNS+WHTR*FMNS*DELTAR*SIGMAC*SIGMAC*2.

WRITE(21,7016) PMNS

7016 FORMAT(' PMNS SUM(R)=',E10.4)

901 CONTINUE

C***** END OF RADIAL INTEGRATION LOOP (901) *****

SMN=((BETAS2*NBLADE)**2)*MA*MT*OMEGA*PMNS/PI/KMNS
SMN=SMN/(1.-SIGMAR**2)/(OMEGA*MT+XSIGN*MA*KMNS)**2
SMN=-XSIGN*SMN

MULTIPLY OUTPUT BY 2 (ADDS +3DB) TO ACCOUNT FOR ENERGY
IN NEGATIVE FREQUENCY

SMN=SMN*2.

RELPR=SMN

IPWR=1

IF(RELPR.EQ.0.) GO TO 915

RELPR=10.*ALOG10(ABS(RELPR))

GO TO 920

915 IPWR=0

920 CONTINUE

IF(XSIGN.LT.0.) GO TO 9000

WRITE(5,3000)

FORMAT('UPSTREAM ')

WRITE(5,8101) GMNS

3000

```

8101  FORMAT(' GAMMA M,N,SB =',E16.8)
      WRITE(5,8102) SMN
8102  FORMAT(' REL. MODAL SOUND POWER SPECTRAL DENSITY=',E10.4)
      WRITE(5,8500) IER
      WRITE(5,5500) ISUMR
8500  FORMAT(' SUM OF ALL ERRORS IN PSI CALCULATIONS =',I5)
      IF(IPWR.EQ.0) GO TO 970
      WRITE(5,3600) RELPRL
      GO TO 980
970   CONTINUE
      WRITE(5,952)
980   CONTINUE
8600  FORMAT(' REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=',E10.4)
      WRITE(21,7200)
7200  FORMAT(' END OF UPSTREAM INTEGRATION')
      XSIGN=-1.
      SPWR(1)=RELPWR
      GO TO 111

```

ORIGINAL PAGE IS
OF POOR QUALITY

C
C***** RETURN TO LINE 111 TO COMPUTE DOWNSTREAM PROPAGATION
C*****

```

C
9000  WRITE(5,8200)
8200  FORMAT('DOWNSTREAM')
      WRITE(5,8201) GMNS
8201  FORMAT(' GAMMA M,N,SB =',E16.8)
      WRITE(5,8202) SMN
8202  FORMAT(' REL. MODAL SOUND POWER SPECTRAL DENSITY=',E10.4)
      WRITE(5,8400) IER
      WRITE(5,5500) ISUMR
5500  FORMAT(' SUM OF ALL ERRORS IN RS CALCULATIONS=',I5)
8400  FORMAT(' SUM OF ALL ERRORS IN PSI CALCULATIONS =',I5)
      IF(IPWR.EQ.0) GO TO 950
      WRITE(5,8500) RELPRL
      GO TO 960
950   CONTINUE
      WRITE(5,952)
952   FORMAT(' SOUND POWER SPECTRAL DENSITY FOR MODE=0/UNEXCITED')
960   CONTINUE
      SPWR(2)=RELPWR
      WRITE(21,7202)
7202  FORMAT(' END OF DOWNSTREAM INTEGRATION')
      RETURN
      END

```


PROGRAM MAINTW

This is a calling program to control the computation of pressure data for the wake turbulence case.

PROGRAM MAINTW
 DIMENSION IDATA(10),RDATA(20),VGEOM(10,7)
 DIMENSION VELOCV(10,2)
 REAL MT,MA,MUV,LX,L2,LTHETA
 INTEGER PSTART,PEND,P,PRANGE,PSTEP
 DATA (IDATA(J),J=1,10)/10*0/
 DATA (RDATA(J),J=1,20)/20*0.0/

ORIGINAL PAGE IS
 OF POOR QUALITY

ROTOR WAKE TURBULENCE-STATOR INTERACTION---MATRIX STORAGE

THIS PROGRAM GROUP CALCULATES AND STORES VECTORS OF
 THE COMPLEX PRESSURE DISTRIBUTION ACROSS THE STATOR VANE.

DATA REQUIRED TO EXECUTE THIS ROUTINE INCLUDE:

1. VANE GEOMETRY
2. ROTOR OPERATING SPEEDS
3. NUMBER OF RADIAL AND CHORDWISE POSITIONS AT WHICH THE
 PRESSURES ARE CALCULATED
4. FREQUENCY RANGE OF INTEREST (EXPRESSED IN TERMS
 OF HARMONIC ORDER OF SHAFT ROTATION).

THE RANGE OF CIRCUMFERENTIAL MODE NUMBER M IS 0 TO NVANE-1.

NCHORD MUST BE NO GREATER THAN 20.

```

1001  FORMAT(G20.8)
      WRITE(5,2001)
2001  FORMAT(' NVANE=')
      READ(5,1001) NVANE
      WRITE(5,2101) NVANE
2101  FORMAT(' NVANE=',I3)
      WRITE(5,2002)
2002  FORMAT(' NBLADE=')
      READ(5,1001) NBLADE
      WRITE(5,2102) NBLADE
2102  FORMAT(' NBLADE=',I3)
      WRITE(5,2003)
2003  FORMAT(' HUB RADIUS DIVIDED BY DUCT RADIUS =')
      READ(5,1001) SIGMAR
      WRITE(5,2103) SIGMAR
2103  FORMAT(' SIGMAR=',E16.8)
      WRITE(5,2004)
2004  FORMAT(' VANE TIP CHORD DIVIDED BY DUCT RADIUS=')
      READ(5,1001) SIGMAC
      WRITE(5,2104) SIGMAC
2104  FORMAT(' SIGMAC=',E16.8)
      WRITE(5,2006)

```

2006 FORMAT(' NDAT =')
READ(5,1001) NDAT
WRITE(5,2106) NDAT
2106 FORMAT(' NDAT=',I3)
WRITE(5,2007)
2007 FORMAT(' VANE GEOMETRY MATRIX INPUT')
WRITE(5,2008)
2008 FORMAT(' FEED MATRIX IN ONE ROW AT A TIME, FROM HUB TO TIP')

ORIGINAL PAGE IS
OF POOR QUALITY

C
C

DO 10 IROW=1,NDAT
WRITE(5,2009) IROW
2009 FORMAT(' ROW=',I3,' R/RDUCT =')
READ(5,1001) VGEOM(IROW,1)
WRITE(5,2010)
2010 FORMAT(' C/CTIP =')
READ(5,1001) VGEOM(IROW,2)
WRITE(5,2011)
2011 FORMAT(' THETA (DEGREES) =')
READ(5,1001) VGEOM(IROW,3)
VGEOM(IROW,3)=VGEOM(IROW,3)*.0174533
10 CONTINUE

C
C
C

WRITE(5,2020)
2020 FORMAT(' VANE GEOMETRY MATRIX IS')
DO 11 IROW=1,NDAT
WRITE(5,2120) (VGEOM(IROW,ICOLMN),ICOLMN=1,3)
2120 FORMAT(' ',7E10.3)
11 CONTINUE

C
C
C
C

WRITE(5,5000)
5000 FORMAT(' TYPE 1 TO INPUT ROTOR WAKE VELOCITY; 0 FOR FREE
1 VORTEX')
READ(5,1001) IVOR
WRITE(5,5010) IVOR
5010 FORMAT(' IVOR=',I3)
IF (IVOR.EQ.0) NVELO=0
IF (IVOR.EQ.0) GO TO 4005

C
C

WRITE(5,3000)
3000 FORMAT(' NUMBER OF RADII FOR SPECIFYING MEAN ROTOR FLOW =')
READ(5,1001) NVELJ
WRITE(5,3002) NVELJ
3002 FORMAT(' NVELJ=',I3)
WRITE(5,3004)
3004 FORMAT(' INPUT MATRIX FOR MEAN ROTOR FLOW')
WRITE(5,3006)

3006 FORMAT(' FEED MATRIX IN ONE ROW AT A TIME, FROM HUB TO TIP')
 DO 4000 IROW=1,NVELO
 WRITE(5,3008) IROW
 3008 FORMAT(' ROW=',I3,' R/RDUCT=')
 READ(5,1001) VELOCV(IROW,1)
 WRITE(5,3012)
 3012 FORMAT(' MEAN CIRCUMFERENTIAL VELOCITY RATIO(U CIRCUM/U
 1 AXIAL)=')
 READ(5,1001) VELOCV(IROW,2)
 4000 CONTINUE

C
 C
 WRITE(5,3014)
 3014 FORMAT(' MEAN ROTOR FLOW VELOCITY MATRIX IS')
 DO 4002 IROW=1,NVELO
 WRITE(5,3016) (VELOCV(IROW,ICOLMN),ICOLMN=1,2)
 3016 FORMAT(' ',2E10.4)
 4002 CONTINUE

C
 C
 4005 CONTINUE

C
 C
 C
 C
 WRITE(5,2030)
 2030 FORMAT(' MT =')
 READ(5,1001) MT
 WRITE(5,2130) MT
 2130 FORMAT(' MT=',E16.8)
 WRITE(5,2031)
 2031 FORMAT(' MA =')
 READ(5,1001) MA
 WRITE(5,2131) MA
 2131 FORMAT(' MA =',E16.8)

ORIGINAL PAGE IS
 OF POOR QUALITY

C
 C
 C
 C
 IF(IVOR.EQ.1) GO TO 6000
 WRITE(5,2032)
 2032 FORMAT(' VYFM/VXM @ R=RDUCT=')
 READ(5,1001) MUV
 WRITE(5,2132) MUV
 2132 FORMAT(' MUV=',E10.4)
 6000 CONTINUE
 IF (IVOR.EQ.1) MUV=0.

C
 C
 C
 WRITE(5,2035)

```
2035  FORMAT(' NUMBER OF RADIAL STATIONS =')
      READ(5,1001) NRAD
      WRITE(5,2135) NRAD
2135  FORMAT(' NRAD=',I4)
      WRITE(5,2036)
2036  FORMAT(' NUMBER OF CHORDWISE STATIONS (.LE.20) =')
      READ(5,1001) NCHORD
      WRITE(5,2136) NCHORD
2136  FORMAT(' NCHORD=',I4)
```

C
C

```
      WRITE(5,100)
100   FORMAT(' START FREQUENCY(HARMONIC NO. OF SHAFT) =')
      READ(5,1001) PSTART
      WRITE(5,110) PSTART
110   FORMAT(' PSTART=',I4)
      WRITE(5,120)
120   FORMAT(' END FREQUENCY(HARMONIC NO. OF SHAFT) =')
      READ(5,1001) PEND
      WRITE(5,130) PEND
130   FORMAT(' P END=',I4)
```

C
C

```
      WRITE(5,140)
140   FORMAT(' FREQUENCY STEP SIZE (HARMONIC ORDERS) =')
      READ(5,1001) PSTEP
      WRITE(5,150) PSTEP
150   FORMAT(' PSTEP=',I4)
      PRANGE=(PEND-PSTART)/PSTEP+1
      IDATA(1)=NVAN3
      IDATA(2)=NBLADE
      IDATA(3)=NRAD
      IDATA(4)=NCHORD
      IDATA(5)=NDAT
      IDATA(6)=PSTART
      IDATA(7)=PEND
      IDATA(8)=PSTEP
      IDATA(9)=IVOR
      IDATA(10)=NVELO
```

ORIGINAL PAGE IS
OF POOR QUALITY

C
C

```
RDATA(1)=MT
RDATA(2)=MA
RDATA(4)=SIGMAC
RDATA(5)=SIGMAR
RDATA(6)=MUV
```

C
C

```
CALL STATOR(IDATA,RDATA,VGEOM,VELOCV)
STOP
END
```

PROGRAM STATOR

Program calculates and stores the pressures generated on a turbofan stator by wake turbulence.

SUBROUTINE STATOR(IDATA,RDATA,VGEOM,VELOCV)

ORIGINAL PAGE IS
OF POOR QUALITY

DIMENSION OF DELTAP=20

DIMENSION JF CASCET=(NCHORD,NRAD,NVANE,PRANGE)

NOTE NCHORD MUST BE NO GREATER THAN 20

DIMENSION DELTAP(20)

DIMENSION VGEOM(10,7),RDATA(20),IDATA(10),XX(6)

DIMENSION CASCET(3,5,11,3)

DIMENSION A(72),VELOCV(10,2)

REAL KB,MR,MA,MT,MYN,MTHETA

COMPLEX I,DELTAP,CASCET

INTEGER PSTART,PEND,P,PRANGE,PSTEP

I=(0.,1.)

PI=3.1415926

NVANE=IDATA(1)

NBLADE=IDATA(2)

NRAD=IDATA(3)

NCHORD=IDATA(4)

NOAT=IDATA(5)

PSTART=IDATA(6)

PEND=IDATA(7)

PSTEP=IDATA(8)

IVOR=IDATA(9)

NVELO=IDATA(10)

WRITE(5,160)

160 FORMAT(' ENTER TITLE FOR DATA FILE(MAX 72 CHARACTERS)')

READ(5,1003) A

1003 FORMAT(72A1)

MT=RDATA(1)

MA=RDATA(2)

SIGMAC=RDATA(4)

SIGMAR=RDATA(5)

IDAT=2

IDOT=2

START LOOPS TO CALL CASC--BEGIN WITH LOOP ON RADIAL
POSITION TO MINIMIZE INTERPOLATION.

DO 300 IX=1,NRAD

DO 308 P=PSTART,PEND,PSTEP
IP=IP+1

ORIGINAL PAGE IS
OF POOR QUALITY

OMEGBC=MT*SIGMAC*B*P

MR=(MA**2+MTHETA**2)**.5

KB=MT/MR*B*SIGMAC*P
SIGMA=-2.*PI*MM/NVANE

H=2.*PI*R/NVANE/SIGMAC/B

ANGLE= -TnETA

WRITE(21,300)
300 FURMAT('0INPUT TO SUBROUTINE CASC')
WRITE(21,302) OMEGBC
302 FORMAT(' OMEGBC=',E10.4)
WRITE(21,304) MR,KB,SIGMA
304 FORMAT(' MR=',E10.4,' KB=',E10.4,' SIGMA=',E10.4)
WRITE(21,306) H,ANGLE,NCHORD
306 FORMAT(' H=',E10.4,' ANGLE=',E10.4,' NCHORD=',I3)

CALL CASC(OMEGBC,MR,KB,SIGMA,H,ANGLE,NCHORD,DELTAP,IERP)

STORE RESULTS OF CASC IN STORAGE MATRIX FOR DISK FILE.
MATRIX POSITION DESCRIPTORS ARE(IN ORDER OF APPEARANCE):
1. CHORDWISE POSITION(TRAILING TO LEADING EDGES)
2. RADIAL POSITION(INNER RADIUS TO OUTER RADIUS)
3. CIRCUMFERENTIAL MODE NUMBER + 1 (M+1)
4. ORDER OF FREQUENCY COMPUTATIONS(FIRST TO LAST)
WITH: IP=1 FOR PSTART
IP=PRANGE FOR PEND

DO 310 ICK=1,NCHORD
CASCET(ICK,IR,MCOUNT,IP)=DELTAP(ICK)


```

310      CONTINUE
        WRITE(5,7500) IERP
7500      FORMAT(' ERROR CODE FROM INVERSION ROUTINE=',I3)
        WRITE(21,7025)
7025      FORMAT(' OUTPUT FROM CASC:(DELTAP(IQ),IQ=1,NCHORD')
        WRITE(21,7002) (DELTAP(IQ),IQ=1,NCHORD)
7002      FORMAT(5X,6E10.4)

```

308 CONTINUE

STORE MATRIX OF PRESSURE VALUES ON THE DISK FOR LATER
PROCESSING BY OTHER PROGRAMS.

```
CALL OPFILE(23,"STAT")
WRITE (23) A
WRITE (23) IDATA
WRITE (23) RDATA
WRITE (23) VGEOM
WRITE (23) VELOCV
WRITE (23) CASCET
```

ENDFILE 23

**STOP
END**

**ORIGINAL PAGE IS
OF POOR QUALITY**

PROGRAM WASXCH

Program determines which modes
propagate for the case of rotor
wake turbulence and controls the
noise computation.

PRECEDING PAGE BLANK NOT FILMED

C

C

C

C

6

C

C

C

i

C

C

C

c

C

C

c.

2

c

C

C

3

1

C

1

—

10

ORIGINAL PAGE IS
OF POOR QUALITY

C
C
C ENTER NOISE FREQUENCY OF INTEREST(MUST BE POSITIVE FREQUENCY)
C

1001 FORMAT(G24.8)
WRITE(5,110)
110 FORMAT(' NOISE FREQUENCY/SHAFT FREQUENCY=')
READ(5,1001) JMEGA
RDATA(1)=JMEGA
115 FORMAT(' JMEGA=',E12.4)
WRITE(5,115) RDATA(1)

C
C SELECT NO. OF RADIAL POSITIONS TO INTERPOLATE PRESSURES
C (ASSUMED THAT NRADNU.GE.NRAD)
C

C*****NOTE: NRADNU MUST BE .LE.30 UNLESS DIMENSION STATEMENTS IN
C "DIFORMS" ARE TO BE MODIFIED
C*****

WRITE(5,120)
120 FORMAT(' NUMBER OF RADIAL POSITIONS FOR ACOUSTIC COMP.=')
READ(5,1201) NRADNU
RDATA(13)=FLOAT(NRADNU)
WRITE(5,130) NRADNU
130 FORMAT(' NRADNU=',14)
WRITE(5,2037)
2037 FORMAT(' ACCURACY OF BESSEL FLS=')
READ(5,1401) EB
WRITE(5,2137) EB
2137 FORMAT(' EB=',E14.4)
WRITE(5,2038)
2038 FORMAT(' ACCURACY OF CONVERGENCE TO ROOT XNN=')
READ(5,1401) EC
WRITE(5,2138) EC
2138 FORMAT(' EC=',E14.4)

C
C ENTER TURBULENCE CHARACTERISTICS
C

ORIGINAL PAGE IS
OF POOR QUALITY

WRITE(5,2033)
2033 FORMAT(' NAME WIDTH=')
READ(5,1401) WIDTH
WRITE(5,2133) WIDTH
2133 FORMAT(' WIDTH=',E14.4)
WRITE(5,2034)
2034 FORMAT(' TURBULENCE INTENSITY(RMS FLUCTUATING U/U BAR)=')
READ(5,1001) EPSN
2134 FORMAT(' EPSN=',E12.4)
WRITE(5,2134) EPSN

C
WRITE(5,6010)
6010 FORMAT(' TURBULENCE LENGTH SCALE IN AXIAL DIRECTION=')
READ(5,1401) LX
WRITE(5,6002) LX

CALL ANRI (MARS,X,SIGMAR,18,20,XM1,123,120)

IF MODE IS CUT OFF, GO TO 6000

IF(XM1.GE.XM1X) GO TO 6722

ORIGINAL PAGE IS
OF POOR QUALITY

```

3000 WRITE(21,3000)
      FORMAT('MODE DATA')
      WRITE(21,3001) OMEGA,M,N,XM1
3001 FORMAT('OMEGA=',E12.4,' M=',13,' N=',13,' XM1=',E10.4)
      IF(XM1.EQ.0.) GO TO 1200
      COEFFA=XM1X/XM1
      WRITE(21,4000) COEFFA
4000 FORMAT('CUTOFF RATIO FOR MODE=',E12.4)
      GO TO 1205
1200 CONTINUE
      WRITE(21,4000)
4005 FORMAT('PLANE WAVE MODE: CUTOFF RATIO IS + INFINITE')
1205 CONTINUE
      WRITE(21,3002) 123
3002 FORMAT('SUM OF BESSEL FUNCTION ERROR CODES =',13)
      WRITE(21,3003) 120
3003 FORMAT('ERROR CODE FOR CONVERGENCE TO ROOT XM1 =',13)
      C
      C NORMALIZE MODE AMPLITUDE
      C
      CALL EIGEN (MARS,SIGMAR,AM1,AM1,BM1,EP,IER)
      C
      C
      WRITE(21,3004) AM1,BM1
3004 FORMAT('AM1 =',E10.8,' BM1 =',E10.8)
      WRITE(21,3005) 122
3005 FORMAT('ERROR CODE FOR BESSEL FNS IN AM1 AND BM1 CALC =',812)
      C
      C
      RDATA(11)=AM1
      RDATA(12)=AM1
      RDATA(13)=BM1
      LDATA(6)=0
      LDATA(7)=0
      C
      C
      CALL WATURN(LDATA,RDATA,VG0UM,VLLUC,SPWR,CASCET,WPCUN,
1 ISUMTU)
      POWER(1)=POWER(1)+SPWR(1)
      POWER(2)=POWER(2)+SPWR(2)

```

```

C
C
C
C DO NOT SWITCH SIGN ON 4 IF M=2
C   IF (4.E4.1) GO TO 20
C   IDATA(5)=-IDATA(5)
C
C   WRITE(21,8302) IDATA(5),IDATA(7),RDATA(3)
8302   FORMAT('M=',I3,' N=',I5,' OMEGA=',E10.4)
C
C SWITCH SIGN ON 4 AND RECALCULATE
C   CALL MATOPB(IDATA,RDATA,VEGOM,VELOCV,SPWR,CASCET,RPCON,
C     1   ISUATD)
C     POWER(1)=POWER(1)+SPWR(1)
C     POWER(2)=POWER(2)+SPWR(2)
C
C   IDATA(5)=-IDATA(5)
C
C   GO TO 20
C
C
C
C IF MODE IS CUTOFF, DECIDE WHICH MODE TO TRY NEXT.
C
8000   IF (4.E4.1) GO TO 7000
C
C   N=MAX=N-1
C   WRITE(21,8001) NMAX
8001   FORMAT('LARGEST PROPAGATING N FOR THIS 4 =',I3)
C
C   J=J+1
C
C INCREMENT N
C
C   M=N+1
C   GO TO 15
C
C
C N=1 TO REACH THIS POINT
7000 CONTINUE

```

ORIGINAL PAGE IS
OF POOR QUALITY

C
C

```
      WRITE(21,7021)
7021  FORMAT(' NO MORE PROPAGATING MODES FOR THIS OMEGA')
10    CONTINUE
      WRITE(5,9021)
9021  FORMAT(' PROBLEM COMPLETED')
      DO 504 JJ=1,2
        IF(POWER(JJ).EQ.0.) GO TO 5215
        RELPR(JJ)=10.*ALOG10(ABS(POWER(JJ)))
        GO TO 557
5215  RELPR(JJ)=1.E+35
550    CONTINUE
        IF(RELPR(1).EQ.1.E+35) GO TO 5315
        WRITE(5,610) RELPR(1)
        GO TO 627
5315  WRITE(5,5510)
5610  FORMAT(' FREQUENCY IS CUT OFF')
600    CONTINUE
512  FORMAT(' RELATIVE POWER SPECTRAL DENSITY LEVEL UPSTREAM=',E13.4)
      IF(RELPR(2).EQ.1.E+35) GO TO 5415
      WRITE(5,630) RELPR(2)
      GO TO 627
5415  WRITE(5,5510)
520    CONTINUE
630  FORMAT(' REL. POWER SPECTRAL DENSITY LEVEL DOWNSTREAM=',E12.4)
      STOP
      END
```

ORIGINAL PAGE IS
OF POOR QUALITY

PROGRAM WATURB

Program computes the sound power
generated by a turbofan *stator*
subjected to wake turbulence.

PRECEDING PAGE BLANK NOT FILMED

SUBROUTINE NATURR(IDATA,RDATA,VGEOM,VELOCV,SPWR,CASCET,NPCON,
1 ISUMTO)

PROGRAM COMPUTES THE SOUND POWER GENERATED BY A TURBOFAN
STATOR SUBJECTED TO INLET TURBULENCE. THIS IS A SIMPLIFIED
VERSION SUITABLE FOR VERY SMALL TURBULENCE LENGTH SCALES
IN THE RADIAL DIRECTION

PROGRAM INTERPOLATES IN RADIAL POSITION AND FREQUENCY FROM A
STORED MATRIX OF PRESSURE DISTRIBUTIONS (NAME=CASCET)

DIMENSION VGEOM(10,7),RDATA(20),IDATA(10),AX(6),IERPSI(2),SPWR(2)
DIMENSION BJ(20)
DIMENSION PSISTO(30),NPCON(4),RR(30),RRNU(30)
DIMENSION VELOCV(10,2)
DIMENSION CASCET(8,5,11,3)
DIMENSION ISUMTO(100),SUMTJT(100,30)
INTEGER P,PSTEP,PRANGE,PSTART,PEND,S1
REAL KMNS,MR,MT,MA,LR,LTHETA,LX,MYM,MTHETA
COMPLEX I,QMNS,A1,CASCET
COMPLEX Z,RRS,RRRS,MMNST
COMPLEX X

C *****
C DIMENSION OF PSISTO AND RRNU MUST BE .GE. NRAONU
C DIMENSION OF RX MUST BE .GE. NRAU
C *****

I=(0,1.)
PI=3.1415926

NRAONU=IFIX(RDATA(15))
NNAME=IDATA(1)
NBLADE=IDATA(2)
NRAU=IDATA(3)
NCHORD=IDATA(4)
NDAT=IDATA(5)
NM=IDATA(6)
NN=IDATA(7)
IVOR=IDATA(9)
NVELO=IDATA(10)
OMEGA=RDATA(8)
PRANGE=NPCON(4)
PSTART=NPCON(1)
PEND=NPCON(2)
PSTEP=NPCON(3)
SIGMA=RDATA(5)

ORIGINAL PAGE IS
OF POOR QUALITY

ORIGINAL PAGE IS
OF POOR QUALITY

C
C

8300 WRITE(5,6320) M4,NN,OMEGA
7204 FORMAT('M=',15,' N=',15,' OMEGA=',E10.4)
FORMAT('NRAD=',13,' NCHORD=',13)

C
C
C
C
C

LIST NONDIMENSIONAL RADIAL POSITIONS AVAILABLE IN STORED
DATA (NEEDED FOR INTERPOLATION)

DO 5 IR=1,NRAD
R=SIGMAR+(IR-1.)*(1.-SIGMAR)/(NRAD-1.)
RR(IR)=R
CONTINUE

C
C
C
C
C
C
C
C
C

FORMAT('R VALUES FROM STORAGE ARE')
FORMAT(7E10.4)

MT=RDATA(1)
MA=RDATA(2)
EPSW=RDATA(3)
SIGNAC=RDATA(4)
MUV=RDATA(6)
WIDTH=RDATA(7)
ED=RDATA(9)
EC=RDATA(10)
XMN=RDATA(11)
AMN=RDATA(12)
BMN=RDATA(13)
LX=RDATA(15)
LR=RDATA(16)
LTHETA=RDATA(17)

C
C
C
C
C
C
C

INITIALIZE APROR CODE ACCUMULATOR IN PSI COMPUTATIONS
IER=2

LIST NONDIMENSIONAL RADIAL POSITIONS TO BE USED IN INTERPOLATION

DO 7 IRNU=1,NRADNU
R=SIGMAR+(IRNU-1.)*(1.-SIGMAR)/(NRADNU-1.)
RRNU(IRNU)=R

C
C
C

COMPUTE AND STORE MODE SHAPE WEIGHTING AT EACH RADIUS

```

C
      ARG=AMN*R
      CALL KMODE(MM,ARG,AMN,BMN,PSI,EB,IERPSI)
      PSISTO(IRNU)=PSI
      IER=IER+IERPSI(1)+IERPSI(2)
7     CONTINUE
C
C
9     FORMAT(' R VALUES FOR INTERPOLATION ARE')
11    FORMAT(' PSISTO VALUES ARE')
C
C     PERFORM SUMMATION OVER TRANSFORMS OF AUTOCORRELATION
C     FUNCTIONS FOR LATER USE. THIS SUMMATION IS A
C     FUNCTION OF MODE NUMBER M AND RADIUS R FOR A GIVEN SET
C     OF INPUT PARAMETERS.
C
C     CHECK TO SEE WHETHER SUM IS AVAILABLE FROM STORAGE
C
      MINDEX=MM+50
      IF(ISUMTO(MINDEX).EQ.1) GO TO 6040
C
C     MAKE SURE STORAGE LIMITS ARE NOT EXCEEDED
C
      IF(MM.GT.49) WRITE(5,5010)
6010  FORMAT(' MODE NUMBER M EXCEEDS STORAGE OF MATRIX SUMTOT')
      IF(MM.GT.49) STOP
C
C     COMPUTE SUMMATION AS A FUNCTION OF R AND STORE IN SUMTOT
C
      DO 6020 IRNU=1,NRADNU
      K=KRNU(IRNU)
      SUMTOT(MINDEX,IRNU)=0.
C
C     LIMITS ON DOUBLE SUM ADAPT TO PHYSICAL PARAMETERS
C
      MM1MAX=INT(23.*R/NBLADE/WIDTH)
      MM1MAX=INT(1./NVANE*(16.*R/LTHETA+MM1MAX*NBLADE+20.))
      DO 6002 MM1=-MM1MAX,MM1MAX
      FARG=MM1*NBLADE*WIDTH/R
      PHIARG=MT*LX/4A*(OMEGA+MM1*NBLADE)
      TERM1=PHIXHT(PHIARG)*(ABS(PHAT(FARG)))**2
      DO 6003 MM1=-MM1MAX,MM1MAX
      THEARG=((MM1*NVANE)-(MM1*NBLADE)-MM)*LTHETA/R
      TURM1=TERM1*PHITHE(THEARG)
      SUMTOT(MINDEX,IRNU)=SUMTOT(MINDEX,IRNU)+TURM1
6000  CONTINUE
      WRITE(21,6015) MM,OMEGA,R,SUMTOT(MINDEX,IRNU)
6015  FORMAT(' M=',I5,' OMEGA=',E10.4,' R=',E10.4,' SUMTOT=',E10.4)
C
C
6020  CONTINUE
      ISUMTO(MINDEX)=1

```

ORIGINAL PAGE IS
OF POOR QUALITY

C
6040 CONTINUE

ORIGINAL PAGE IS
OF POOR QUALITY

BETASQ=1.-MA**2
KMNS=((OMEGA*MT)**2-3BETASQ*XMN**2)**.5)*ABS(OMEGA)/OMEGA
WRITE(21,7010) KMNS
7010 FORMAT(' KMNS=',310.4)

C
C
C CHECK TO BE SURE MODE NUMBER M IS IN RANGE OF STORED DATA

C IF(MM.LT.0) GO TO 300

C FOR POSITIVE M, WANT 0.LE.M.LE.(NVANE-1)

C IF(0.LE.MM.AND.MM.LE.(NVANE-1)) GO TO 310

C IF M POSITIVE BUT OUT OF RANGE, SUBTRACT INTEGER*NVANE

C MTRIAL=MM

C NTRIAL=0

320 CONTINUE

C NTRIAL=NTRIAL+1

C MSUM=MTRIAL-NTRIAL*NVANE

C IF(0.LE.MSUM.AND.MSUM.LE.(NVANE-1)) GO TO 330

C GO TO 320

330 MUSE=MSUM+1

C GO TO 340

C FOR NEGATIVE M, ADD INTEGER*NVANE TO M

300 MTRIAL=MM

C NTRIAL=0

350 CONTINUE

C NTRIAL=NTRIAL+1

C MSUM=MTRIAL+NTRIAL*NVANE

C IF(0.LE.MSUM.AND.MSUM.LE.(NVANE-1)) GO TO 360

C GO TO 350

360 MUSE=MSUM+1

C GO TO 340

C 310 MUSE=MM+1

C 340 CONTINUE

C 341 FORMAT(' MM=',I5,' MUSE=',I5)

C
C KILL PROGRAM IF DESIRED FREQUENCY IS OUT OF RANGE
C OF STORED DATA

```

C
      PSTARF=FLOAT(PSTART)
      PENDF=FLOAT(PEND)
      IF(PSTARF.LE.OMEGA.AND.JMEGA.LE.PENDF) GO TO 343
      WRITE(5,342)
342  FORMAT(' FREQUENCY OUT OF RANGE OF DATA')
      STOP
343  CONTINUE

C
C
C SEARCH HARMONIC ORDERS FOR FREQUENCY INTERPOLATION
C
C WANT PMIN.LE.OMEGA.LE.PMAX
C
      NUPMIN=PSTART
      NUPMAX=PEND
      DO 10 P=PSTART,PEND-PSTEP,PSTEP
      IF (OMEGA.GE.(1.*P)) NUPMIN=P
10   CONTINUE
      DO 20 P=PEND,PSTART,-PSTEP
      IF (OMEGA.LT.(1.*P)) NUPMAX=P
20   CONTINUE

C
C
C
C
C CONVERT TO FIND IP PARAMETER OF DATA STORAGE IN CASSET
C
      IP=0
      DO 25 P=PSTART,PEND,PSTEP
      IP=IP+1
      IPP=P
      IF (NUPMIN.EQ.IPP) IPMIN=IP
      IF (NUPMAX.EQ.IPP) IPMAX=IP
25   CONTINUE

C
21   FORMAT(' NUPMIN=',I5,' NUPMAX=',I5)
22   FORMAT(' IPMIN=',I5,' IPMAX=',I5)

C
C
C
110  XSIGN=1.
C
C***** RETURN TO LINE (111) TO REPEAT FOR DOWNSTREAM
C      PROPAGATION *****
C
111  GMNS=(NT*MA*OMEGA+XSIGN*K4NS)/BETASQ
C
C

```

ORIGINAL PAGE IS
OF POOR QUALITY

C INITIALIZE VARIABLES

C ISUMR IS ERROR CODE ACCUMULATOR FOR BESSEL WEIGHTING FUNCTION
C **S

C PMNS IS RESULT OF DOUBLE INTEGRAL

C S*IR IS WEIGHTING SIGN FUNCTION IN RADIAL INTEGRATION

C PMNS=0.

C DELTAR=(1.-SIGMAR)/(NRADNJ-1)

C ISUMR=0

C IDOT=2

C IDAT=2

C S*IR=-1.

C *****START RADIAL INTEGRATION LOOP HERE *****

C DO 901: IRNU=1,NRADNU

C RADIAL POSITION SEARCH FOR INTERPOLATION COORDINATES

C WANT RR(IRMIN).LE.RRNU(IRNU).LE.RR(IRMAX)

C ***NOTE: RR(1)=RRNU(1)

C RR(NRAD)=RRNU(NRADNU)

C IF (IRNU.EQ.1) GO TO 50

C IF (IRNU.EQ.NRADNU) GO TO 60

C IRMIN=1

C IRMAX=NRAD

C DO 30 IR=1,NRAD-1,1

C IF (RRNU(IRNU).GE.RR(IR)) IRMIN=IR

30 CONTINUE

C DO 40 IR=NRAD,1,-1

C IF (RRNU(IRNU).LT.RR(IR)) IRMAX=IR

40 CONTINUE

C GO TO 70

50 CONTINUE

C IRMIN=1

C IRMAX=2

C GO TO 70

60 CONTINUE

C IRMIN=NRAD-1

C IRMAX=NRAD

C GO TO 70

70 CONTINUE

ORIGINAL PAGE IS
OF POOR QUALITY

```

71      FORMAT(' IRMIN=',I5,' IRMAX=',I5)
72      FORMAT(' RR(IRMIN=',E10.4,' RRNU(NU=',E10.4,' RR(IRMAX=',E10.4)
C
C
C      BLADE GEOMETRY AT RADIAL STATION OF INTEGRATION
      R=RRNU(IRNU)
      IF(R.LE.VGEOM(IDAT,1)) GO TO 201
      IDAT=IDAT+1
      IF(IDAT.GT.NDAT) IDAT=NDAT
201     DELTA=(R-VGEOM(IDAT,1))/(VGEOM(IDAT,1)-VGEOM(IDAT-1,1))
      DO 210 IX=2,3
210     XX(IX-1)=VGEOM(IDAT,IX)+DELTA*(VGEOM(IDAT,IX)-VGEOM(IDAT-1,IX))
C
C
      B=XX(1)/2.
      THETA=XX(2)
      WRITE(21,7010) B,THETA,R
7010    FORMAT(' B=',E10.4,' THETA=',E10.4,' R=',E10.4)
C
C
C
      COSTHE=COS(THETA)
      SINTE=SIN(THETA)
C
C
      IF (IVOR.EQ.0) GO TO 4020
C
C
C      INTERPOLATE TO GET MEAN CIRCUMFERENTIAL MACH NUMBERS AT THIS R
C
      IF (R.LE.VELOCV(IDOT,1)) GO TO 4001
      IDOT=IDOT+1
      IF (IDOT.GT.NVELO) IDOT=NVELO
4001    DELTA=(R-VELOCV(IDOT,1))/(VELOCV(IDOT,1)-VELOCV(IDOT-1,1))
      XVEL=VELOCV(IDOT,2)+DELTA*(VELOCV(IDOT,2)-VELOCV(IDOT-1,2))
      MTHETA=XVEL*MA
C
4015    FORMAT(' R=',E10.4,' MTHETA=',E10.4)
C
4020    CONTINUE
C
C
C      MYM IS CIRCUMFERENTIAL MACH NUMBER OF WAKE IMPINGING ON STATOR
C
      MYM=MT*R-MA*MOV/R
      IF (IVOR.EQ.1, MYM=MT*R-MTHETA
      IF (IVOR.EQ.0) MTHETA=MA*MOV/R

```

ORIGINAL PAGE IS
OF POOR QUALITY

C
C COMPUTE R SUB S, THE WEIGHTING FUNCTION AT THE CHORDAL
C STATION

C NOTE THAT Z=I*IKOUNT BSLON

C
C RRRS=(0.,0.)
C Z=(1.,0.)
C DO 5000 IKOUNT=0,NCHORD
C BM=1.
C IF (IKOUNT.EQ.0.OR.IKOUNT.EQ.NCHORD) BM=0.5
C ARGU=IKOUNT*IZ*PI/NCHORD
C IF (IKOUNT.GT.0) GO TO 5010
C RRS=BM*Z*BJ0
C GO TO 5020

5010 CONTINUE
C RRS=BM*Z*BJ(IKOUNT)*COS(ARGU)

5020 CONTINUE
C Z=Z*I
C RRRS=RRRS+RRS

5000 CONTINUE

C
C RRRS=RRRS*2.*PI/NCHORD
C BN=1.
C IF (IZ.EQ.NCHORD) BN=0.5

C
C
C INTERPOLATE PRESSURE VALUES IN FREQUENCY AND RADIUS

C
C MCOUNT=MUSE
C Y=(1.-PP)*(1.-QQ)*CASCET(IZ,IRMIN,MCOUNT,IPMIN)
C Y=Y+PP*(1.-QQ)*CASCET(IZ,IRMAX,MCOUNT,IPMIN)
C Y=Y+QQ*(1.-PP)*CASCET(IZ,IRMIN,MCOUNT,IPMAX)
C Y=Y+PP*QQ*CASCET(IZ,IRMAX,MCOUNT,IPMAX)

C
2 FORMAT(' CASCET=',2E10.4)

C
C EVALUATE FINITE CHORDWISE SUM TO APPROX. INTEGRAL

C
C QMNST=Y*RRRS*BN
C QMNS=QMNS+Y*RRRS*BN
5030 FORMAT(' IZ=',I5,' QMNST=',2E10.4)
220 CONTINUE

C
C *****END OF CHORDWISE INTEGRATION LOOP (220) *****

C
7022 FORMAT(' IRNU=',I3,' QMNS=',2E10.4)

C
C
C ISUMR=ISUMR+ISERR

7021 CONTINUE

ORIGINAL PAGE IS
OF POOR QUALITY

CA=MM*COSTHE/R+GMNS*SINTHE
CB=(CA*PS(UMNS)*PSISTO(IRNU)*CA*8)**2
CD=((MT*R)**2+1.)*.5

ORIGINAL PAGE IS
OF POOR QUALITY

FMNS=CB*CD*SUNTJT(MINDEX,IRNU)/(R**2)/COSCHI

WHTR=1.+SWTR/3.
SWTR=-SWTR
IF(IR.EQ.1.OR.IR.EQ.NRAD) WHTR=WHTR/2.

PMNS=PMNS+WHTR*FMNS*DELTA/R
7016 FORMAT(' PMNS SUM(R)=',E10.4)
901 CONTINUE

C***** END OF RADIAL INTEGRATION LOOP (901) *****

CC=LR*LIHETA*LX*(EPS*#WIDTH)**2

SMN=((BETASQ*NBLEAD*NVANE)**2)*MT*OMEGA*PMNS/KMNS*MA**3
SMN=SMN/(1.-SIGMAR**2)/(OMEGA*MT*XSIGV*MA*KMNS)**2
SMN=SMN*CC*SIGMAC*SIGMAC*(-XSIGN)/32./(PI**4)

MULTIPLY OUTPUT BY 2 (ADDS +3DB) TO ACCOUNT FOR ENERGY
IN NEGATIVE FREQUENCY
SMN=SMN*2.

RELPR=SMN
IPWR=1
IF(RELPR.EQ.0.) GO TO 915
RELPR=10.*ALJG10(ABS(RELPR))
GO TO 920
915 IPWR=0
920 CONTINUE

IF(XSIGN.LT.0.) GO TO 9000

WRITE(5,3000)

```

3000  FORMAT('UPSTREAM ')
8101  FORMAT(' GAMMA M,N,SB =',E16.8)
      WRITE(21,8102) SMN
8102  FORMAT(' REL. MODAL SOUND POWER SPECTRAL DENSITY=',E10.4)
      WRITE(21,8500) IER
      WRITE(21,5500) ISUMR
8500  FORMAT(' SUM OF ALL ERRORS IN PSI CALCULATIONS =',I5)
      IF(IPWR.EQ.0) GO TO 970
      WRITE(5,8600) RELPRL
      GO TO 980
970   CONTINUE
      WRITE(5,952)
980   CONTINUE
8600  FORMAT(' REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=',E10.4)
      WRITE(21,7200)
7200  FORMAT(' END OF UPSTREAM INTEGRATION')
      XSIGN=-1.
      SPWR(1)=RELPWR
      GO TO 111

```

C
C***** RETURN TO LINE 111 TO COMPUTE DOWNSTREAM PROPAGATION
C*****

```

C
9000  WRITE(5,8200)
8200  FORMAT('DOWNSTREAM')
8201  FORMAT(' GAMMA M,N,SB =',E16.8)
      WRITE(21,8202) SMN
8202  FORMAT(' REL. MODAL SOUND POWER SPECTRAL DENSITY=',E10.4)
      WRITE(21,8400) IER
      WRITE(21,5500) ISUMR
5500  FORMAT(' SUM OF ALL ERRORS IN RS CALCULATIONS=',I5)
8400  FORMAT(' SUM OF ALL ERRORS IN PSI CALCULATIONS =',I5)
      IF(IPWR.EQ.0) GO TO 950
      WRITE(5,8600) RELPRL
      GO TO 960
950   CONTINUE
      WRITE(5,952)
952   FORMAT(' SOUND POWER SPECTRAL DENSITY FOR MODE=0/UNEXCITED')
960   CONTINUE
      SPWR(2)=RELPWR
      WRITE(21,7202)
7202  FORMAT(' END OF DOWNSTREAM INTEGRATION')
      RETURN
      END

```

ORIGINAL PAGE IS
OF POOR QUALITY

SUBROUTINE ANRT

Program finds the roots of the
boundary value equation for an
annular duct.

PRECEDING PAGE BLANK NOT FILMED

(+)

C
C
C
C
C
C
C
C
C
C
C
C
C
C
C

.....

SUBROUTINE ANRT(M,N,S,EB,EC,XMN,IEB,IEC)

(AN)NULAR FUNCTION (R)OJ(T)

PURPOSE

START WITH A GUESS SOLUTION FOR XM1
AND GET A BETTER VALUE FOR XM1.

GUESS EACH HIGHER ORDER ROOT FROM

$XM(N+1) = XMN + 3.14159$

AND THEN REFINES IT TO GET THE (M,N)

ROOT TO : $F = P(JS*Y - YS*J) = 0$

ORIGINAL PAGE IS
OF POOR QUALITY

.....

IF(M.EQ.0.AND.N.EQ.1) GO TO 6

$XMN = M - 3.14159$

DO 5 NN=1,N

$DX = .31415$

$IS = (-1)**(NN+1)$

$X = XMN + 3.14159$

$J = 1$

CALL ANFU(M,X,S,EB,F,IEB)

$DX = -ISIG(F*IS)*DX$

$TE = F$

1 IF (ABS(F) .LE. EC) GO TO 3
IF (J .GT. 100) GO TO 2

$X = X + DX$

CALL ANFJ(M,X,S,EB,F,IEB)

IF ((F*TE) .LT. 0.) $DX = -DX/2.$

$J = J + 1$

$TE = F$

GO TO 1

2 IEC = 1
GO TO 4

3 IEC = 0

4 $XMN = X$

5 CONTINUE

RETURN

6 CONTINUE

IEB=0

IEC=0

$XMN=0.$

RETURN

END

-L

(+)

.....
SUBROUTINE ANFU(M,X,S,EB,F,IEB)

(AN)NULAR (?U)NCTION

ORIGINAL PAGE IS
OF POOR QUALITY

PURPOSE

EVALUATE THE DETERMINANT $F = P(JS*Y - YS*J)$
.....

IF (M .NE. 0) GO TO 1
CALL BESJ(X,1,ZJ ,EB ,IE3)
CALL BESJ(S*X,1,ZJS ,EB ,IE4)
CALL BESY(X,1,ZY , IE7)
CALL BESY(S*X,1,ZYS , IE8)
IEB = IE3+IE4+IE7+IE8
GO TO 2

C
1 CALL BESJ(X,M-1,BJM ,EB ,IE1)
CALL BESJ(S*X,M-1,BJMS,EB ,IE2)
CALL BESJ(X,M+1,BJP ,EB ,IE3)
CALL BESJ(S*X,M+1,BJPS,EB ,IE4)
ZJ = .5*(BJM -BJP)
ZJS = .5*(BJMS-BJPS)
CALL BESY(X,M-1,BYM , IE5)
CALL BESY(S*X,M-1,BYMS, IE6)
CALL BESY(X,M+1,BYP , IE7)
CALL BESY(S*X,M+1,BYPS, IE8)
ZY = .5*(BYM -BYP)
ZYS = .5*(BYMS-BYPS)
IEB = IE1+IE2+IE3+IE4+IE5+IE6+IE7+IE8

C
2 F = ZJS*ZY - ZJ*ZYS
RETURN
END
~L

SUBROUTINE BESJ

ORIGINAL PAGE IS
OF POOR QUALITY

PURPOSE

COMPUTE THE J BESSEL FUNCTION FOR A GIVEN ARGUMENT AND ORDER

USAGE

CALL BESJ(X,N,BJ,D,IER)

DESCRIPTION OF PARAMETERS

X -THE ARGUMENT OF THE J BESSEL FUNCTION DESIRED

N -THE ORDER OF THE J BESSEL FUNCTION DESIRED

BJ -THE RESULTANT J BESSEL FUNCTION

D -REQUIRED ACCURACY

IER-RESULTANT ERROR CODE WHERE

IER=0 NO ERROR

IER=1 N IS NEGATIVE

IER=2 X IS NEGATIVE OR ZERO

IER=3 REQUIRED ACCURACY NOT OBTAINED

IER=4 RANGE OF N COMPARED TO X NOT CORRECT (SEE REMARKS)

REMARKS

N MUST BE GREATER THAN OR EQUAL TO ZERO, BUT IT MUST BE
LESS THAN $20+10*X-X^{2/3}$ FOR X LESS THAN OR EQUAL TO 15 $90+X/2$ FOR X GREATER THAN 15

SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED

NONE

METHOD

RECURRENCE RELATION TECHNIQUE DESCRIBED BY H. GOLDSTEIN AND
R.M. THALER, "RECURRENCE TECHNIQUES FOR THE CALCULATION OF
BESSEL FUNCTIONS", M.T.A.C., V.13, PP.102-108 AND I.A. STEGUN
AND M. ABRAMOWITZ, "GENERATION OF BESSEL FUNCTIONS ON HIGH
SPEED COMPUTERS", M.T.A.C., V.11, 1957, PP.255-257

SUBROUTINE BESJ(X,N,BJ,D,IER)

BJ=.0

IF (X .NE. 0.) GO TO 9

IER = 0

IF (N .EQ. 0) BJ = 1.

RETURN

C

```
9      IF(N)10,20,20
10     IER=1
      RETURN
20     IF(X)30,30,31
30     IER=2
      RETURN
31     IF(X-15.)32,32,34
32     NTEST=20.+10.*X-X** 2/3
      GO TO 36
34     NTEST=90.+X/2.
36     IF(N-NTEST)40,38,38
38     IER=4
      RETURN
40     IER=0
      N1=N+1
      MPREV=.0
```

ORIGINAL PAGE IS
OF POOR QUALITY

C

C

C

```
      COMPUTE STARTING VALUE OF M
      IF(X-5.)50,50,60
50     MA=X+6.
      GO TO 70
60     MA=1.4*X+60./X
70     MB=N+IFIX(X)/4+2
      MZERO=MAX0(MA,MB)
```

C

C

C

```
      SET UPPER LIMIT OF M
      MMAX=NTEST
100    DO 190 M=MZERO,MMAX,3
```

C

C

C

```
      SET F(M),F(M-1)
      FM1=1.0E-28
      FM=.0
      ALPHA=.0
      IF(M-(M/2)*2)120,110,120
110    JT=-1
      GO TO 130
120    JT=1
130    M2=M-2
      DO 160 K=1,M2
      MK=M-K
      BMK=2.*FLOAT(MK)*FM1/X-FM
      FM=FM1
      FM1=BMK
      IF(MK-N-1)150,140,150
140    BJ=BMK
150    JT=-JT
      S=1+JT
```

C <MTHEOBALD>ANRT.FOR;3 Mon 14-Jan-88 6:31PM

PAGE 4:2

160 ALPHA=ALPHA+BMK*S
BMK=2.*FM1/X-FM
IF(N)180,170,180
170 BJ=BMK
180 ALPHA=ALPHA+BMK
BJ=BJ/ALPHA
IF(ABS(BJ-BPREV)-ABS(D*BJ))200,200,190
190 BPREV=BJ
IER=3
200 RETURN
END

ORIGINAL PAGE IS
OF POOR QUALITY

.....
SUBROUTINE BESY

PURPOSE

COMPUTE THE Y BESSEL FUNCTION FOR A GIVEN ARGUMENT AND ORDER

USAGE

CALL BESY(X,N,BY,IER)

DESCRIPTION OF PARAMETERS

X -THE ARGUMENT OF THE Y BESSEL FUNCTION DESIRED

N -THE ORDER OF THE Y BESSEL FUNCTION DESIRED

BY -THE RESULTANT Y BESSEL FUNCTION

IER-RESULTANT ERROR CODE WHERE

IER=0 NO ERROR

IER=1 N IS NEGATIVE

IER=2 X IS NEGATIVE OR ZERO

IER=3 BY HAS EXCEEDED MAGNITUDE OF 10**70

REMARKS

VERY SMALL VALUES OF X MAY CAUSE THE RANGE OF THE LIBRARY
FUNCTION ALSO TO BE EXCEEDED

X MUST BE GREATER THAN ZERO

N MUST BE GREATER THAN OR EQUAL TO ZERO

SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED

NONE

METHOD

RECURRENCE RELATION AND POLYNOMIAL APPROXIMATION TECHNIQUE
AS DESCRIBED BY A.J.M.HITCHCOCK, "POLYNOMIAL APPROXIMATIONS
TO BESSEL FUNCTIONS OF ORDER ZERO AND ONE AND TO RELATED
FUNCTIONS", M.T.A.C., V.11,1957,PP.86-88, AND G.N. WATSON,
"A TREATISE ON THE THEORY OF BESSEL FUNCTIONS", CAMBRIDGE
UNIVERSITY PRESS, 1958, P. 62.....
SUBROUTINE BESY(X,N,BY,IER)

CHECK FOR ERRORS IN N AND X

IF(N)180,10,10

10 IER=0

IF(X)190,190,20

BRANCH IF X LESS THAN OR EQUAL 4

20 IF(X-4.0)40,40,30

C
C
C COMPUTE Y0 AND Y1 FOR X GREATER THAN 4ORIGINAL PAGE IS
OF POOR QUALITY

30 T1=4.0/X
T2=T1*T1
P0=((((-0.0000037043*T2+.0000173565)*T2-.0000487613)*T2
1 +.00017343)*T2-.001753062)*T2+.3989423
Q0=((((-0.0000032312*T2-.0000142070)*T2+.0000342468)*T2
1 -.00000869791)*T2+.0004564324)*T2-.01246594
P1=((((-0.0000042414*T2-.0000200920)*T2+.0000580759)*T2
1 -.000223203)*T2+.002921825)*T2+.3989423
Q1=((((-0.0000035594*T2+.00001622)*T2-.0000398708)*T2
1 +.0001064741)*T2-.0005390400)*T2+.03740084
A=2.0/SQRT(X)
B=A*T1
C=X-.7853982
Y0=A*P0*SIN(C)+B*Q0*COS(C)
Y1=-A*P1*COS(C)+B*Q1*SIN(C)
GO TO 90

C
C
C COMPUTE Y0 AND Y1 FOR X LESS THAN OR EQUAL TO 4

40 XX=X/2.
X2=XX*XX
T=ALOG(XX)+.5772157
SUM=0.
TERM=T
Y0=T
DO 70 L=1,15
IF(' -1)50,60,50
50 SUM=SUM+1./FLOAT(L-1)
60 FL=L
TS=T-SUM
TERM=(TERM*(-X2)/FL**2)*(1.-1./(FL*TS))
70 Y0=Y0+TERM
TERM = XX*(T-.5)
SUM=0.
Y1=TERM
DO 80 L=2,16
SUM=SUM+1./FLOAT(L-1)
FL=L
FL1=FL-1.
TS=T-SUM
TERM=(TERM*(-X2)/(FL1*FL))*((TS-.5/FL)/(TS+.5/FL1))
80 Y1=Y1+TERM
PI2=.6366198
Y0=PI2*Y0
Y1=-PI2/X+PI2*Y1

C
C
C CHECK IF ONLY Y0 OR Y1 IS DESIRED

90 IF(N-1)100,100,130

C
C RETURN EITHER Y0 OR Y1 AS REQUIRED
C

100 IF(N)110,120,110

110 BY=Y1

GO TO 170

120 BY=Y0

GO TO 170

C
C PERFORM RECURRENCE OPERATIONS TO FIND YN(X)
C

130 YA=Y0

YB=Y1

K=1

140 T=FLOAT(2*K)/X

YC=T*YB-YA

IF(ABS(YC)-1.7E33)145,145,141

141 IER=3

RETURN

145 K=K+1

IF(K-N)150,160,150

150 YA=YB

YB=YC

GO TO 140

160 BY=YC

170 RETURN

180 IER=1

RETURN

190 IER=2

RETURN

END

-L

ORIGINAL PAGE 13
OF POOR QUALITY

SUBROUTINE CASC

Program computes the complex
pressure distribution across
a blade chord for incident
turbulence.

PRECEDING PAGE BLANK NOT FILMED

SUBROUTINE EIGEN

Program computes the weighting
factors for the eigen functions
(mode shapes).

PRECEDING PAGE BLANK NOT FOLLOWS

```

SUBROUTINE EIGEN(MM,STGMAR,XMM,MN,BMN,D,IER)
DIMENSION IER(8)
IF(MM.EQ.0.) GO TO 22
N=MN
IF(M.LT.0) M=-N
MMINUS=IABS(N-1)
MPLUS=N+1
XMMHUB=XMM*SIGMAR
S=STGMAR**2
CALL PESJ (XMM,M,BJM,D,IER(1))
CALL PESY (XMM,M,BYM,IER(2))
CALL PESJ (XMMHUB,M,BJMH,D,IER(3))
CALL PESY (XMMHUB,M,BYMH,IER(4))
CALL PESJ (XMM,MPLUS,BJMP,D,IER(5))
CALL PESY (XMM,MPLUS,BYMP,IER(6))
CALL PESJ (XMM,MMINUS,BJMM,D,IER(7))
CALL PESY (XMM,MMINUS,BYMM,IER(8))
IF(M.GT.0) GO TO 100
BJMV=-BJMV
BYMV=-BYMV
100 BJPRIM=(BJMV-BJMP)/2.
BYPRIM=(BYMV-BYMP)/2.
IF(ABS(BJPRIM).LT.ABS(BYPRIM)) GO TO 10
AMN=-BYPRIM/BJPRIM
BMN=1.
GO TO 20
10 AMN=1.
BMN=-BJPRIM/BYPRIM
20 PART1=(1.-(MM/XMM)**2)*(AMN*BJM+BMN*BYM)**2/(1.-S)
PART2=(S-(M**2/XMM)**2)*(AMN*BJMH+BMN*BYMH)**2/(1.-S)
FACTOR=(PART1-PART2)**.5
AMN=AMN/FACTOR
BMN=BMN/FACTOR
RETURN
22 CONTINUE
AMN=1.
BMN=0.
DO 24 J=1,8
24 IER(J)=0
RETURN
END

```

ORIGINAL PAGE IS
OF POOR QUALITY

SUBROUTINE EPSD

Program yields the inlet RMS
turbulence intensity.

ORIGINAL PAGE IS
OF POOR QUALITY

SUBROUTINE FHAT

Program computes the Fourier
transform of the spatial
distribution of wake turbulence.

PRECEDING PAGE BLANK NOT FILMED

FUNCTION FHAT(FARG)

C
C FUNCTION YIELDS THE FOURIER TRANSFORM OF THE SPATIAL
C DISTRIBUTION OF WAKE TURBULENCE VELOCITY FOR
C SUBROUTINE OUTURD

C DATA PI/3.14159/

C
C NEED SWITCH TO AVOID UNDERFLOW ON EXPONENTIATION :
C RANGE IS E+-38.

C
C A=(FARG**2)/4./PI
C IF(A.GT.87.) GO TO 10
C B=EXP(-A)
C GO TO 20
10 B=0.
20 CONTINUE
C FHAT=B
C RETURN
C END

ORIGINAL PAGE IS
OF POOR QUALITY

SUBROUTINE KERNEL

Program computes the kernel
of the Green's function.

```

SUBROUTINE KERNEL(X,K,GAMMA,MR,H1,H2,ERROR,CKF)
REAL K,MR
COMPLEX I,CKF,AN,ANP,ANM,RN,RJOT
RN(AN)=BETAR**2*H2/(2.*D**2)*(AN**2-K**2)*CEXP(I*(AN+K*MR)
1 *X)/((AN-GN*H1/D**2)*(AN+K/MR))
DATA I/(0.,1.)/,PI/3.14159/,XMIN/.001/
BETAR=SQRT(1.-MR**2)
IF(ABS(X).GT.XMIN) GO TO 10
CKF=BETAR/(2.*PI)*CEXP(-I*BETAR**2*K*X/MR)*(1./X-I*K/MR
1 *ALOG(ABS(X)))
RETURN
10 CONTINUE
D=SQRT(H1**2+(BETAR*H2)**2)
R=D*SQRT(K**2+(D*ALOG(ERROR)/(BETAR*H2*X))**2)
N1=(GAMMA-R)/(2.*PI)
N2=(GAMMA+R)/(2.*PI)
CKF=0.
IF(X.GT.0.) GO TO 50
DO 40 N=N1,N2
GN=GAMMA-2.*PI*N
S=(K*D)**2-GN**2
IF(S.GE.0.) RJOT=-SQRT(S)*ABS(K)/K
IF(S.LT.0.) RJOT=I*SQRT(-S)
ANM=(GN*H1-BETAR*H2*RJOT)/D**2
CKF=CKF+RN(ANM)
40 CONTINUE
RETURN
50 CONTINUE
DO 70 N=N1,N2
GN=GAMMA-2.*PI*N
S=(K*D)**2-GN**2
IF(S.GE.0.) RJOT=-SQRT(S)*ABS(K)/K
IF(S.LT.0.) RJOT=I*SQRT(-S)
ANP=(GN*H1+BETAR*H2*RJOT)/D**2
CKF=CKF-RN(ANP)
70 CONTINUE
CKF=CKF-BETAR**2*K/(2.*MR)*SINH(BETAR**2*K
1 *H2/MR)*CEXP(-I*BETAR**2*K*X/MR)/(COSH(BETAR**2*K*H2/MR)-
2 COS(GAMMA+K*H1/MR))
RETURN
END

```

ORIGINAL PAGE IS
OF POOR QUALITY.

SUBROUTINE PHITHH

Program computes the Fourier
transform of the correlation
function in the circumferential
direction.

FUNCTION PHITHH(ARGUM2)

C
C
C PROGRAM CALCULATES THE FOURIER TRANSFORM OF THE CORRELATION
C FUNCTION IN THE AZIMUTHAL DIRECTION AS A FUNCTION OF

C
C 12/14/79 VERSION USES GAUSSIAN AUTOCORRELATION FUNCTION.
C FORM FOLLOWS EQUATION 27 IN W.D. MARK'S "ROTOR INLET
C TURBULENCE" PAGE 10.

C DATA PI/3.14159/

C
C NEED SWITCH TO AVOID UNDERFLOW IN EXPONENTIATION. RANGE
C IS E+38.

C
C A=ARGUM2**2
C B=A/PI
C IF(B.GT.87.) GO TO 10
C C=2.*EXP(-B)
C GO TO 20
10 C=0.
20 CONTINUE
PHITHH=C
RETURN
END

ORIGINAL PAGE IS
OF POOR QUALITY

SUBROUTINE PHIXHT

Program calculates the Fourier
transform of the correlation
function in the axial direction.

FUNCTION PHIXHT(ARGUM1)

C
C PROGRAM CALCULATES THE FOURIER TRANSFORM OF THE CORRELATION
C FUNCTION IN THE AXIAL DIRECTION AS A FUNCTION OF
C NONDIMENSIONAL FREQUENCY

C
C 12/14/79 VERSION USES GAUSSIAN AUTOCORRELATION FUNCTION.
C FORM FOLLOWS EQUATION 27 IN W.D. MARK'S "ROTOR INLET
C TURBULENCE" PAGE 17.

C
C NEED SWITCH TO AVOID UNDERFLOW ON EXPONENTIATION. RANGE
C IS E+-38

C
C DATA PI/3.14159/
C A=ARGUM1**2
C B=A/PI
C IF(B.GT.87.) GO TO 10
C C=2.*EXP(-B)
C GO TO 20
10 C=0.
20 CONTINUE
PHIXHT=C
RETURN
END

ORIGINAL PAGE IS
OF POOR QUALITY

(+)

SUBROUTINE PRES

Program generates the complex
pressure distribution across
the stator vane chord.

```
SUBROUTINE PRES(WH,X,K,GAMMA,MR,H1,H2,MSEG,F,IER)
REAL K,MR,KX
COMPLEX I,WH,F,A,CKF
COMPLEX G,G0,G1,G2,G3
DIMENSION F(100),A(100,100),WA(100),B(100)
DATA I/(0.,1.)/,ERROR/.0001/,PI/3.14159/
DATA (B(J),J=1,100)/100*1.3/
G(X)=(G0+G1*X+G2*X**2+G3*X**3)*CEXP(I*K*MR*X)
B(MSEG)=.5
BFTAR=SQRT(1.-MR**2)
G0=I*BFTAR*K/(2.*PI*MR)
G1=BFTAR*K**2/(2.*PI)*(1./MR**2-0.5)
G2=I*BFTAR*K**3/(4.*PI)*(1./(2.*MR)-1./MR**3)
G3=-BFTAR*K**4/(12.*PI)*(1./MR**4-1./(2.*MR**2)-2.125)
DO 10 M=1,MSEG
X=COS((M-.5)*PI/MSEG)
F(M)=WH*CEXP(I*KX*X)
10 CONTINUE
N=MSEG
DO 50 M=1,N
DO 50 L=1,N
S=-ALOG(2.)
DO 40 IR=1,N
S=S-2.*B(IR)/IR*COS((M-.5)*IR*PI/N)*COS(PI*IR*L/N)
40 CONTINUE
ARG=COS((M-.5)*PI/N)-COS(L*PI/N)
CALL KERNEL(ARG,K,GAMMA,MR,H1,H2,ERROR,CKF)
A(M,L)=P(L)*(CKF+G(ARG)*(S-ALOG(ABS(ARG))))*PI/N
50 CONTINUE
CALL LEQTIC(A,MSEG,100,F,1,100,3,WA,IER)
RETURN
END
```

ORIGINAL PAGE IS
OF POOR QUALITY

SUBROUTINE RMODE

Program computes the radial
mode shape for an annular
duct.

```

SUBROUTINE RMODE (MM,X,AMN,BMN,PSI,D,IERROR)
DIMENSION IERROR(2)
IF(X.EQ.0.) GO TO 300
FACTOR=1.
M=MM
IF(M.LT.1) GO TO 100
200 CONTINUE
CALL BESJ (X,M,BJ,D,IERROR(1))
CALL BESY (X,M,BY,IERROR(2))
PSI=FACTOR*(AMN*BJ+BMN*BY)
RETURN
102 M=-M
K=M/2
IF((1.*M)/(2.).GT.(1.*K)) FACTOR=-1.
GO TO 200
300 CONTINUE
PSI=AMN
IERROR(1)=0
IERROR(2)=0
RETURN
END

```

ORIGINAL PAGE IS
OF POOR QUALITY

SUBROUTINE SCALLR

Program yields the turbulence
length scale in the radial
direction.

FUNCTION SCALLP(R)

C
C PROGRAM CALCULATES THE INLET TURBULENCE LENGTH
C SCALE IN THE RADIAL DIRECTION AS A FUNCTION OF THE MEAN RADIUS.
C THE LENGTH SCALE IS NONDIMENSIONALIZED ON THE DUCT RADIUS.
C NOTE SIGVAR.LE.R.LE.1.

C
C 12/21/79 VERSION USES A CONSTANT

R=0.50
SCALLR=B
RETURN
END

ORIGINAL PAGE IS
OF POOR QUALITY

SUBROUTINE SCALLX

Program yields the turbulence
length scale in the axial
direction.

C <MTHEDPALD>SCALLY.FOR;4 Mon 29-Sep-80 11:11PM PAGE 1

FUNCTION SCALLY(R)

C
C PROGRAM CALCULATES THE INLET TURBULENCE LENGTH SCALE
C IN THE AXIAL DIRECTION AS A FUNCTION OF THE MEAN RADIUS.
C LENGTH SCALE IS NONDIMENSIONALIZED ON THE DUCT RADIUS.

C
C 12/16/79 VERSTON USES A CONSTANT
C NOTE SIGMAF.LE.R.LE.1.

R=40.
SCALLX=8
RETURN
END

ORIGINAL PAGE 13
OF POOR QUALITY

SUBROUTINE STHETA

Program yields the turbulence
length scale in the circumfer-
ential direction.

C <MTHEODALD>STHETA.FOR;4 Mon 29-Sep-80 11:12PM PAGE 1

FUNCTION STHETA(R)

C
C PROGRAM CALCULATES THE INLET TURBULENCE LENGTH SCALE
C IN THE AZIMUTHAL DIRECTION AS A FUNCTION OF MEAN RADIUS.
C THE LENGTH SCALE IS NONDIMENSIONALIZED ON THE DUCT RADIUS.

C DATA PI/3.14159/

C
C 12/18/79 VERSION USES A CONSTANT
C NOTE SIGVAR.LE.R.LF.1.

B=0.5
STHETA=B
RETURN
END

ORIGINAL PAGE 19
OF POOR QUALITY

PROGRAM MAPIN/
SUBROUTINE MAPPER
(with sample execution)

Program lists which duct modes
will propagate for inlet turbu-
lence noise.

```

DIMENSION RDATA(20)
REAL MT,MA

```

```

C
C
C
C  INPUT VARIABLES TO SUBROUTINE MAPPER FOR LISTING OF ALL
C  PROPAGATING MODES FOR TURBULENCE PROGRAMS AT A
C  GIVEN FREQUENCY

```

```
1001    FORMAT(G20.8)
        WRITE(5,2003)
2003    FORMAT(' HUB RADIUS DIVIDED BY DUCT RADIUS =')
        READ(5,1001) SIGMAR
        WRITE(5,2103) SIGMAR
2103    FORMAT(' SIGMAR=',E16.8)
```

```

C
      WRITE(5,2030)
2030  FORMAT(' MT =')
      READ(5,1001) MT
      WRITE(5,2130) MT
2130  FORMAT(' MT=',E16.8)
      WRITE(5,2031)
2031  FORMAT(' MA =')
      READ(5,1001) MA
      WRITE(5,2131) MA
2131  FORMAT(' MA =',E16.8)
      WRITE(5,2037)
2037  FORMAT(' ACCURACY OF BESSEL FN =')
      READ(5,1001) EB
      WRITE(5,2137) EB
2137  FORMAT(' EB=',E16.8)
      WRITE(5,2038)
2038  FORMAT(' ACCURACY OF CONVERGENCE TO ROOT XMN =')
      READ(5,1001) EC
      WRITE(5,2138) EC
2138  FORMAT(' EC=',E16.8)

```

```
RDATA(1)=MT
RDATA(2)=MA
RDATA(9)=EB
RDATA(10)=EC
```

```
RDATA(5)=SIGM/R
```

```
CALL MAPPER(RDATA)
STOP
END
```

ORIGINAL PAGE IS
OF POOR QUALITY

```

SUBROUTINE MAPPER(RDATA)
  DIMENSION IER(3),PDATA(20)
  REAL MT,MA

```

ORIGINAL PAGE IS
OF POOR QUALITY

PROGRAM LISTS ALL PROPAGATING MODES FOR INLET AND WAKE
TURBULENCE PROGRAMS WITHOUT CALCULATING MODAL
AMPLITUDES. USE THIS PROGRAM AS A PRECURSOR TO
INTURB OR WATURB SEARCH ROUTINES TO ESTIMATE RUN TIME.

```

1001  FORMAT(G20.8)
      WRITE(5,110)
110   FORMAT(' NOISE FREQUENCY/SHAFT FREQUENCY=')
      READ(5,1001) OMEGA
      RDATA(8)=OMEGA
115   FORMAT(' OMEGA=',E10.4)
      WRITE(5,115) RDATA(8)
      MT=RDATA(1)
      MA=RDATA(2)
      SIGMAR=RDATA(5)
      EB=RDATA(9)
      EC=RDATA(10)

```

$$XMAX=OMEGA*MT/(1.-MA**2)**.5$$

```
WRITE(5,2001) XMAX
2001 FORMAT(' XMAX('XAX) FOR PROPAGATION =',E16.8)
```

START WITH PLANE WAVE MODE (0,1). COUNT UP IN N, THEN M UNTIL ALL POSSIBLE HIGHER MODES ARE CUT OFF.

J=1
M=0

RESTART N COUNT HERE FOR NEW M

$$N = \emptyset$$

C INCREMENT N

C
20 N=N+1

ORIGINAL PAGE IS
OF POOR QUALITY

C
C
C MABS=IABS(M)

C
C
C
C CALL ANRT (MABS,N,SIGMAR,EB,EC,XMN,IEB,IEC)

C
C
C
C IF MODE IS CUT OFF, GO TO 6000

C
C IF(XMN.GE.XMAX) GO TO 6000

C
C
C
3000 WRITE(5,3000)
FORMAT('MODE DATA')
3001 WRITE(5,3001) OMEGA,M,N,XMN
3001 FORMAT('OMEGA=',E10.4,' M=',I3,' N=',I3,' XMN=',E10.4)
IF(XMN.EQ.0.) GO TO 1000

COFFRA=XMAX/XMN
4020 WRITE(5,4000) COFFRA
FORMAT('CUTOFF RATIO FOR MODE=',E10.4)
GO TO 1005

1000 CONTINUE
4005 WRITE(5,4005)
FORMAT(' PLANE WAVE MODE: CUTOFF RATIO IS + INFINITE')
1005 CONTINUE

WRITE(5,3002) IEB
3002 FORMAT('SUM OF BESSEL FUNCTION ERROR CODES =',I3)
3003 WRITE(5,3003) IEC
3003 FORMAT('ERROR CODE FOR CONVERGENCE TO ROOT XMN =',I3)

C
C
C NORMALIZE MODE AMPLITUDE

C
C CALL EIGEN (MABS,SIGMAR,XMN,AMN,BMN,EB,IER)

C
C
3004 WRITE(5,3004) AMN,BMN
FORMAT('AMN =',E16.8,' BMN =',E16.8)
3005 WRITE(5,3005) IER
FORMAT('ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC =',I3)

C
C
C
C
C
C

ORIGINAL PAGE IS
OF POOR QUALITY

C
C

MMM=M

C
C

DO NOT SWITCH SIGN ON M IF M=0

C
C

IF(M.EQ.0) GO TO 20

C
C

MMM=-MMM

C
C

WRITE(5,8300) MMM,N,RDATA(8)

8300 FORMAT('JM=',I5,' N=',I5,' OMEGA=',E10.4)

C
C

SWITCH SIGN ON M

C
C

C
C

C
C

GO TO 20

C
C

C
C

C
C

IF MODE IS CUTOFF, DECIDE WHICH MODE TO TRY NEXT.

C
C

C
C

C
C

NMAX=N-1

WRITE(5,6001) NMAX

C
C

C
C

J=J+1

C
C

INCREMENT M

C
C

M=M+1

GO TO 15

C
C

C
C

N=1 TO REACH THIS POINT

C
C

7000 CONTINUE

C
C

WRITE(5,7001)

C
C

7001 FORMAT(' NO MORE PROPAGATING MODES FOR THIS OMEGA')

10 CONTINUE

WRITE(5,9001)

C
C

C
C

9001 FORMAT(' PROBLEM COMPLETED')

RETURN

END

Sample Execution of MAPIN/MAPPER

MAPPER
HUB RADIUS DIVIDED BY DUCT RADIUS =
.484
SIGMAR= 0.48400000E+00
MT =
.508
MT= 0.50800000E+00
MA =
.323
MA = 0.32300000E+00
ACCURACY OF BESSEL FN =
.0001
EB= 0.10000000E-03
ACCURACY OF CONVERGENCE TO ROOT XMN =
.0001
EC= 0.10000000E-03
NOISE FREQUENCY/SHAFT FREQUENCY=
15.
OMEGA= .1500E+02
XMN(MAX) FOR PROPAGATION = 0.80515728E+01

MODE DATA

OMEGA= .1500E+02 M= 0 N= 1 XMN= .0000E+00
PLANE WAVE MODE: CUTOFF RATIO IS + INFINITE
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.10000000E+01 BMN = 0.00000000E+00
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

MODE DATA

OMEGA= .1500E+02 M= 0 N= 2 XMN= .6205E+01
CUTOFF RATIO FOR MODE= .1298E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = -0.26166472E+01 BMN = 0.27171760E+01
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

LARGEST PROPAGATING N FOR THIS M = 2
%FRSAPR Floating underflow PC= 3100
%FRSAPR Floating underflow PC= 3146

ORIGINAL PAGE 13
OF POOR QUALITY

MODE DATA

OMEGA= .1500E+02 M= 1 N= 1 XMN= .1371E+01
CUTOFF RATIO FOR MODE= .5873E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.15152306E+01 BMN = -0.42119467E+00
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -1 N= 1 OMEGA= .1500E+02

MODE DATA

OMEGA= .1500E+02 M= 1 N= 2 XMN= .6390E+01
CUTOFF RATIO FOR MODE= .1260E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.14356938E+01 BMN = 0.32269858E+01
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -1 N= 2 OMEGA= .1500E+02

LARGEST PROPAGATING N FOR THIS M = 2

MODE DATA

OMEGA= .1500E+02 M= 2 N= 1 XMN= .2708E+01
CUTOFF RATIO FOR MODE= .2973E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.20525722E+01 BMN = -0.42471320E+00
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -2 N= 1 OMEGA= .1500E+02

MODE DATA

OMEGA= .1500E+02 M= 2 N= 2 XMN= .6920E+01
CUTOFF RATIO FOR MODE= .1164E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.36560636E+01 BMN = 0.74837045E+00
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

ORIGINAL PAGE 18
OF POOR QUALITY

M= -2 N= 2 OMEGA= .1500E+02

LARGEST PROPAGATING N FOR THIS M = 2

MODE DATA

OMEGA= .1500E+02 M= 3 N= 1 XMN= .3987E+01
CUTOFF RATIO FOR MODE= .2020E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.26023450E+01 BMN = -0.32589376E+00
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -3 N= 1 OMEGA= .1500E+02

MODE DATA

OMEGA= .1500E+02 M= 3 N= 2 XMN= .7747E+01
CUTOFF RATIO FOR MODE= .1039E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.35705322E+01 BMN = -0.89511162E+00
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -3 N= 2 OMEGA= .1500E+02

LARGEST PROPAGATING N FOR THIS M = 2

MODE DATA

OMEGA= .1500E+02 M= 4 N= 1 XMN= .5200E+01
CUTOFF RATIO FOR MODE= .1549E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.31336392E+01 BMN = -0.20930877E+00
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -4 N= 1 OMEGA= .1500E+02

LARGEST PROPAGATING N FOR THIS M = 1

C-3

ORIGINAL PAGE 13
OF POOR QUALITY

MODE DATA

OMEGA= .1500E+02 M= 5 N= 1 XMN= .6355E+01
CUTOFF RATIO FOR MODE= .1267E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.36182370E+01 BMN = -0.11930907E+00
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -5 N= 1 OMEGA= .1500E+02

LARGEST PROPAGATING N FOR THIS M = 1

MODE DATA

OMEGA= .1500E+02 M= 6 N= 1 XMN= .7473E+01
CUTOFF RATIO FOR MODE= .1077E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.40542452E+01 BMN = -0.61590101E-01
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -6 N= 1 OMEGA= .1500E+02

LARGEST PROPAGATING N FOR THIS M = 1
NO MORE PROPAGATING MODES FOR THIS OMEGA
PROBLEM COMPLETED
STOP

END OF EXECUTION

CPU TIME: 29.82 ELAPSED TIME: 3:4.03

EXIT.

^C

MAPPER

HUB RADIUS DIVIDED BY DUCT RADIUS =

.484

SIGMAR= 0.48400000E+00

MT =

.508

MT= 0.50800000E+00

MA =

.323

MA = 0.32300000E+00

ACCURACY OF BESSEL FN =

.0001

EB= 0.10000000E-03

ORIGINAL PAGE
OF POOR QUALITY

ACCURACY OF CONVERGENCE TO ROOT XMN =
.0001
EC= 0.10000000E-03
NOISE FREQUENCY/SHAFT FREQUENCY=
30.
OMEGA= .3000E+02
XMN(MAX) FOR PROPAGATION = 0.16103146E+02

MODE DATA

OMEGA= .3000E+02 M= 0 N= 1 XMN= .0000E+00
PLANE WAVE MODE: CUTOFF RATIO IS + INFINITE
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.10000000E+01 BMN = 0.00000000E+00
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

MODE DATA

OMEGA= .3000E+02 M= 0 N= 2 XMN= .6205E+01
CUTOFF RATIO FOR MODE= .2595E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = -0.26166472E+01 BMN = 0.27171760E+01
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

MODE DATA

OMEGA= .3000E+02 M= 0 N= 3 XMN= .1224E+02
CUTOFF RATIO FOR MODE= .1316E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = -0.24929737E+01 BMN = 0.47091179E+01
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

LARGEST PROPAGATING N FOR THIS M = 3
ZFRSAPR Floating underflow PC= 3100

ZFRSAPR Floating underflow PC= 3146

MODE DATA

OMEGA= .3000E+02 M= 1 N= 1 XMN= .1371E+01
CUTOFF RATIO FOR MODE= .1175E+02
SUM OF BESSEL FUNCTION ERROR CODES = 0

ORIGINAL PAGE 15
OF PCOR QUALITY

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.15152306E+01 BMN = -0.42119467E+00
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -1 N= 1 OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02 M= 1 N= 2 XMN= .6390E+01
CUTOFF RATIO FOR MODE= .2520E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.19356938E+01 BMN = 0.32269858E+01
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -1 N= 2 OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02 M= 1 N= 3 XMN= .1232E+02
CUTOFF RATIO FOR MODE= .1307E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.43514410E+01 BMN = 0.30726765E+01
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -1 N= 3 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 3

MODE DATA

OMEGA= .3000E+02 M= 2 N= 1 XMN= .2708E+01
CUTOFF RATIO FOR MODE= .5946E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.20525722E+01 BMN = -0.42471320E+00
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -2 N= 1 OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02 M= 2 N= 2 XMN= .6920E+01
CUTOFF RATIO FOR MODE= .2327E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0

ORIGINAL PAGE IS
OF POOR QUALITY

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.36560636E+01 BMN = 0.74837045E+00
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -2 N= 2 OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02 M= 2 N= 3 XMN= .1258E+02
CUTOFF RATIO FOR MODE= .1280E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.44592966E+01 BMN = -0.29055613E+01
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -2 N= 3 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 3

MODE DATA

OMEGA= .3000E+02 M= 3 N= 1 XMN= .3987E+01
CUTOFF RATIO FOR MODE= .4039E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.26023450E+01 BMN = -0.32589376E+00
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -3 N= 1 OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02 M= 3 N= 2 XMN= .7747E+01
CUTOFF RATIO FOR MODE= .2079E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.35705322E+01 BMN = -0.89511162E+00
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -3 N= 2 OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02 M= 3 N= 3 XMN= .1301E+02
CUTOFF RATIO FOR MODE= .1238E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0

ORIGINAL PAGE IS
OF POOR QUALITY

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = -0.18754669E+00 BMN = 0.53089864E+01
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0

M= -3 N= 3 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 3

MODE DATA

OMEGA= .3000E+02 M= 4 N= 1 XMN= .5200E+01
CUTOFF RATIO FOR MODE= .3097E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.31336392E+01 BMN = -0.20930877E+00
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0

M= -4 N= 1 OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02 M= 4 N= 2 XMN= .8798E+01
CUTOFF RATIO FOR MODE= .1830E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.33061669E+01 BMN = -0.15169850E+01
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0

M= -4 N= 2 OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02 M= 4 N= 3 XMN= .1359E+02
CUTOFF RATIO FOR MODE= .1185E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.34317489E+01 BMN = 0.40298049E+01
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0

M= -4 N= 3 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 3

ORIGINAL PAGE IS
OF POOR QUALITY

MODE DATA

OMEGA= .3000E+02 M= 5 N= 1 XMN= .6355E+01
CUTOFF RATIO FOR MODE= .2534E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.36182370E+01 BMN = -0.11930907E+00
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -5 N= 1 OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02 M= 5 N= 2 XMN= .9995E+01
CUTOFF RATIO FOR MODE= .1611E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.32789852E+01 BMN = -0.15982724E+01
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -5 N= 2 OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02 M= 5 N= 3 XMN= .1432E+02
CUTOFF RATIO FOR MODE= .1125E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.50087871E+01 BMN = 0.16051647E+01
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -5 N= 3 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 3

MODE DATA

OMEGA= .3000E+02 M= 6 N= 1 XMN= .7473E+01
CUTOFF RATIO FOR MODE= .2155E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.40542452E+01 BMN = -0.61590101E-01
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -6 N= 1 OMEGA= .3000E+02

ORIGINAL PAGE IS
OF POOR QUALITY

MODE DATA

OMEGA= .3000E+02 M= 6 N= 2 XMN= .1127E+02
CUTOFF RATIO FOR MODE= .1429E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.34647685E+01 BMN = -0.14296053E+01
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0

M= -6 N= 2 OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02 M= 6 N= 3 XMN= .1518E+02
CUTOFF RATIO FOR MODE= .1061E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.51904865E+01 BMN = -0.42382837E+00
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0

M= -6 N= 3 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 3

MODE DATA

OMEGA= .3000E+02 M= 7 N= 1 XMN= .8565E+01
CUTOFF RATIO FOR MODE= .1880E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.44478450E+01 BMN = -0.30159084E-01
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0

M= -7 N= 1 OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02 M= 7 N= 2 XMN= .1257E+02
CUTOFF RATIO FOR MODE= .1281E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.37694693E+01 BMN = -0.11581721E+01
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0

M= -7 N= 2 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 2

ORIGINAL PAGE IS
OF POOR QUALITY

MODE DATA

OMEGA= .3000E+02 M= 8 N= 1 XMN= .9641E+01
CUTOFF RATIO FOR MODE= .1670E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.48101954E+01 BMN = -0.14625833E-01
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -8 N= 1 OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02 M= 8 N= 2 XMN= .1386E+02
CUTOFF RATIO FOR MODE= .1162E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.41235105E+01 BMN = -0.85984372E+00
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -8 N= 2 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 2

MODE DATA

OMEGA= .3000E+02 M= 9 N= 1 XMN= .1071E+02
CUTOFF RATIO FOR MODE= .1504E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.51513706E+01 BMN = -0.65555876E-02
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -9 N= 1 OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02 M= 9 N= 2 XMN= .1512E+02
CUTOFF RATIO FOR MODE= .1065E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.44743524E+01 BMN = -0.59372922E+00
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -9 N= 2 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 2

ORIGINAL PAGE IS
OF POOR QUALITY

MODE DATA

OMEGA= .3000E+02 M= 10 N= 1 XMN= .1177E+02
CUTOFF RATIO FOR MODE= .1368E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.54757875E+01 BMN = -0.30348101E-02
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -10 N= 1 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 1

MODE DATA

OMEGA= .3000E+02 M= 11 N= 1 XMN= .1283E+02
CUTOFF RATIO FOR MODE= .1256E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.57877752E+01 BMN = -0.13177058E-02
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -11 N= 1 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 1

MODE DATA

OMEGA= .3000E+02 M= 12 N= 1 XMN= .1388E+02
CUTOFF RATIO FOR MODE= .1160E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.60893310E+01 BMN = -0.63729882E-03
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -12 N= 1 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 1

MODE DATA

OMEGA= .3000E+02 M= 13 N= 1 XMN= .1493E+02
CUTOFF RATIO FOR MODE= .1079E+01
SUM OF BESSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.63824353E+01 BMN = -0.1813051E-03
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

ORIGINAL PAGE 13
OF POOR QUALITY

M= -13 N= 1 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 1

MODE DATA

OMEGA= .3000E+02 M= 14 N= 1 XMN= .1598E+02

CUTOFF RATIO FOR MODE= .1008E+01

SUM OF BESSEL FUNCTION ERROR CODES = 0

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0

AMN = 0.66676797E+01 BMN = -0.10550421E-03

ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -14 N= 1 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 1

NO MORE PROPAGATING MODES FOR THIS OMEGA

PROBLEM COMPLETED

STOP

END OF EXECUTION

CPU TIME: 1:40.60

ELAPSED TIME: 8:6.24

EXIT.